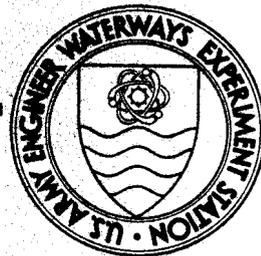


DREDGED MATERIAL RESEARCH PROGRAM



TECHNICAL REPORT D-78-43

PHYSICAL AND CHEMICAL CHARACTERIZATION OF DREDGED MATERIAL SEDIMENTS AND LEACHATES IN CONFINED LAND DISPOSAL AREAS

by

Kar Y. Yu, Kenneth Y. Chen

Environmental Engineering Program

University of Southern California

Los Angeles, Calif. 90007

and

Robert D. Morrison, James L. Mang

SCS Engineers

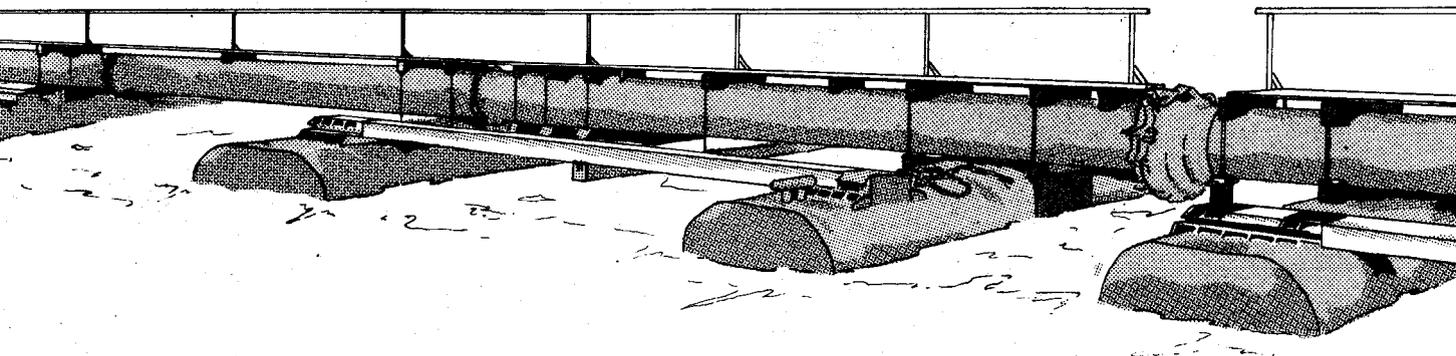
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IN REPLY REFER TO: WESEV

30 September 1978

SUBJECT: Transmittal of Technical Report D-78-43

TO: All Report Recipients

1. The technical report transmitted herewith represents the results of Work Unit 2D05 of Task 2D, Confined Disposal Area Effluent and Leachate Control, of the Corps of Engineers' Dredged Material Research Program (DMRP). Task 2D was a part of the Environmental Impacts and Criteria Development Project (EICDP). This project was, in part, concerned with establishing a data base and evaluating potential pollution problems associated with different modes of dredged material disposal. The work units in Task 2D dealt more specifically with environmental impacts of confined land disposal of dredged material.

2. The overall objective of the Work Unit 2D05 study was to gather field data on the quality and quantity of interstitial waters and leachates from within, beneath, and down-gradient from four confined land disposal areas. Initially considerable background information on each site was obtained from the literature, personal contacts, and from concise field measurements. Factors deemed important in affecting the production and composition of leachates include: (a) dredged material composition, (b) composition of the adjacent and underlying soils, (c) hydrogeological conditions beneath the site (e.g., groundwater flow rate and pattern, geological formations encountered, and extent of groundwater regime), (d) climate, and (e) site-specific conditions (e.g., chemical and biological activities, soil moisture and precipitation patterns, pH, and Eh).

3. At each of the four field sites, ten sampling locations were usually established: four locations within the disposal area, four off-site monitoring stations down-gradient in the groundwater flow pattern, and two off-site stations up-gradient in the groundwater flow pattern for background data. Sediment and water samples were initially obtained from four depths. At locations within the disposal area, two sampling horizons were within the old dredged material. Each sampling station was hand bored and cored; sediment samples were collected at horizons later used for the collection of water samples. Samples were obtained from the unsaturated zone above the local groundwater table with ceramic cup soil water samplers, while groundwater samples were collected from plastic wellheads. Four sets of water samples were collected over a nine-month period.

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4. The results of the study showed that leachate quality is a function of the physical and chemical nature of the disposed dredged material, site-specific hydrogeological patterns, and environmental conditions of the area surrounding the site (e.g., physical and chemical nature of the adjacent soils). In general, the study found that sodium, potassium, calcium, magnesium, chloride, total organic carbon, alkalinity, and manganese in leachates from disposal areas may impact local groundwater, especially if the water is used for drinking water or agricultural purposes. The data also indicated that low concentrations of cadmium, copper, iron, mercury, lead, zinc, nickel, and phosphate may reach groundwaters, but the levels should not pose water quality problems. Iron and manganese appeared to be produced by localized environmental conditions, and thus their mobility was not considered directly related to dredged material disposal activities. Certain sites showed localized high levels of certain contaminants, including nickel, cadmium, and copper. The highest levels for most trace metals were in off-site (monitoring and background) water samples, collected beneath an acid, poorly buffered salt marsh habitat. The major contaminants at the brackish water sites appeared to be the salts of major ions.

5. The data in this publication should be used, in context with past and future findings, for determining the impact of land disposal on groundwater quality. It is anticipated that these published results should aid those persons involved with criteria development, groundwater monitoring, environmental impact reports, permit programs, or other regulatory functions.



JOHN L. CANNON

Colonel, Corps of Engineers
Commander and Director

20. ABSTRACT (Continued).

Twenty-six sampling devices were installed at each site with 12 on-site, 10 off-site, and 4 beneath the site. Water samples were collected four times in nine months; soil and dredged material samples were collected during the first sampling visit.

Analytical data show some significant increase in concentrations of chloride, potassium, sodium, calcium, magnesium, TOC, alkalinity, iron, and manganese in downgradient groundwaters. Concentrations of chlorinated hydrocarbons, cadmium, copper, mercury, lead, zinc, phosphate, and nickel were generally very low.

Results obtained from this limited monitoring period have shown some degradation of groundwater quality due to the upland disposal of dredged material. Additional data are needed to formulate guidelines for the selection of disposal sites with minimal environmental impacts.

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SUMMARY

When dredged material is disposed of in upland areas, the water quality impacts can be divided into two categories; the discharge of effluent slurries to surface waters, and the migration of leachates into underlying groundwaters. The purpose of this study was to evaluate the latter impact. This field study was conducted to evaluate the possible degradation of groundwater quality from confined upland disposal of dredged material.

Prior to site selection, a literature review and field investigation of prospective areas were conducted. This information provided the basis for choosing the four locations which best suited the goals of this study. The four sites selected for field investigation were Grand Haven, Michigan; Sayreville, New Jersey; Houston, Texas; and Pinto Island, Alabama. All available records pertaining to each site were examined, including: information such as historic, geographic, topographic and climatological data as well as, regional and site-specific hydrological data. Additional hydrogeological data were obtained in the field study.

A simplistic representation of the groundwater hydrology at each of these case study sites may be seen on Figure 69.

A comprehensive review of sampling devices and techniques was also performed. Vacuum/pressure lysimeters were chosen for interstitial water sampling and PVC well points for groundwater monitoring. In addition, by using specially constructed ABS sampling tubes, dredged material and soil samples were obtained from locations that would provide insight as to both lateral and vertical chemical and physical stratification. Twenty-six water samplers were installed at each site with 12 on-site, 10 off-site, and four directly beneath the sites. The ratio of lysimeters versus well points at each locality was determined by the specific hydrogeologic framework at the site. Four sampling visits were scheduled approximately every three months. Sampling and shipping techniques developed for the study were implemented during these visits.

The results from the analysis of on-site dredged material and off-site soils in relation to the examination of vertical and lateral differentiations, in general, failed to reveal any systematic

changes. For any particular parameter, both increases and decreases in values occurred in different locations as well as at different depths within each site. This is most likely due to the stratification caused by intermittent disposal operations.

Results of the particle size analysis of the dredged material suggested that the material in upland disposal areas is slightly more sandy than original bottom sediments. The reason for the difference might be due to the fact that finer particles tend to be carried with effluents to surface receiving waters due to turbulence and/or insufficient residence time.

Analysis of leachates and groundwaters indicate that potential adverse water quality impacts will most likely be due to the increases of chloride, potassium, sodium, calcium, total organic carbon, alkalinity, iron, and manganese. The extent of the potential impact was found to be a function of the physiochemical properties of the disposed dredged material, site-specific groundwater hydrogeological patterns, and environmental conditions of the area surrounding the site. The field monitoring of the case study sites generally revealed very low concentration levels of cadmium, copper, mercury, lead, zinc, phosphate, and nickel in downgradient groundwater.

In general, soluble phase sodium, potassium, and chloride were shown to have similar behavior. Dilution was the most important mechanism affecting the migration of these ions. Sodium and potassium might also be affected by ion-exchange reactions with the exchangeable ions held in the soil/dredged material. All three ions were shown to have affected the groundwater in at least one site.

Soluble phase calcium and magnesium were higher in the on-site dredged material samples than the off-site samples at two sites, indicating a potential for these two ions to migrate away from the site. Actual leaching of these two ions was also observed. Possible mechanisms regulating the transport of these two ions included ion exchange reactions with soil/dredged material, dissolution of nesquehonite and hydromagnesite for magnesium.

Levels of TOC and alkalinity were observed to have increased in groundwater below two of the case study sites. The transport of

alkalinity was probably regulated by biological oxidation and the dissolution/precipitation of calcite.

The soluble phase phosphate concentrations detected in this study were low, ranging from below the detection limit to a high of 0.91 mg/l (as P). The low level phosphate detected was probably due to adsorption onto clay particles. Although one of the case study sites had a higher phosphate average for the on-site samples than the off-site samples, there was no appreciable difference among the groundwater samples collected directly below the sites, downgradient from the site and upgradient from the site.

With the exception of manganese and iron, concentrations of trace metals in the leachate samples were mostly in the ppb or sub-ppb ranges. At such a low concentration range, solid transformation due to change in the redox condition, precipitation/dissolution, complexation, and adsorption were expected to play dominant roles in regulating their transport.

In general, in an aerobic environment, the stable solids that control the solubilities of these metal ions are oxides, hydroxides, carbonates, and silicates. Under reducing conditions, especially in saline sediments, most trace metals may gradually precipitate as sulfides with very low soluble concentrations in solution.

Adsorption could help account for the low levels of certain trace metals and chlorinated hydrocarbons in the soil/dredged material interstitial waters. The most important adsorbents included hydrated oxides of iron and manganese, soil organic matter and various clay minerals.

Total chlorinated hydrocarbons appeared to exist at higher levels in the dredged material than in off-site soil samples. This could be due to the accumulation of chlorinated hydrocarbons from industrial/domestic discharges into the waterways. The upper soil samples generally contained higher concentrations of chlorinated hydrocarbons than the samples obtained a few feet below. No soluble chlorinated hydrocarbons were observed in groundwater. It is expected that the chlorinated hydrocarbons that accumulated in the dredged material will not migrate away from the site.

The complexation effect usually accounted for the high levels of trace metals found in the soil/dredged material interstitial

waters. The major ligands responsible for complexation were chloride, organic species, hydroxide, carbonate, and sulfate.

The results of this limited study have shown that leachates from upland dredged material disposal areas have caused some degradation of underlying groundwaters. Due to the short duration of this monitoring effort, this conclusion can only be regarded as tentative. It is recommended that additional efforts should be directed to the formulation of guidelines for site selection. In order to achieve this goal, it will be necessary to carry out long-term extensive monitoring programs on the existing sites.

PREFACE

The work described in this report was performed under Contract No. DACW39-76-C-0171, entitled, "Physical and Chemical Characterization of Dredged Material Sediments and Leachates in Confined Land Disposal Areas," dated September 29, 1976, between the U. S. Army Engineer Waterways Experiment Station (WES), Vicksburg, Mississippi, and the University of Southern California, Los Angeles, California. The research was sponsored by the Environmental Laboratory (EL), WES, under the Dredged Material Research Program (DMRP), Work Unit 2D05. The study was part of DMRP Task 2D, "Confined Disposal Area Effluent and Leachate Control," of the Environmental Impacts and Criteria Development Project (EICDP).

This report is the result of field studies designed to evaluate the effect of the disposal of dredged material in confined upland areas on the quality of downgradient groundwater.

The research was conducted under the supervision of Dr. K. Y. Chen, Professor and Director, Environmental Engineering Program, USC. This report was a basis for the dissertation of K. Y. Yu, who performed most of the laboratory and data analysis.

The field studies were performed by R. D. Morrison and J. L. Mang of SCS Engineers, acting as a subcontractor to USC in this study. Individuals who contributed to different portions of the laboratory operations were: N. McCamy, L. Bhatt, J. Stone, S. Kooklam, G. Sawtelle, T. P. Pan, and A. Z. Sycip. Individuals who participated in field investigations were D. Myers, T. Boston, K. Borgers and J. Tierney. Ms. C. McMahon performed the editing and typing. Special thanks are due Dr. P. Saint of California State University at Fullerton, Department of Environmental Studies, who served SCS as Hydrological Technical Advisor.

This contract was monitored by Mr. R. E. Hoeppel, Research Microbiologist of the EL, WES, under the supervision of Dr. R. M. Engler, Manager of the EICDP. Director of the WES during the period of this study was COL J. L. Cannon, CE. Technical Director was Mr. F. R. Brown.

CONVERSION FACTORS, U. S. CUSTOMARY TO METRIC (SI)
UNITS OF MEASUREMENT

U. S. customary units of measurement used in this report can be converted to metric (SI) units as follows:

Multiply	By	To Obtain
acres	4046.873	square metres
Fahrenheit degrees	5/9*	Celsius degrees or Kelvins
feet	0.3048	metres
gallons (U.S. liquid)	3.785412	cubic decimetres
inches	25.4	millimetres
miles (U.S. statute)	1.609344	kilometres
mils	0.0254	millimetres

* To obtain Celsius (C) temperature readings from Fahrenheit (F) readings, use the following formula: $C = (5/9)(F - 32)$. To obtain Kelvin (K) readings, use: $K = (5/9)(F - 32) + 273.15$.

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PHYSICAL AND CHEMICAL CHARACTERIZATION OF
DREDGED MATERIAL SEDIMENTS AND LEACHATES
IN CONFINED LAND DISPOSAL AREAS

PART I: INTRODUCTION

Need for Corps Research

1. Sediments serve as a repository of much of the heavy metals, pesticides, biostimulants, and other organic and inorganic waste released into waterways from municipal and industrial waste discharge, mining and agriculture activities, and other point and non-point pollution sources. The physical presence of sediments in waterways necessitates dredging of the deposited material. It has been estimated that in recent years the Corps of Engineers alone has dredged an average of 290 million m³ of sediments annually from the Nation's waterways.¹ About 65 percent of this is discharged into open-water sites away from shipping channels. The rest is disposed of on land usually within a dike structure. One of the major concerns of this activity is the possible degradation of quality of both surface and groundwaters in the proximity of the disposal area.

2. Normally sediment-bound pollutants are considered to be chemically stable and unlikely to be released to the overlying waters. Considering the extremely low levels of trace metals found in the present-day ocean, despite the continuous input from land sources, it would seem that sediments are the permanent sink of trace metals. However, a disturbance in environmental conditions may result in a shift in equilibrium affecting the mobilization of chemical constituents. Open-water disposal operations have been drastically reduced in recent years due to strict water quality legislation. This curtailment is occurring despite the results of many recent studies²⁻⁵ which indicate that the release of soluble contaminants during open-water disposal is minimal. It is anticipated that confined land disposal will be a rapidly expanding activity.

Problem Assessment

3. Little information is available concerning physicochemical transformations, migration, and fate of soluble contaminants associated with the disposal of dredged sediments in confined land disposal areas. This lack of scientific data is generating some concern on the possibility of both long- and short-term contamination of surface and groundwaters. Many questions exist regarding the migration and transport mechanisms of dredged sediment leachates.

4. During dredging operations, sediment and water are mixed, transported, and disposed of in open waters, or diked areas or on uncontained land areas. This process may result in the release or removal of metals and other toxicants, with the direction of transfer being determined by the redox and chemical conditions existing at the time. When dredged material is disposed on land it is subjected to oxidation by the mixing with oxygen-rich surface waters. Repeated oxidation and reduction, induced by air contact with the influent slurry and repeated wetting and drying of the sediments by precipitation, drainage, and evaporation, may promote a short- or long-term potential for contaminant migration in sediment leachates. A schematic of a representative active disposal site is shown in Figure 1.

5. Once leachate reaches the zone of saturation, it moves under the influence of gravity flow. Two flow systems influence the eventual path of the leachate. One is a local system that usually involves a fairly short travel distance, following the local water table contour to the nearest discharge point. However, some of the water may continue to migrate downward and enter the regional flow system. The regional system is usually at greater depths, passing under local discharge points toward major points of discharge. Therefore, leachate originating at a particular site could result in the pollution of both local and regional water.⁶

6. Investigations of the generation, composition, and control of municipal landfill leachates have been conducted during recent years, primarily under the sponsorship of the Environmental Protection Agency. Most of the information generated is not

directly applicable to an understanding of leachate production from dredged sediments in confined land disposal areas because leachate production mechanisms and resulting leachate characteristics associated with dredged sediments are not comparable to those associated with municipal refuse leachates. Several significant contributing factors are:

- a. The composition and availability (release) of soluble constituents in dredged sediments are markedly different from those in municipal refuse.
- b. The moisture content of dredged material, in most cases, is much greater than that of municipal refuse.
- c. The field capacity and permeability of dredged sediments and municipal refuse are probably significantly different.

Objectives of the Study

7. Field studies are needed to determine if leachates from dredged material present a serious threat to groundwater supplies or if soil attenuation offers adequate protection. There are several general factors affecting the composition of leachate and its production. The most important of these are:

- a. The dredged material composition.
- b. The climate.
- c. Hydrogeological conditions beneath the site.
- d. Site-specific conditions; e.g., chemical and biological activities, soil moisture, pH, Eh, and other characteristics.

These factors vary considerably from site to site.

8. The overall objective of this study was to gather field data on the quality and quantity of interstitial waters and leachates from within and beneath active confined land disposal areas, together with background hydrochemical data, to determine the pollution potential of contaminated materials resulting from subsurface vertical and horizontal leaching. Specifically, objectives

were:

- a. To monitor the leachate and groundwater quality at four dredged material confined land disposal areas on four different occasions over a 9-month period. Water samples were to be analyzed for trace metals, chlorinated hydrocarbons, nutrients, and other parameters. These data were to be used to determine:

 - (1) Time-dependent changes in leachate quality at different depths.
 - (2) Effects of soil attenuation of mobile constituents.
 - (3) Changes in soil moisture.
 - (4) Groundwater dilution of leachates.

- b. To perform a detailed physical and chemical characterization of dredged sediment and sub-soil core samples at all sampling sites. These data were to be used to define:

 - (1) The pollution potential of contaminated dredged sediments.
 - (2) Transport mechanisms responsible for the migration of contaminants.
 - (3) The magnitude and extent of contaminant migration from dredged material containment areas.

PART II: EXPERIMENTAL

Grand Haven, Michigan

Site Description

9. The Grand Haven, Michigan, site provided an excellent opportunity for investigating the migration of leachates from an upland disposal area situated in a freshwater hydrologic regime. Distinctive and pertinent characteristics are listed in Table 1.

10. The dredged material disposal facility at Grand Haven, Michigan, is located near the eastern shore of Lake Michigan on the north banks of the Grand River. The Grand River empties into Lake Michigan approximately 1 mile downstream. The regional map (Figure 2) shows the location of the site in relation to the Grand River and Lake Michigan.

11. The Grand Haven site covers about 2.4 ha (6 acres) which have been diked, resulting in a roughly rectangular configuration. The northern side of the site which measures 168 m (553.8 ft) is bordered by open land; the east by land owned by Verplank Coal and Dock Company. The southern edge of 181 m (594 ft) is set back from the Grand River by about 60.9 m (200 ft). The western edge is offset from an area of low relief, referred to as the Sag, by 53.6 m (176 ft); the area between the site and the Sag is marshland.

12. The dike which encloses the site is an embankment consisting of a core of concrete/asphalt slabs from demolition work in the area. The dike has measured heights ranging from 4.5 m (15 ft) on the southern extremity to 5.4 m (18 ft) along the north (as measured December 4, 1976). Additions to the existing berm were made during April, when newly dredged material was placed in the fill; dredged material from within the site was draglined for use in the construction of this addition.

13. Depth of the dredged material, as determined during borings on December 4, 1976, was fairly uniform, ranging from 1.8 to 4.2 m (6 to 8 ft). The site map (Figure 3) shows the locations of these corings, labeled MA to MJ.

14. Dredged material removed by the Corps of Engineers from Grand Haven Harbor has been deposited at several disposal sites in the vicinity. The study site was offered to the Corps by Verplank Coal and Dock Company in 1970. Since the land was in a swampy area and of no commercial value in its natural state, the Corps issued a permit to fill the site; filling has been taking place since 1972 (personal communication, 2 November 1976, Ross Kettleman, Chief Engineer, Corps of Engineers, Grand Haven Area Office).⁷

15. Prior to its filling with dredged material, the site was characterized by a freshwater marsh flora and fauna: remnants are visible in the strip of land adjacent to the eastern edge of the fill. This area is inundated with water during the spring, when the snow melt drains to the harbor.

16. This former degraded marsh will probably be used for industrial purposes, depending upon zoning ordinances for the area, when it is filled.

Hydrological Characterization

17. Site investigations and information gathered during the literature search provided a composite of the total hydrologic system in the Grand Haven area. Table 2 lists the dates of the various field trips and the specific hydrological tests conducted during each visit.

18. The total hydrological system at the Grand Haven case study site is characterized in terms of:

- a. Climatological environment.
- b. Surface waters.
- c. Groundwater.

Site-specific field testing and accepted hydrological procedures, as well as a literature search, were employed to accurately define the nature of each of these systems.

Climatology

19. Historical climatological data for the region were obtained from the weather station at the Muskegon County Airport, approximately 16 km (10 miles) north of Grand Haven. Precipitation, temperature, relative humidity, and mean hourly wind speed recorded at this station during a 36-yr period, 1931 to 1966, are tabulated

on Table 3.⁸ A more detailed day-by-day record of precipitation and temperature extremes, and wind speed are included in Appendix A; the dates upon which field visits occurred are indicated by brackets.

Surface water

20. Surface water in the immediate vicinity of the Grand Haven disposal site normally filters through highly permeable sands of the area to a near-to-surface perched groundwater table; other surface waters drain to and accumulate in several drainage ditches, one being east of the site, which diverts runoff into the Grand River (Figure 3). Surface drainage flows from the higher elevations north of the site to the vicinity of the Grand River in the south.

21. Drainage within the diked area of the site flows from north to south and empties into the Grand River through several drainage pipes. Dredging and the subsequent leveling of the dikes during April of 1977 integrated on-site surface drainage patterns into the normal patterns for the area (surface runoff entering the site from the north and emptying into either of the drainage ditches) (Figure 3).

22. The Grand River is a major surface water body and acts as a discharge area for the shallow groundwaters in the vicinity of the site.⁹ The absence of major tidal fluctuations in Lake Michigan, into which the river flows, suggests that tidal differences would scarcely affect groundwater gradients. In order to quantify the degree to which the tide could affect flow patterns, on November 4, 1976, three 3.1-cm (1¼-in) metal well points (M4, M8, M1) were installed in a triangular configuration on the perimeter of the site. This triangulation provided the field team with a gross understanding of the suspected flow patterns at the site. Six additional well points were driven, on-site and off-site, into the shallow groundwater to further define the flow patterns (Figure 3). All well points were surveyed and absolute elevations obtained. Recordings were obtained from these wells at various time intervals to coincide with tidal variations.

23. When the nine well points had been installed and surveyed, a series of water level readings were taken at each well for a 7-hr period; measurements were recorded on an hourly basis. An

identical test was conducted on April 6, 1977, to ascertain whether tidal or elevation differences in the Grand River influenced groundwater gradients. Measurements on both test days indicated that the river stage caused no noticeable change in the water level surface; this trend was observed on all five trips in which water level measurements were taken.

25. The effect of wind chop or standing waves in Grand Haven Harbor on groundwater patterns immediately adjacent to the river-banks was not indicated by any of the constructed water table maps.

Groundwater

26. Characterization of the groundwater flow patterns at Grand Haven was determined by hydrologic investigations in three areas:

- a. Visual investigation of surface features.
- h. Water level readings from the network of nine well points and twelve monitoring wells.
- c. An off-site pumping test.

27. An attempt was made to identify those surface features which could provide signs of groundwater characteristics. The drainage ditch illustrated in Figure 3 and the designated marsh areas were studied. The area south of the site on the Harbor River showed that the Grand River acted as a point of discharge for the shallow groundwater, suggesting that this groundwater, in the immediate vicinity of the fill, was flowing towards the Grand River.

28. Phreatophytes with shallow roots were noted at the site, which indicated a shallower depth to the groundwater in the southwest. The lack of this same vegetation in the north suggested greater groundwater depths in the north and northeast. Surface vegetation provided an indication as to the most advantageous areas for installing the previously mentioned metal well points.

29. The well points designated M1 to M9 (Figure 3) also acted as monitoring stations for defining the groundwater flow near the site. A series of five water level readings, corresponding to the five sampling visits, were recorded. The results of these measurements are portrayed in the water level contour maps in Figures 4 through 8. The first three maps show that the groundwater

flows from northeast to southwest; a less pronounced gradient within the fill was due to the deposit of dredged material in April and was responsible for the change in contours in the last two maps.

Pumping tests

30. A pumping test, designed to provide information concerning the characteristics of the shallow groundwater system, was the third element of the hydrological investigation. Both on- and off-site pumping tests were originally planned but the on-site tests were unsuccessful, because the dredged material yielded little water at a pumping rate of 151 g (40 gal) per minute. Therefore, further attempts at an on-site pumping test were curtailed.

31. Off-site pumping and monitoring wells were drilled on December 4, 1976, and designated MP and MO, respectively. The location of these wells, situated north of the site to minimize any effect on the Harbor River, is shown in Figure 3. Construction and depth of the wells, as well as the lithology in which the well screens were placed, are depicted in Figure 9.

32. The off-site pumping test was conducted on August 4, 1977; results are illustrated in Figures 10 and 11. An average coefficient of transmissibility value of 10,490 gal/ft/day was calculated from the drawdown and recovery curves.

Geology

33. The geology of the Grand Haven site is presented in terms of both the regional and site-specific geology in order to present both the macrogeologic and microgeologic systems affecting the site.

Regional geology

34. Grand Haven lies within the geologic province known as the Michigan Geologic Basin, a synclinal depression filled with Paleozoic-aged sediments. In the general area around Grand Haven, most of these sediments consist of lower Mississippian formations composed primarily of sandstone, shale and limestone.¹⁰

35. Figure 12 illustrates the relation of these series to others in western Michigan. The glacial drift deposits are primarily clays, silts, sands, and gravels, extending to a depth of 60 to 274 m (200 to 900 ft). The Marshall formation (sandstone,

siltstone, and shale) which underlies these glacial deposits is the major bedrock in the Grand Haven area.¹¹ In many parts of Michigan this formation provides a major source of water from the fractured sandstone horizons.¹²

Site geology

36. Site geology is typical of the glacial deposits in this part of Michigan. In all the on- and off-site borings, indigenous soils of fine sand were contiguous to a depth of 6 m (20 ft) where a dense clay stratum was encountered.

37. On November 4, 1976, this layer of clay was identified in a resistivity survey using a Wenner spacing configuration. Figure 13 shows the location of the survey profile north of the site (R1 to R).

38. The soil column for the Grand Haven area (Figure 13) shows a typical sequence of fine to coarse sands over the clays. The clay layer is reportedly several hundred feet thick, as derived from nearby well logs and on-site boxing logs (Appendix B). The fence diagram in Figure 14 was constructed from on- and off-site well logs and illustrates the uniform clay layer under the site.

Sayreville, New Jersey

Site Description

39. The physical setting at Sayreville, New Jersey, is listed in Table 4 and indicates its potential for study in a salt marsh area with pronounced tidal effects.

40. The dredged material disposal facility near Sayreville, New Jersey, is located in the eastern part of the state on the southern banks of the Raritan River, which empties into the Atlantic Ocean several miles to the east. Raritan Bay is approximately 1.6 km (1 mile) downstream from the site (see Figure 15). The disposal site is located at the head of a small peninsuls bordered by the river.

41. Relief in the immediate vicinity of the site is fairly level; the site itself is an approximately 17-ha (44-acre) slightly elevated diked area with a roughly rectangular configuration. The north side of the site (513.7 m or 560 yd) is bordered by the Raritan River, the west side (596.3 m or 650 yd) by U.S. 9, the east side (348.6 m or 380 yd) by New Jersey Highway 35, and the south side

(435.7 m or 475 yd) by a vacant lot adjacent to Amboy's Drive-In Theatre.

42. The dike that encloses the site is an earthen embankment approximately 5.1 m (17 ft) high. The outer dimension on November 28, 1976 was 8.2 m (27 ft) from the surrounding land to the top of the berm, while the distance from the top of the berm to the dredged material within was 3.0 m (10 ft) on the same date. Depth of the dredged material fluctuated between 6.0 m (20 ft) and 7.6 m (25 ft), as determined by on-site borings on November 2 and 3, 1976 (Figure 16). The material within the enclosure is fairly level, interrupted only by a small baffle dike (Figure 17).

43. Berm height has been increased throughout the life of the site, most recently in April 1977. There have been intermittent dredge and fill operations, as well as additions to the dike.

44. The Sayreville, New Jersey, disposal site is owned by National Lead Industries. Their titanium oxide plant, which operates the site and three other disposal lagoons in the general vicinity, is located approximately 0.8 km (½ mile) east of the site: two of the disposal ponds are west of the site (see Figure 16).

45. Before filling, the land was a salt marsh; remnants of these wetlands are still visible to the east and southeast. The phreatophyte Phragmites communis is the major flora species in the marsh.¹³

46. The lowlands east of the case study site are inundated daily by the 1.5 m (5.0 ft) mean tidal range of the Raritan River, although the disposal area itself is free from this tidal inundation as well as from flooding.¹⁴⁻¹⁶

Hydrological Features

47. The hydrological system at Sayreville, New Jersey was characterized via a series of site investigations using data from field investigations in conjunction with hydrological information gathered during the background literature search. Table 5 lists the dates of the various field investigations and the specific hydrological tests.

48. The results of these investigations are categorized in terms of three subject areas:

a. Climatological environment.

b. Surface waters.

c. Groundwater.

These sources provided information that accurately defined the nature of each of the components at Sayreville, New Jersey.

Climatology

49. Historical climatological data for the region was obtained from the weather station at Newark Airport (approximately 32 km (20 miles), north of Sayreville (see Table 6). Precipitation, temperature, relative humidity, and mean hourly wind speed were recorded: data are based upon a 36-yr period, from 1931 to 1966.⁸ A more detailed day-by-day record of the same elements is included in Appendix C; the dates of the field visits are indicated by brackets.

Surface water

50. Surface waters are a major influence upon the hydrological system at Sayreville. Because of the large artificially impermeable area (e.g., asphalt paving at the nearby theater, roads, etc.), the majority of the average annual 115 cm (45 in) precipitation in the immediate vicinity is channeled into drainage ditches that direct the surface runoff directly into the Raritan River or into the nearby salt marsh east of the site (Figure 16).

51. Surface water within the diked area of the site flows from south to north forming shallow ponds in the lower areas and finally draining through either of the 2 cm (18 in) discharge pipes (Figure 17). This phenomenon was observed during field investigations on November 4 and 28, 1976. The position of the effluent pipes implies that the on-site surface water drainage pattern has been constant throughout the history of the site.

52. The Raritan River has a pronounced effect upon the hydrological system of the Sayreville, New Jersey, site. According to tide tables published by the U. S. Department of Commerce, the mean tidal range in the vicinity of the site is 1.5 m (5 ft). This surging of waters through the salt marsh reverses the normal hydraulic gradient through the wetlands in the immediate vicinity of the river.

53. In order to determine the impact of the tide upon ground-

water flow patterns, three 3.1 cm (1/8 in) diameter metal well points (NJ3, NJ7, and NJ6) were installed in a triangle around the site and surveyed to relative elevations. Measurements from these wells provided the field team with the necessary information for a gross understanding of the groundwater flow patterns. Seven additional well points were driven into the shallow groundwater on- and off-site to further define these patterns (Figure 17).

54. Well points installed on November 2, 1976, along the northern rim of the site (NJ3, NJ4, NJ5, NJ6, NJ7) were specifically located to quantify the tidal effect. The top of the well points and subsequent monitoring devices were surveyed by SCS personnel from Reston, Virginia, to provide the field team with relative measurements for developing isopotential water level maps. All surveying was accomplished within a second order of traverse. Also, three bench marks were located on-site to assist the surveying during subsequent field visits to the monitoring/sampling wells.

55. On November 11, 1976, a series of water level measurements from this well point network were obtained over the course of 5 hr. Groundwater contour maps were then constructed to determine the effect of tidal inundations upon groundwater flow patterns. None of the on-site wells were dramatically affected by the tidal cycle; the extent to which water levels in the off-site wells were affected was directly related to the wells proximity to the Raritan River. Interference by winds that could have disrupted the tidal range was not a factor during the measurements recorded on November 11, 1976.¹⁵

56. Figures 18 through 23 illustrate the changing configuration of the water level contours developed from measurements obtained on November 11, 1976. Analysis of these contours provided the field team with the data necessary to determine the optimum location of the monitoring/sampling wells and pumping wells.

Groundwater

57. Groundwater flow patterns at the Sayreville case study site were determined by:

- a. Visual investigation of surface features.
- b. Water level readings from the network of

well points;

C. An off-site pumping test.

The following discussion on groundwater is a result of the field findings from these investigations.

58. On November 2 and 28, 1976, an intensive inspection of the Sayreville case study site determined the surface features which were, perhaps, indicative of subsurface groundwater contours. The drainage ditches, marsh areas, baffle dikes, and other features noted are illustrated in Figure 17. Water was observed seeping through the earthen dam into the surrounding marsh and/or drainage ditches, as illustrated in Figure 24. The cross-sectional area, labeled A₁-1 may be seen on the eastern segment of the site in Figure 24.

59. Leakage from the site was observed along the entire length of the dike, providing the first indication that the fill acted as an effluent or recharge source to the surrounding groundwaters. Later, data from the on-site wells demonstrated that this seepage corresponded to water levels within the fill.

60. There were phreatophytes adjacent to the fill and surface manifestations of groundwater seepage near the Raritan River. Structures that could possibly impede the flow of groundwater, road embankments, bridge foundations, etc. were studied and noted. This preliminary field survey provided manifestations of possible groundwater characteristics.

61. A network of 10 metal well points installed on November 2, 1976, and 10 monitoring/sampling wells installed November 28, 1976, provided a comprehensive monitoring network for identifying the groundwater flow patterns both on-site and in the immediate vicinity. A series of four water level readings were recorded during field monitoring visits to the site. The results of these measurements are depicted in the water level contour maps (Figures 25 through 28) for each of the four sampling periods. These readings were obtained on November 28, 1976; and April 6, June 2, and August 3, 1977. Measurements were also obtained on November 2, 1976, but could not be used to construct a contour map, since water levels had not stabilized sufficiently for representative

readings. This condition was due primarily to the low-yielding characteristics of the clays.

62. The on-site contours of 31.5 m (105 ft) in Figures 27 and 28 were the result of the complete ponding of the site from recent dredging. The standing water level was compared to known elevations of wells within the site in order to provide an approximate contour gradient value.

63. The water level contours indicated that groundwater patterns in the area were directly controlled by the dewatering at the disposal site; this recharge source is illustrated in the streamlines on each contour map which depict a generally radial flow from the site which was consistent throughout the project.

Pumping test

64. The third segment of the hydrological investigation, the pumping test, was designed to provide information concerning the shallow groundwater system and data on pumping time versus constituent concentration during pumping. Locations for the wells were based upon the extent of the tidal influence upon the groundwater. ¹⁷

65. Well construction, distances, and depths of both on- and off-site pumping and monitoring wells are illustrated in Figures 29 and 30. Efforts to perform a pumping test on-site were unsuccessful, because both the well and pump became clogged with dredged material. The results of the off-site pumping performed on August 4, 1977, are depicted in Figures 31 and 32. Using drawdown and recovery curves, an average coefficient of transmissibility value of 8264 R/m/day (7,161 gal/ft/day) was calculated.

Geology

66. Geological characteristics of the Sayreville site are presented in terms of the regional geologic regime and site-specific geology. Regional geology will be presented first, so an understanding the the geology of the site in relation to the general area may be understood.

Regional geology

67. The Sayreville site is in Middlesex County, New Jersey, which lies in two physiographic provinces, the Coastal Plain and Piedmont. The site itself is located within the Coastal Plain

Province and is characterized by unconsolidated sands, clays, and marls of Cretaceous age, with low-angle dips to the southeast. Sediments in the eastern segment of Middlesex County in the general vicinity of the site include nonconformities between the Upper Triassic Newark Group (predominantly shales and sandstone with interbedded volcanics) and the upper Cretaceous Raritan River formation, composed predominantly of unconsolidated sands, clays and greensand marls.¹⁸ In several areas, the Pensauken Formation of Quaternary age is visible, capping the hills south of the site and exposed in the river valleys. Where the Raritan River has cut through the river valley, a formation of alluvium has been deposited by the meandering river (see Figure 33).

Site geology

68. Site-specific geology follows the general pattern for the regional geology of river valleys. The case study site is in an area of river deposition at the mouth of Raritan Bay. Indigenous soils are derived from the flooding of the Raritan River, as well as normal erosional deposits from the nearby hills. The resulting sequences, as depicted in the soil column in Figure 34, are a series of interbedded sands, silts and clays; the soil column was derived from boring logs compiled and indexed in Appendix D. These on- and off-site borings provided the basis for the fence diagram (Figure 35) that also illustrates the relation of the water levels to on- and off-site land. A stratum of clay encountered in NJP3 and NJP4 appeared to be a discontinuous lens.

69. No major surface or subsurface anomalies were seen in the alluvial materials. Lack of surface evidence, coupled with the geological literature, indicate that the general area is seismically inactive.¹⁸

Houston, Texas

Site Description

70. The dredged material disposal site near Houston, Texas, was chosen as a case study site because it is characteristic of a highly contaminated upland disposal area in a wet, humid environment. Also it represented an inland site, located about a mile (1.6 km) from the ship channel. Table 7 lists the physical characteristics identified at the start of the project and confirmed

at a field investigation' on November 2, 1976.

71. The Houston site, known as the Clinton Disposal Site, is owned and operated by the Galveston District, U.S. Army Corps of Engineers, and is located approximately 8 km (5 miles) east of Houston, Texas, between Galena Park and Pasadena. The land was formerly marshland (Figure 36). The 226 ha (560 acre) site is rectangular, approximately 1,295 m (4,250 ft) by 1,981 m (6,500 ft) and is roughly bisected by Mercury Road which links Galena Park to Pasadena (Figure 37). Surrounding land use is primarily urban, although there is some open land to the east.

72. The dike that encloses the site was constructed of indigenous materials by the Corps and varies from approximately 3.6 to 4.5 m (12 to 15 ft) in height, and 9.1 to 12 m (30 to 40 ft) in width at the base. Extensive additions were made to the levees in March 1967 when material was added to the outer base of the dike for erosion control.

73. Only the eastern half of the Clinton Disposal Site, approximately 111 ha (275 acres), was studied for this report; the total site was simply too large (226 ha or 560 acres).

74. The southeastern corner of the study area, approximately 4.6 to 6.0 m (15 to 20 ft) higher than the rest of the acreage, did not show the ponding visible elsewhere on visits on November 6 and December 7, 1976. As determined from on-site borings, the depth of the dredged material in this section ranged from 6 to 7.6 m (20 to 25 ft). Figure 38 shows the location of the ten corings, labeled monitoring devices (HA - HJ), as well as the two wells (ONPW and ONOW) drilled for the on-site pumping test.

Hydrological Features

75. Background information pertaining to both regional and site-specific hydrological features was solicited to augment the data collected from the specific hydrological studies performed as listed in Table 8. The total hydrological system at the Clinton Disposal Site is described in terms of:

- a. Climatological environment.
- b. Surface waters.
- c. Groundwater characterization.

Climatology

76. Historical climatological data for the region was obtained from the weather station at the Galveston Post Office, approximately 40 km (25 miles) south of the site (Table 9). Precipitation, temperature, relative humidity, and mean hourly wind speed were recorded at this station for a 36-yr period, 1931 to 1966.⁸ A more detailed day-by-day record of precipitation and temperature may be found in Appendix E; the dates upon which the field visits took place are indicated by brackets.

Surface water

77. Surface waters in the vicinity of the site drain through creeks and drainage channels to the Houston Ship Channel, approximately 3.2 km (2 miles) to the south. The drainage ditch north of the site also empties into this channel (Figure 37).

78. On-site surface drainage from precipitation and dewatering flows to the northern portion of the site due to normal topographic gradients, and subsequently collects in a pond as observed during sampling visits. The ponded water flows through a 1.3-m (4½ ft) pipe into a drainage ditch, which empties into Hunting Creek 0.8 km (0.5 mile) east of the site and then into the Houston Ship Channel (Figure 37).

79. The Houston Ship Channel is the nearest large body of surface water. Its distance from the site and the subsurface nature of the soils preclude any tidal interference with the on-site groundwater.

Groundwater

80. The groundwater characteristics of the Clinton Disposal Site were determined through:

- a. Visual investigation of surface features.
- b. Water level readings from the network of well points and monitoring wells.
- c. On- and off-site pumping tests.

81. On the visits of November 6 and December 12, 1976, an effort was made to identify those surface features which would indicate groundwater characteristics. Both the drainage ditch and the dike along the northern perimeter of the site were studied.

Shallow borings on either side of the ditch indicated that the surface waters flowing eastward were perched upon impervious clays. Inspection of the dike at the northern border of the disposal area exhibited no seepage from the on-site ponded waters; exposed sections of the soil at road cuts and ditches around the site provided no evidence of springs or seepage. Other visible indications of near-to-surface groundwater such as phreatophytes (e.g., willows and salt cedar) were also studied.

82. Twelve 3.1-cm (1¼ in) diameter metal well points were installed on November 6, 1976, on- and off-site, to identify baseline groundwater flow patterns and thus provide a comprehensive shallow groundwater monitoring network; these wells, labeled H1 through H12, are shown in Figure 38.

83. Although the on-site wells intersected groundwater at relatively shallow depths (4.5 m, or 15 ft), all of the off-site wells were dry. Moreover, the compact nature of the native clays prevented the well points from being driven to a depth greater than 6 m (20 ft) at any location. As shown in Figure 38, the well points labeled H1, H8, and H9 were all located within 3.0 m (10 ft) of a drainage ditch. These wells, which were dry despite their proximity to the ditches, reinforced the earlier observation that the native clays provided an effective aquitard to surface infiltration from the drainage ditches.

84. Groundwater, assumed to be primarily from sediment disposal within the site and precipitation, was detected in each of the eight on-site well points, the first indication that groundwater artificially introduced within the fill system was separate from deeper native aquifers.

85. Water level contours were developed from measurements taken from the on-site wells and monitoring devices illustrated in Figure 38. The contours followed the general topographical gradients within the site; the areas of highest hydraulic gradient corresponded to the vicinity where the dredged material was pumped onto the site, further suggesting that on-site contours are artificially produced as a result of disposal operations.

86. Water level contour maps constructed from readings

obtained on the dates listed in Table 8 are depicted in Figures 39 through 43.

87. Subsequent drilling on- and off-site suggested that on-site groundwater was indeed independent of off-site systems. Water levels in on-site versus off-site wells and the results of the pumping test reinforced this conclusion.

88. The dense clays underlying the dredged material, as observed in the on-site pumping and observation wells (ONPW and ONOW, respectively), would act as an effective impermeable barrier and prevent large amounts of on-site water from infiltrating to the regional groundwater. It was not within the scope of this study to determine if such clays underlaid the entire Clinton Disposal Site.

Pumping test

89. Wells for pumping tests were installed on- and off-site. The previously mentioned on-site wells (ONPW and ONOP in Figure 38) were drilled 10.6 m (35 ft) deep, with a 3.0 m (10 ft) well screen (Figure 44). Off-site pumping and monitoring wells, similarly labeled OFPW and OFMW, were drilled to a depth of 10.6 m (35 ft) where a thick layer of sand under artesian pressure was encountered. A piezometric head of 3.0 m (10 ft) was measured. Figure 45 illustrates the construction of these wells, as well as the lithology of the area in which they were placed.

90. When a second off-site pumping well (OPFW2) was installed north of the site, a thin stratum of water-bearing sandy clays was encountered at a depth of 9.7 to 12.1 m (32 to 40 ft).

91. An on-site pumping test failed, because the pump and hose clogged with dredged material; efforts on December 6, 1976, and March 25, 1977, were both unsuccessful.

92. A pumping test using off-site wells ONPW and ONOP was performed on December 7, 1976. Although the water in the wells was subject to artesian pressure, dewatering took place after only a few seconds of pumping at 151 l (40 gal) per minute. The time delay required for the well to become recharged, along with the rapid dewatering of the well, resulted in inadequate data. Similar results were obtained when a pumping test in well OFPW2 was attempted, suggesting that the water-yielding sands encountered

by both off-site wells represented isolated lenses of permeable deposits, rather than parts of a continuous aquifer. Well logs from nearby city wells suggested that no major aquifer existed for several hundred feet below ground surface.¹⁹

Geology

93. Geologic characteristics of the Clinton Disposal Site are presented in terms of regional and site-specific geology.

Regional geology

94. The Clinton Disposal Site is located in a sector of southeastern Texas, which is part of the Gulf Coast geosyncline. This area is typified by reworked sediments which were deposited in the lowland areas. At depths of several thousand feet, the Beaumont and Lissie Formations, primarily shales and sandstones, are the predominant bedrock formations.²⁰ The geologic map for this area (Figure 46) shows the area to have sediments of Quarternary age including both the Beaumont and Lissie Formations.

Site geology

95. The geological setting at the site is similar to the general pattern of predominantly clayey sediments, which characterize this Gulf Coast geology. Soils encountered during off-site borings were essentially tight clays with some sands. Figure 47 shows a generalized soil column for the native soils at the site. This soil column was derived from background data and corings performed by the field team. Boring logs included in Appendix F were used to construct the fence diagram (Figure 48).

96. Boring logs from water wells drilled for the nearby city of Galena Park, approximately 91 m (100 yd) south of the site, indicate that with depth, shale of either the Beaumont or Lissie Formations becomes predominant. This is consistent with the general Gulf Coast morphology information gathered during the literature search for this area.

97. Information from the Gulf Coast Subsidence District and USGS personnel investigating faulting in the region indicate that no faults appear to lie under the site (personal communication, 8 November 1976, Ed Wagoner, General Manager, Galveston, Coastal

Subsidence District). Moreover, the field team saw no signs of seismic activity in the area of the Clinton Disposal Site.

Pinto Island, Alabama

Site description

98. The dredged material disposal site on Pinto Island, Alabama (adjacent to Mobile Bay), was selected because it complemented the previously selected locations. It represented an island hydrologic environment, which was subjected to the disposal of estuarine dredged material. Site characteristics are given in Table 10.

99. The 26.3 ha (65 acres) Pinto Island site is located west of Mobile, Alabama at the upper terminus of Mobile Bay. A small isthmus at the northern end of the island connects it to Blakeley Island which, in turn, is connected to Mobile. Figure 49 shows Pinto Island in relation to Mobile, as well as the location of Mobile in Alabama.

100. The dredged material disposal site at Pinto Island lies in an area which was formerly tidal marshland. The surrounding area on the island exhibits little relief, with the highest point on the island only 4.5 to 6.0 m (15 to 20 ft) above the surrounding waters of Mobile Bay. The rectangular site consists of 26.3 ha (65 acres) of enclosed land which has been used for disposal of dredged material from Mobile Bay (Figure 49). The site is surrounded on three sides by an earthen dike; the natural difference in elevation on the east makes a berm unnecessary in this section. Berm height, as measured on January 17, 1977, was approximately 2.7 m (9 ft) above the level of the dredged material. Dredging at the site during March 1977 made the dredged material nearly level with the dike in most areas.

101. Depth of the dredged material as measured by a series of on-site corings on January 17, 1977, ranged from 4.5 to 5.1 m (15 to 17 ft). Figure 50 shows the location of these corings, labeled "monitoring wells".

Hydrological features

102. Hydrological investigations at the Pinto Island disposal site were conducted on the days listed in Table 11. Specific

hydrologic tests were performed to complement or substantiate previously gathered background information. Table 11 also summarizes the prominent physical and climatological anomalies observed during each of the visits.

103. The results of these investigations were categorized into three subject areas, which, when combined, characterize the hydrological system at the Pinto Island disposal site. They are:

- a. Climatological environment.
- b. Surface waters.
- c. Groundwater characterization

The field testings listed in Table 11 were specifically designed to develop the information required for defining these components.

Climatology

104. Historical meteorological data for the Pinto Island dredged material disposal site, based upon a 30-yr average, 1931 to 1960, are tabulated in Table 12. Precipitation, temperature, relative humidity and mean hourly wind speeds were recorded at Bates Field, approximately 24 km (15 mi) west of the site. A more detailed day-by-day record of precipitation and temperature was also collected at Bates Field. This information is included in Appendix G; the dates of field visits are indicated in brackets.

Surface water

105. Surface runoff on Pinto Island drains into Mobile Bay through several drainage ditches; one located west of the site empties into the bay at the southern tip of the island (Figure 50).

106. On-site drainage from precipitation and dewatering at the disposal site flows to the eastern portion of the site under normal hydraulic gradient and, subsequently, ponds as observed during the four site visits: ponded water drains through a 0.7 m (2½ ft) pipe at the southeastern corner of the site near the well into Mobile Bay (Figure 50).

107. The effect of the tidal fluctuations of Mobile Bay on surface and groundwater gradients at the site were investigated. The mean tidal range of 0.33 to 0.45 m (1.1 to 1.5 ft) in Mobile Bay exerted no measurable influence upon the monitoring wells installed at the site.¹⁵ Water level readings in all the wells

throughout several tidal cycles were measured during field investigations on November 14, 1976, and June 8, 1977; no discernible differences in static water levels were observed during either of these visits, which corresponded roughly to the differences between the summer and winter tidal cycles.

Groundwater

108. Groundwater at the Pinto Island site was characterized through an analysis of the site involving:

- a. Visual investigation of the surface features.
- b. Water level readings from the network of well points and monitoring wells.
- c. On- and off-site pumping tests.

109. A visit to the site on January 13, 1977, identified those surface features which could indicate groundwater characteristics. The drainage ditch west of the site was of special interest, since the shallow groundwater emptied into it, demonstrating that the ditch acted as an effluent system. A survey of phreatophytes on-site and adjacent to the fill was also made. The dominant off-site herbs indentified included Pluchea purpurascens, Aster subulatus, and Panicum dichotomiflorum; Phragmites communis was the major on-site species.

110. To define groundwater flow patterns, a series of twelve 0.3 cm (1¼ in) diameter PVC well points were installed on- and off-site on January 14, 1977. A professional engineering company was subcontracted to survey absolute elevations of these wells to an accuracy of a second-order survey. Bench marks were established on- and off-site for future use. Once the wells were developed and water levels stabilized, static water measurements were recorded from each of the devices, and water level contours developed. Figures 51-54 illustrates the configuration of these contours, which indicate that the groundwater flows roughly in a radial configuration from the site to discharge points in Mobile Bay and the drainage ditch west of the site. Water level elevations, obtained on subsequent field visits to the site, are shown in Figures 51 through 54; as is apparent, basic streamline patterns remained constant.

Pumping test

111. The third segment of the hydrological investigation was a pumping test designed to provide information concerning the characteristics of the shallow groundwater system. Both on- and off-site pumping tests were originally planned. However, because on-site pumping tests were not successful at the other three sites (due to the properties of the dredged material), no on-site wells were placed at Pinto Island.

112. Off-site pumping test and monitoring wells were drilled on August 2, 1977; Figure 50 shows the location of these wells, designated OMW and ONW (off-site monitoring and off-site pumping wells, respectively). Well construction and the lithology in which the well screens were placed are depicted in Figure 55.

113. The off-site pumping test was performed on August 2, 1977; results are presented in Figures 56 and 57. A coefficient of transmissibility value of 13.67 l/m/day (11,843 gal/ft/day) was calculated by averaging the results of the pumping and recovery curves.

Geology

114. Geologic characteristics at the Pinto Island disposal site are presented in terms of both regional and site-specific geology.

Regional geology

115. The Pinto Island dredged material disposal site is located at the mouth of the Mobile River. Sediments in this part of the Gulf Coast are primarily recent deposits; those in the vicinity of Mobile are Holocene in age.¹⁰ The deposit of these reworked sediments is characteristic of the newly emerging geosynclinal area of the Gulf Coast region. Figure 58 is a portion of a geological map of the area and shows younger sediments characteristic of this portion of the Gulf Coast delta.

Site geology

116. The geological environment at Pinto Island is identical to that of many of the nearby small sand islands in Mobile Bay. Borings performed to shallow depths, 3.0 m (10 ft) by hand augering, and off-site borings in excess of 6.0 m (20 ft) displayed primarily

sand horizons along with some sandy silts and clays. Figure 59 is a typical soil column developed from the well logs and visual inspection of exposed profiles along the banks of the drainage ditch to the west of the site. On- and off-site borings, recorded during the installation of the monitoring devices are included in Appendix H. These borings provided the subsurface information needed for construction of the fence diagram (Figure 60) which shows the nature of the geologic setting.

117. There have been no domestic water wells installed on Pinto Island, and discussion with operators of several industries on the island revealed that no wells have ever been drilled, since the domestic and industrial water supplies are piped from Mobile onto the island.

118. Test wells drilled to 15 m (50 ft) for foundation studies for Alabama Dry Docks revealed brackish water in sands and silts with poor water-yielding characteristics (personal communication, 1 August 1977, Henry Seawell, geophysicist, Vester J. Thompson Consulting Engineers, Mobile, Alabama)²¹ while well logs from Blakely Island, approximately 1.6 km (1 mile) north of Pinto Island revealed similar sequences of sand, silts and clays.

Shipping and Sampling Procedures

119. The primary goal of this section was to develop a comprehensive sampling and shipping system for dredged material, soil, and water samples so as to obtain representative samples from the field situation. The system had to be designed to prevent contamination from the sampling process itself as well as from chemical and microbiological conversions during the shipping of the samples from the field to the laboratory.

120. Pertinent systems were reviewed and evaluated by the project team; basic approaches were adapted to accommodate the variety of site-specific conditions. Soil/dredged material sampling devices, groundwater well installation and sampling methodologies, on-site testing apparatus, as well as sample preservation and shipping techniques were evaluated and adapted to the subject project.

121. The literature review assessed methodologies and products in terms of applicability to:

- a. Dredged material/soil sampling.
- b. Interstitial and groundwater sampling.
- c. Soil/dredged material, and groundwater sampling containers.
- d. Shipping procedures.
- e. Ease of well/lysimeter installation, use, and subsequent sampling.
- f. Adaptability of sampling methods in various environments.
- g. Reliability of sampling methods.
- h. Degree of maintenance required after installation.

122. Table 13 lists the five general categories for which methodologies were considered and the corresponding potential systems which were evaluated. The consulted references in Table 12 include knowledgeable individuals and reliable literature sources.

123. The data were categorized and assessed in terms of the previously-mentioned criteria; the resulting procedures selected are listed in Table 14. As is apparent in the table, existing systems were inadequate for this study. Deficiencies were primarily due to the potential for contamination (i.e., by trace metals) from the use of these devices. Specialized equipment or methodologies were, therefore, developed for the specific demands of the study.

124. A brief discussion of the rationale used for the selection of the shipping and sampling procedures listed in Table 14 follows; an explanation of equipment designed for use in those categories where present technologies were inadequate is included.

Sampling Devices and Procedures

Dredged material/soil sampling

125. The sampling of dredged materials at the four sites as well as of off-site soils at each location consisted of two steps:

- a. Hand coring to the desired depth.
- b. Collecting the sample.

Equipment and procedures had to be highly adaptable to a wide

range of site-specific conditions and had to function in materials possessing a wide range of physical properties and compositions.

126. A variety of devices were evaluated as potential methods for coring. Portability and ease of coring were major considerations. Dredged material stability, as well as access into the desired areas at each site, posed major problems for the utilization of heavy equipment, i.e., drilling rigs. The ability to interchange auger heads easily in a variety of dredged material was a major advantage. The bucket and posthold auger heads illustrated in Figure 61 were chosen to provide the widest range of coring capabilities; with extensions to the auger head, it would be possible to core to a depth of over 9.1 m (30 ft).

127. As indicated in Table 14, present techniques for collecting samples were inadequate. A method for collection of the dredged material was, therefore, developed by the SCS project team. The sampler configuration, designed for obtaining both dredged material and soil samples, is illustrated in Figure 62. It consisted of a 0.9 m (3 ft) section of ABS schedule-40 pipe, fitted with a metal trap valve at the bottom (A in Figure 62); the trap valve was coated with 1.5 to 2 mm (0.05 to 0.07 in) of abrasive resistant Teflon (rinsed in ultra-pure distilled water between samplings). The pipe was threaded at the opposite end from the trap valve (Figure 62). By connecting the pipe to 1.5 m (5 ft) plastic extension sections, lower depths could be reached.

128. The coring proceeded with hand augers. When a predetermined depth was reached, the sampler was placed in the hole. The desired dredged material or soil profile was forced into the sample tube by driving the sampler into the material, and the entire assemblage was withdrawn from the cored hole and capped at both ends with ABS-threaded caps (see B in Figure 62). Contacts between the sample tube threads and caps were waxed with melted paraffin to prevent possible leakage. The labeled tube was inserted into a 4 mm polyethylene sheath, further ensuring the integrity of the sample for shipping, and sealed with duct tape at both ends.

129. The sample tube had been appropriately labeled, on the side, listing site designation (code), depth from which the sample

was obtained, and samplin'g date. Another label defined the relationship of the core to the ground surface, i.e., which end of the sample tube was nearest to the surface.

130. The information on the label of the sample tube was recorded on a separate numbered list; the same number was placed upon the sample tube. This list acted as a "back-up" system in the event that the first label on the sample tube was damaged during shipment.

131. Deviations from sampling procedures. With only one relatively minor change, the above-mentioned sampling and shipping procedures were used in the field. At Pinto Island, Alabama, the soil and dredged material collection methods designed by scs were abandoned for a quicker collection approach which did not, however, compromise contamination for expediency; instead of the ABS sampler (Figure 62) employed at the other sites, soil and dredged material were collected with a posthole auger head coated with 1.5 to 2 mil of abrasive-resistant Teflon. The hole was cored to a depth from which a sample was to be taken with a bucket auger head; the head on the auger stem was then replaced with the Teflon-coated posthole auger and the samples collected and placed in a soil tube identical to those previously used. The tube was capped, sealed, and labeled in an identical fashion as on the other three sites.

132. The Teflon-coated posthole auger head was used only when a sample was to be obtained, and was rinsed with distilled water between samples. Several additional posthole auger heads were coated and used, when the Teflon coating on the auger head in use indicated that the metal head was soon to be exposed to the soil sample.

133. This collection method enabled two team members to collect the soil and dredged material samples, rather than the five or six required for the earlier method. No other segment of the soil/dredged material collection process was altered.

134. Field procedures. Specific field procedures were implemented at each of the four case study sites to facilitate sampling and to minimize sample contamination. While most of these field procedures dealt with equipment operations, those developed for

well/lysimeter placements involved more than equipment use.

135. Prior to placement of any subsurface sampling device within or outside of the disposal site, a preliminary coring was made near each selected installation area with the hand auger; depths of this coring fluctuated, depending upon the site and whether the hole was within or outside of the disposal area. This preliminary coring provided subsurface data which were useful in determining the exact depth at which each soil/dredged material sample was to be obtained, along with the corresponding placement of the sampling devices. A boring log was kept for each of these initial corings.

136. A second coring, to be used for collection of soil samples and sample device placement, was augered within approximately 1.5 m (5 ft) of the initial hole, to the depth to which soil sample and sampling device placement was to occur, based upon the subsurface data derived from the first coring. This field procedure, while time consuming, ensured that sample collection and sampling equipment installation would be at the optimum subsurface locations.

Interstitial and groundwater sampling

137. Interstitial water. A variety of devices for the collection of interstitial water was examined; review of the state-of-the-art systems (Table 14) indicated that a pressure vacuum lysimeter was most ideally suited to this task. Therefore, in areas where interstitial water samples were required, the pressure-vacuum soil water lysimeter illustrated in Figure 63 was installed.

138. The design for the pressure-vacuum lysimeter is based upon the same principle as that of the porous cup tensiometers routinely used by soil scientists for measuring soil water tension; it is intended to intercept gravitational water percolating through an unsaturated zone prior to reaching the zone of saturation. By placing the lysimeters at various depths in the unsaturated zone, profiles of the water quality can be obtained.

139. The lysimeters used for this study are based upon those developed by Parizek and Lane in 1970 at Pennsylvania State University, and consist of a two-bar entry valve porous ceramic cup attached to the end of a 0.9 m (3 ft) long and 4.8 cm (1.9 in) O.D. PVC pipe which is fitted with a rubber stopper at the opposite

end (Figure 63). Two holes are drilled in the stopper to accommodate two 0.6 cm ($\frac{1}{4}$ in) O.D. polyethylene tubes, one for the evacuation and pressurization of the lysimeter and the other for the collection of the water samples. The vacuum or pressure is applied by a hand-operated, two-way pump, resembling a bicycle pump (Figure 64); the portable pump eliminated the need for carrying bulky electrical equipment to each site. During the study, water was pumped to a head of over 6 m (20 ft).

140. Two lengths of 0.6 cm ($\frac{1}{4}$ in) O.D. polyethylene tubing were inserted into the holes in the rubber stopper attached to one end of the lysimeter, the length of tubing determined by the lysimeter depth in the augered hole. One tube, the vacuum-pressure, extended about 5 cm (2 in) below the stopper, while the other, the discharge tube, extended to within 1.2 cm (0.5 in) of the bottom of the ceramic cup. Prior to the sealing of the top of the lysimeter with paraffin, the discharge tube was coded with strips of identifying tape to distinguish it from the vacuum-pressure tube.

141. When more than one lysimeter was installed, bentonite plugs were placed at the top and bottom of the holes and between the lysimeters during backfilling. This helped to eliminate the entry of surface water and to prevent water from channeling to the sampling points by flowing down the polyethylene tubing. The porous ceramic cup in each lysimeter was surrounded by a slurry of wet, fine quartz sand which ensured hydrological continuity with the saturation zone. The final installation for a single lysimeter is depicted in the lower half of Figure 63.

142. After placement of the lysimeter, a vacuum was created through the use of the vacuum-pressure pump (Figure 64). One polyethylene tube was crimped by pinch clamp, while a negative pressure of 50 to 85 centibars (15 to 25 in of Hg) was drawn with the hand pump; the other tube was then clamped to maintain the vacuum within the lysimeter. This process is illustrated in Figure 65.

143. Water samples were obtained from the pressure-vacuum lysimeter by connecting one polyethylene tube to a collection bottle, and the other tube to the pressure port of the hand pump (Figure 66). The water collected in the lysimeter was forced out of the sampler and into 0.264 l (1 gal) collection bottle. The water

sample was in turn transferred from the collection bottle into four specially prepared sample bottles which were labeled and chilled prior to shipment in Styrofoam containers specially built to minimize microbiological activity. A more detailed discussion of these bottles and shipping procedures is contained in later sections.

144. Groundwater. Water samples had to be collected from various levels in the zone of saturation. Existing systems were reviewed (Table 13); PVC tubing threaded to a plastic well point proved the most advantageous. A 3 in. plastic well point, constructed of 40-gauge PVC pipe, was selected for collection of the samples (Figure 67). The well points were slotted with 0.25 mm (0.010 in) openings and threaded at one end.

145. Additional lengths of PVC pipe were glued to the well point creating any length desired for well construction. The well point and plastic casing were placed in the sample hole to the required depth. A gravel pack was backfilled the length of the well point to facilitate the movement of water to the well point without clogging. The size of the gravels used for the gravel pack varied, depending upon the subsurface soil conditions. Native soils were compacted over the gravel pack to either the ground surface or to a level at which another well point was to be placed within the same hole.

146. Each well point was developed with a hand pitcher pump attached to a length of 1.8 cm (0.75 in) PVC tubing which was inserted, below the water level, into the well. The pump was primed and pumped for 5 to 10 min.

147. Water samples were obtained from the well points by lowering a polyethylene tube into the well; one end of this tube was connected to a collection bottle in which a vacuum was applied with the previously mentioned hand pump (Figure 68). When a sufficient amount of water was obtained, it was transferred to four specially prepared sample bottles. By switching the input tubing to the pressure outlet on the pump, pressure was used to transfer the water from the collection bottle into the water sample bottles. The water was forced from the collection bottle through the sampling tube and into a sample container. To minimize the potential of

cross-contamination, the collection bottle and tubing were rinsed with ultra-pure water between sampling.

Containers for soil, dredged material, and water samples

148. The previously described sample tubes were also used as sample containers for the dredged material and soil; sample disturbance was minimized by eliminating the transferring of the samples into a second container. Analytical tests determined both the size and type of water sample bottle to be used. Table 15 lists the bottles selected and their respective sizes.

149. University of Southern California personnel determined the appropriate procedures for preparation of containers for water, dredged material, and soil samples (Table 16); the tests to be performed and the elimination of contamination potential were two of the criteria considered.

150. As mentioned above, pressure-vacuum lysimeters were selected to sample interstitial waters. Prior to placement in the ground, the lysimeters were cleansed through a series of acid soaks and rinses, described in Table 16 to reduce the contamination potential. Other equipment to reduce contamination is also listed in Table 16. To eliminate cross contamination, the devices used in the collection process for interstitial and groundwater were rinsed between samples; in the field, distilled water was used to rinse the equipment.

Shipping procedures

151. Shipping containers in which water, dredged material, and soil samples could be packed and transported safely to the University of Southern California were assessed. Review of containers used for past SCS projects involving cross-country sample shipping were studied. The final selections, listed in Table 14 (wooden boxes and plastic ice chests), appeared to provide the best means of protecting the samples during shipment considering the following primary concerns:

- a. Safety from breakage during handling.
- b. Insulative (temperature capacity of containers).

Pertinent criteria listed earlier were also considered.

152. Wooden boxes were constructed to accommodate the ABS tube

samples containing both soil and dredged materials. The boxes were made from 1.2 cm (0.5 in) plywood. Five sample tubes along with packed blue ice could be placed in each box. Water sample bottles were shipped in plastic ice chests, packed with either ice or blue ice. Shipping procedures were developed to guarantee that sample shipment was routed in the most expedient manner.

Sample Preparation

153. Upon receipt of dredged material/soil sample tubes, the samples were stored in a constant temperature-humidity environmental chamber at 4°C until sample preparation procedures were begun.

154. The sample tubes were opened at both ends and immediately emptied into a nitrogen-filled polyethylene bag where they were further purged with nitrogen gas to prevent oxidative processes from occurring. The bagged samples were then placed into a nitrogen-filled glove bag where they could be manipulated with relative ease. Within the glove bag, each sample was mixed and transferred into the following containers:

- a. One-litre plastic bottle with cap (for soil mechanics studies).
- b. Six 20-ml plastic containers with caps (one each for total organic carbon, pesticides, total acid-soluble sulfides, total Kjeldahl nitrogen, total metals, and total phosphorus analyses).
- c. One 250-ml polycarbonate centrifuge bottle with cap, 30 g (for water-soluble and ammonium acetate extractable phase).
- d. One 50-ml tared glass beaker, 10 g (for percent moisture content).

155. All transfers were conducted by using plastic or Teflon spatulas; at no time was the sample in contact with glass or metal. The above-listed containers were soaked in 5 percent acid solution for 24 hours then rinsed with double-distilled water before use. The sample containers were appropriately labeled as to site, depth, and experimental purpose and were kept in the environmental chamber. Details of each analysis are given in Appendix L.

156. Attempts to obtain interstitial water from the dredged material and soil samples by means of a hydraulic squeezer and centrifugation at 10,000 rpm for 1 hour were unsuccessful because of the low moisture content of most samples.

PART III: RESULTS AND DISCUSSION

Introduction

157. The four upland disposal sites chosen for this investigation included freshwater and saline environments. They represented a wide range of physical characteristics. The sizes of the sites varied from 2.4 to 111 hectares (6 to 275 acres). The depths of dredged material ranged from 5 to 35 ft. Native soil varied from sand to clay. The important physical characteristics of the sites are summarized in Table 17. Figure 69 presents the pattern of groundwater interaction with disposal sites.

158. Water samples were collected four times during a 9-month period. Sediments were collected during the first and last sampling period. It is imperative to mention here that disposal of dredged slurries occurred intermittently in three of the four monitored sites during the sampling periods.

159. It was not possible to collect enough water for all the analyses at all locations. Priorities for analysis were assigned as follows:

- a. Trace metals.
- b. Major metal ions.
- c. Mercury.
- d. Total organic carbon
- e. Chloride.
- f. Alkalinity.
- g. Sulfate.
- h. Phosphate.
1. Chlorinated pesticides.
- j. Oil and grease.

160. The sediments in the four monitored sites contained a wide range of industrial and domestic pollution. A total of 26 sampling devices were placed in each site. Figure 70 shows the general position of the samplers. Note that the relative depth and distance is not on scale. Twelve of the samplers were placed inside the disposal site, at four locations, three different

depths at each location. Four samplers were placed directly beneath the site at the same four locations. Eight samplers were placed downstream (groundwater flow) from the site, at four locations and two depths. The remaining two samplers were placed upstream (groundwater flow) from the site.

161. Ideally this would reveal the difference in water quality between the saturated and unsaturated zone, between the new and old dredged material, and also the soil attenuation effect directly below the site. The parameters measured varied among sites as well as within sites. Attempts were made to identify the time-dependent changes in water quality at different depths. Plots of concentrations versus depth, and concentration versus time failed to reveal any systematic changes. For any parameter, both increases and decreases in concentration occurred with time, and random distributions were observed in different locations of the same site. Similar trends were observed in the depth profiles.

162. Based on this observation samples collected from the four sampling periods were grouped broadly into:

- ✦ BG: Background samples. Samples collected from the background (upstream) wells.
- OS: On-site samples. All on-site samples (except those for the Houston site); four locations at three different depths at each site.
- MW: Monitoring well samples. All off-site (downstream) wells; four locations at two different depths at each site.

163. It is extremely difficult to single out a specific trend or mechanism for interpreting the results of this study. Instead, attempts were made to explore the general nature of the systems based on sample variations, i.e., mean and range, pooled from all samples analyzed. As will be explored in later sections, most of the mean values of on-site (OS) group are higher than the monitoring well (MW) and background (BG) group. This could be misleading because of the great variability existing in each site. Student's "t" test will be used to analyze the significance of these differences. The P values obtained are the probabilities of having the difference this large or larger by chance, i.e., lower P values

indicate that the differences are statistically more significant. For samples coming from two different populations, i.e., the two variances cannot be assumed to be equal (as indicated by the F test), the P values will be estimated by the special "t" test as outlined by Davis.⁶⁷

164. To reflect the groundwater condition, samples were grouped into:

- a. US: Under-site samples. These included samples collected with the four sampling devices placed directly below the site.
- b. GW: Groundwater samples from monitoring wells. Samples from the lower depth sampling devices (below groundwater table).

165. It was expected that the results would be site-specific since the release and migration of chemical constituents were expected to be affected by the hydrobiogeochemical conditions of the site. A general discussion of the results of the bulk analysis of dredged material/soil from each site, along with the significance of the parameters, is presented in the following section. Possible mechanisms regulating the transport of trace contaminants are briefly reviewed. The chemical properties of the water samples and the migration trends of the contaminants, with emphasis on groundwater quality, are also discussed in detail.

Characteristics of Dredged Material/Soil

Particle size distribution

166. The results of the particle size distribution analysis are given in Appendix I, Tables 11 to 14. The classification of sediment texture was based on the Corps of Engineers, "Triangular Classification Chart" shown in Figure 71.

167. Particle size distribution is an important property associated with confined disposal operations. Coarse-grained dredged material tends to settle rapidly within the site. Finer particles tend to be carried with the effluent to the receiving waters due to insufficient residence time or turbulence. A decrease in the relative sand portion in the effluent compared with influent was reported by Hoepfel et al.⁶⁸ and Lu et al.⁶⁹. This will, of course, be a function of the original sediment characteristics,

Size of site, and rate of dredged material disposal. Consequently, it is generally expected that the dredged material that settles in land disposal sites will be more sandy than the original bottom sediments. A horizontal stratification may also exist with finer particles settling more closely to the effluent weir. In this study, all but one sample contained more than 50 percent sand, with many made up of more than 90 percent sand.

168. Sayreville samples collected for this study were more varied than the Pinto Island samples. Textures ranged from sand to clay sand. The clay content averaged 20 percent for the on-site samples, and 24 percent for the native soil away from the site; both are the highest among the four sites.

169. The Houston site is an isolated aquifer system, separated from the regional aquifer by underlying native clay. All samples were collected within the site. A wide range in particle size distribution was observed (Table 13).

170. The Grand Haven on-site samples were not as uniform as the samples from the other three sites. Two of the on-site locations (MA and MB), which were much more clayey than the other two (MF and MG), were closer to the effluent weir. Two of the off-site samples showed that the top few feet of the surrounding soil is clay or silty sand followed in sequence by a layer of sand and clay, a typical aquifer profile.

171. Particle size distribution has a profound effect on the chemical properties of leachates produced. Finer particles provide a larger surface area per unit weight for sorption and exchange reactions. It is well-known that clay particles have a higher cation exchange capacity and a higher affinity for organic matter, trace metals, pesticides, and nutrients. In general, the finer soil textures provided for greater attenuation of trace contaminants.

Moisture equivalent, bulk density, hydraulic conductivity

172. The moisture equivalent reported in Tables I1 to I4 was determined in accordance with ASTM Designation D 425-69, "Standard Method of Test for Centrifuge Moisture Equivalent of Soils."⁷⁰ It should be noted that this procedure only approximates natural per-

colation, and it cannot be assumed that the centrifuge moisture equivalent represents the in situ field capacity.^{71,72} Many investigators^{71,72} have shown, however, that the moisture equivalent can be corrected with the actual field capacity for many soils.

173. The field capacity is defined as the smallest value to which the water content of a soil can be reduced by gravity.⁷³ In this study, the Sayreville site had the highest mean moisture equivalent followed by the Grand Haven, Houston, and Pinto Island sites (Table 17). This parallels the trend based on the relative clay contents.

174. Except for the Sayreville samples, most samples had moisture contents close to or exceeding the moisture equivalent values, suggesting a groundwater recharge situation. The conclusion was reinforced by field observations. At the time of sample collection, the surface of the Sayreville site was dry and cracked. Snow covered the Grand Haven site, a potential recharging condition. Four inches of rain was recorded at Pinto Island during the 2 weeks preceding the sampling. Part of the site was actually ponded. Light drizzle was reported at the Houston site. The moisture content was close to the moisture equivalent in the Houston site.

175. The bulk density (apparent density) is defined as the weight per unit volume of a material, including voids inherent in the material as tested. This is an important parameter because the void spaces are the pathways in which the solute will travel. The result of the bulk density analysis are given in Table 11 to 14.

176. Hydraulic conductivity is another parameter that may influence the flux of leachates. Hydraulic conductivity, also called the coefficient of permeability, has the unit of velocity, cm/sec, and reflects the rate of water flow. The significance of this lies in the fact that slow flow rates through the **dredged** material or soil provide longer reaction times for the interactions of solvent contaminants and the dredged material/soil particles.

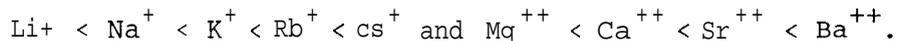
177. The laboratory measured values, obtained using the falling head method, are reported in Tables 11 to 14; the statistical analysis is given in Table 19. A wide range of values covering five orders of magnitude was observed. This is another indication of the heterogeneity of the sites.

Cation exchange capacity'

178. Ion exchange is a reversible chemical reaction that takes place between ions in a solution in contact with ions held near a mineral surface.⁷⁴ The total capacity of the mineral to exchange cations is defined as the cation exchange capacity (CEC), and is usually expressed in meq/100 g dry weight soil.

179. Malcolm and Kennedy⁷⁵ attribute the range of CEC in soils to: (a) parental material (geology), (b) age of weathering surface, (c) climatic factors, (d) degree of weathering, and (e) completeness of chemical and physical dispersion. In simpler terms, the CEC is related to soil texture, type of clay mineral, organic matter content, pH, and the solid to solute ratio.⁷⁴⁻⁷⁶

180. Exchange is found to take place faster in fine sediments, and fine sediments have a relatively high CEC. Carroll⁷⁴ reported that, due to the difference in structure and chemical composition, clay minerals have exchange capacity ranges (in meq/100 g) in the order of halloysite (2 to 10) < kaolinite (3 to 15) < glauconite (11 to 20) < attapulgite (20 to 30) < illite (10 to 140) < montmorillonite (70 to 100) < vermiculite (100 to 150). The order of replaceability of the common ions found in clay minerals has been found to be:⁷³



181. Malcolm and Kennedy⁷⁵ reported a study that demonstrates the significant contribution of organic matter to the CEC of certain size fractions of sediments. The CEC of sand and gravel fractions were found to range from 7 to 16 meq/100 g; 17.6 meq/100 g for the fine silt fraction, and 53.6 meq/100 g for the fine clay fraction. Except for the silt fraction, after accounting for the organic matter, the CEC of the mineral portion was relatively constant at 5.5 to 8.0 meq/100 g.

182. Toth and Ott⁷⁶ reported that the organic matter content of bottom sediments is responsible for about 80 percent of the CEC. Their findings on river sediments, bay sediments, and freshwater impoundment sediments indicate that CEC values, which ranged from 7 to 100 meq/100 g, were much higher than those of soil, which ranged from 1 to 15 meq/100 g. They also reported that the order

of abundance of three exchangeable trace metals in the sediments was $Zn > Cu > Ni$. The quantity of exchangeable trace metals was highly correlated with the amount of organic matter present.

183. On studying the concentration of five elements in suspended materials in streams, Turekian and Scott⁷⁷ reported that, although the CEC of the total suspended load was higher for the Mississippi River and rivers to its west than those to the east, the concentrations of the elements were considerably lower and the composition resembled that of shale. They concluded that the difference was not due to the CEC but rather due to a greater amount of a mobile trace metal-rich soil component and to higher industrial discharge in the eastern rivers.

184. In this study, a wide range of cation exchange capacities was found (Table 19). In general, the mean values are expected to reflect relative texture of the samples. As stated before, Pinto Island samples were generally the most sandy, and they also had the lowest CEC, an average of 11 meq/100 g. The highest CEC was 51 meq/100 g. That particular sample contained 14 percent clay, more than most of the samples from the Pinto Island site.

185. Sayreville samples had the highest mean CEC of 55 meq/100 g and also the highest average clay content. Samples from Grand Haven and Houston were intermediate, again showing the relations between CEC and particle size distribution. However, linear regression analysis showed that only Sayreville samples exhibited a high correlation between CEC and clay content ($R = 0.78$). This is probably due to the difference in TOC content and the difference in clay mineralogy.

pH and Eh

186. pH and Eh are very important factors in regulating the direction and extent of reactions in dredged material and soil. Eh is a measure of the availability of electrons or the electrochemical potential of the system (corrected on the hydrogen electrode). Oxidation and reduction reactions are defined as reactions that involve loss or gain of electrons. In general, oxidation should result in low pH values, and low pH values favor the migration of most trace elements. Redox reactions are

energy-requiring systems. In natural systems, the energy usually comes from the decomposition of organic materials. To complete the reaction, some substances must act as electron acceptors. The electron acceptors that exist in disposed dredged material include oxygen, nitrate, Mn(IV) oxides, Fe(III) oxides/hydroxide, sulfate, and carbon dioxide. The above are listed in order of their oxidizing potential. Reduction of carbon dioxide to methane, the last in the sequence, seldom occurs because most of the organic matter will be oxidized by the other acceptors listed.

188. The biological activities result in a changing supply of organic matter. Total redox equilibrium is not found in nature.⁷⁸⁻⁸² Therefore, the Eh measurements lack specific thermodynamic meaning. They only represent a gross sum of all the simultaneous redox pair reactions.^{79,83-85} However, Eh measurements will serve the function of indicating the general redox condition of the systems.

189. Patrick and Mahapatra classified soil (adjusted to a pH of 7) into four categories:⁸⁶

- a. Oxidized soil: Eh > +400 mV.
- b. Moderately oxidized soil: +400 to +100 mV.
- c. Reduced soil: +100 to -100 mV
- d. Highly reduced soil: -100mV to -300mV

190. Pearsvall and Mortimer⁸⁷ reported that products of oxidation (ferric, nitrate, sulfate) were found in soil, mud, and water with an Eh (at pH of 5) of +350 mV and that their reduced counterparts (ferrous, ammonia, sulfide) were present in zones below this value. They suggested that the mechanisms regulating redox potential in all three types of systems are similar in nature.

191. As a rough guide to the progress of reduction, Ponnamperna⁸⁸ compiled a list of critical potentials observed from stirred soil suspensions:

Observation	Eh (at pH of 7), mV
Oxygen (undetectable)	+330
Nitrate (undetectable)	+220
Manganese (detectable)	+200
Iron (detectable)	+120
Sulfate (undetectable)	-150

192. For this study, the Eh and pH were measured by carefully sticking a platinum and glass electrode into freshly exposed dredged material or soil. The results are presented in Tables 15 to 18. The Pinto Island pH ranged from 4.2 to 7.6, with most values close to 7. The on-site dredged material was slightly more acidic than the off-site soil (means of 6.5 and 7.0, respectively). The Eh ranged from -232 to +353 mV for the dredged material and -82 to +368 mV for the soils. Similar ranges of results were found for other sites.

193. The wide range of Eh and the relatively small range of pH measured were expected. Similar results for various sediments and soils have been extensively reported in the literature.^{5,87,89-92} Eh and pH are theoretically related:

$$Eh = E_0 = \frac{0.059}{n} \log \frac{[Ox]}{[Red]} - 0.059 \frac{m}{n} pH$$

where $\begin{cases} [Ox] = & \text{activity of oxidized species} \\ [Red] = & \text{activity of reduced species} \\ n = & \text{number of electrons involved} \\ m = & \text{number of protons involved} \end{cases}$

194. As mentioned before, Eh is expected to be related to the organic matter present. High TOC usually signifies low Eh levels. However, the Eh, pH, and TOC data indicate that this relationship does not always hold true.

195. During dredging operations, the sediment is mixed with the overlying oxygen-rich water. It is possible that the sediment-bound biostimulants will be affected and transformed. Upon disposal, some organic matter will be oxidized by biological activities. The Eh and pH should often show localized variations within site sediments, depending on the nature and amount of the organic matter present (e.g., its biological activities), oxygen diffusion rate,^{93,94} and the sediment buffering capacity. Eh and pH are the major variables that dictate the extent of most reactions. It was not surprising to find highly localized distribution of soluble species in this study.

Organic matter and other gross parameters

196. The main component of organic matter in sediments is usually humus, resulting mainly from the biodecomposition of lignins, cellulose, and proteins.^{93,94} Humus is primarily composed of highly insoluble complex macromolecules, and is believed to be firmly adsorbed onto clay minerals.^{95,96} Metal ions can form strong ionic or covalent bonds with humus by means of different functional groups (e.g., carbonyl, hydroxyl, amide and sulfhydryl bonding). These mechanisms appear to be partially responsible for the migration and accumulation of trace metals in soils^{97,98} and marine sediments.^{99,100}

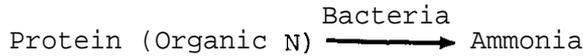
197. Nutrients can be released from the biodegradation of organic matter in the dredged material. Due to its complexity, it is impossible to determine the exact nature of the organic matter. A few general parameters were used to characterize its gross properties.

198. Total organic carbon. The average onsite dredged material TOC value ranged from a low of 0.27 percent for the Houston site to a high of 3.8 percent for the Grand Haven site. The Sayreville off-site soil TOC was slightly higher than the on-site dredged material (1.9 percent and 1.4 percent respectively). Both Pinto Island and Grand Haven had higher on-site values than the off-site values (0.97 percent and 0.53 percent for the Pinto Island site, 3.8 percent and 2.5 percent for the Grand Haven site).

199. Total organic carbon (TOC) in dredged material probably originates from the sedimentation of biological detritus. Few soluble organic compounds found in natural waters are thermodynamically stable.¹⁰¹ Decomposition of organic matter depletes the dissolved oxygen and reduces the Eh. In addition to its high cation exchange capacity, the organic matter in soil also possesses a high capacity to form insoluble complexes with metal ions. Therefore, high TOC in the sediment usually signifies a potential for the immobilization of trace metals through organic matter binding.

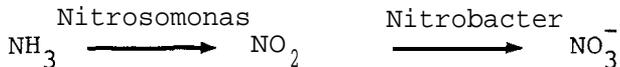
200. Nitrogen compounds. Ammonia and organic nitrogen are other nutrients which were measured in this study. The principal form of nitrogen added to sediments is organic nitrogen, with the bulk usually present as biologically protected protein frag-

ments. Ammonia is most often formed from the decomposition of protein (deamination) by saprophytic bacteria: ¹⁰²



This process is known to take place with or without oxygen, ⁵ but is much faster under aerobic conditions because the more active aerobic bacteria decompose organic matter at an accelerated rate. However, net release of ammonia is greater in anaerobic conditions due to slower biological uptake. ⁹⁰ Ammonia thus tends to accumulate under anaerobic conditions. Accumulation of ammonia in anaerobic lake sediments was observed by Austin and Lee ¹⁰³ and high ammonia content in deep sea interstitial waters was reported in several studies. ^{104,105}

201. When oxygen is present, ammonia is further converted into nitrite and nitrate, mainly by aerobic nitrifying bacteria. The dominant pathway is as follows: ¹⁰²



202. The TKN data are given in Appendix H. The statistics are summarized in Table 19. The average on-site value ranged from a low of 269 mg/kg for the Pinto Island samples to a high of 3170 mg/kg for the Sayreville samples. While there is little leaching of organic nitrogen, dredged material may serve as a nitrogen source for groundwater because of the soluble end-products (ammonia or nitrate) resulting from the biological activities.

203. Phosphorus compounds. Phosphorus exists in sediment and soil in the inorganic and organic form, and in valence state from +5 to -3. The main transformation of phosphorus is the release and mobility of the orthophosphate ion. ⁷¹ Chang and Jackson ¹⁰⁶ classified the inorganic phosphate in the soil into four main groups: calcium phosphate, aluminum phosphate, iron phosphate, and reductant-soluble phosphate, extractable after the removal of the first three forms. ¹⁰⁷ The possibility of the formation of aluminum phosphate minerals (wavellite and variscite) and iron minerals (vivianite and dufrenite) in acid soils has been demonstrated by Stelly and Pierre. ⁻¹⁰⁸ Calcium phosphates exist

mainly as apatite, anapaite, and bushite. ^{78,108}

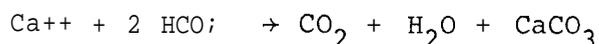
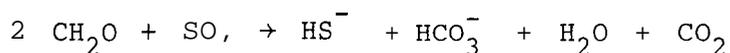
204. The total phosphorus data are given in Tables 15 to 18. Dredged material from the Grand Haven site had a high total phosphorus content (average of 1700 mg/kg) followed by Sayreville (1490 mg/kg), Pinto Island (1360 mg/kg) and Houston (1280 mg/kg). The Sayreville soil samples were as high as the dredged material (Table 19). Pinto Island and Grand Haven soil samples contained considerably less total phosphorus.

205. The transformation of the stable solids is greatly affected by Eh and pH. Phosphate associates mainly with iron and aluminum in acid soils and sediments; calcium phosphate is predominant in neutral and alkaline soils. ^{98,106} The importance of this in regulating phosphate transport will be explored in greater detail when discussing the results of the soluble phosphate in leachates.

206. Oil and Grease. The average oil and grease content at the Sayreville site was higher in the surrounding soil than in the on-site sediments, even though on-site averages are higher than those at the Pinto Island and Grand Haven sites. This is similar to the relative distribution of TOC in these sites. The exact reason for this cannot be assessed by this study. The Sayreville site is bordered by two heavily used highways. It is possible that the exhaust and emission from automobiles may have contributed to the observed result. An oil and grease extract can include a great variety of organic compounds besides petroleum derivatives. Materials which are extractable with petroleum ether include glycerides, high molecular weight fatty acids, gasoline, oils, waxes and other hydrocarbons. Petroleum compounds constitute the greatest proportion in sediments from industrialized areas. High oil and grease in the sediment thus usually indicates industrial pollution. ¹⁰⁹ However, there is essentially no information available on the relationship between such residues and degradation of water quality. ^{109,110} The average oil and grease value for each site is given in Table 19.

207. Sulfides. The acid-soluble sulfide measured in this study included hydrogen sulfide and certain metallic sulfides. The

main source of sulfide in 'sediment interstitial waters is dissolved sulfate. Thermodynamic calculations indicate that sulfate is unstable in the presence of abundant organic matter and absence of oxygen.¹¹¹ However, the reduction of sulfate to sulfide in natural systems is known to occur only through biological mediation.¹¹² The bacteria that carry out this reaction are grouped together under the common name "sulfate reducers." The most widely distributed species belong to the Desulfovibrio genus.^{112,113} Their metabolic activities have profound consequences. The end result of the reduction reaction, as illustrated by the following general equation, include metal sulfide precipitation, increase in alkalinity, carbonate precipitation, Eh and pH modification.^{112,114-117}



208. The production of CO_2 can lower the pH, and the free sulfide produced will combine with the available metallic ion (M^{++}) to form stable solids.

209. Acid-soluble sulfide was detected in all samples. The value generally correlated with the TOC and Eh. The highest value was 2357 mg/kg, found in an off-site Sayreville sample. That sample also had a relatively high TOC (1.7 percent) and low Eh (-168 mV). The lowest value from that site was 23 mg/kg, with a TOC value of 0.02 percent and an Eh value of 408 mV.

210. The availability (or mobility) of trace metals in soil were usually directly related to the solubility products of the metallic sulfides.¹¹⁸



The existence of sulfide in the dredged material/soil samples indicated that sulfides could be the controlling solids for most trace metals. Due to the low solubility of metallic sulfides, the metals are expected to be immobilized.¹¹⁸

Chlorinated hydrocarbons'

211. The chlorinated hydrocarbons measured include three forms of PCB's (Aroclor 1242, 1254, 1260) chlorinated pesticides: op' and pp' isomers of DDT and its analogs DDE and DDD; and dieldrin. Attempts were made to determine the concentrations in the soluble and solid phases. After forty filtered samples from different sites and depths showed no detectable soluble species, no further analyses were made on water samples.

212. Adsorption onto clay and organic matter may explain the fact that no soluble species were detected in this study. Chlorinated hydrocarbons are very hydrophobic. They tend to come out of solution easily and be adsorbed to solid surfaces available to them.^{119,120} Most chlorinated hydrocarbons in the environment are adsorbed onto the soil and sediment particles. The transport of these species is regulated to a large extent by adsorption and transport with clay and organic matter.^{121,122} Leland et al.¹²³ reported that the chlorinated hydrocarbons were mostly concentrated in the upper 2 cm of the sediment. The clay-sized fraction has been shown to be able to adsorb much greater amounts of chlorinated hydrocarbons than sand because finer fractions usually contain both higher organic content and a larger surface area.¹²⁴

213. The complete results for the dredged material/soil samples are presented in Table J1 to J5; ranges, means, and standard deviations are given in Table 20. Most samples contained all the species studied. Total DDT ranged from below the detection limit to 850 ppb. The major form was op' and pp' DDE. A similar distribution in sediments was reported by Choi and Chen.¹¹⁹ Average total DDT (Table 20) was highest for the Sayreville site (96 ppb) followed by Pinto Island (78 ppb), Houston (67 ppb) and Grand Haven (44 ppb). Average total PCB's ranged from a high of 0.58 ppm for the Sayreville site to a low of 0.14 ppm for the Grand Haven site. Average dieldrin was found to be highest at Sayreville (2.3 ppb) followed by Grand Haven (1.2 ppb) and Houston and Pinto Island (both averaged 0.8 ppb) (Table 20).

214. The average total PCB values correlated very well with the average total DDT values ($R = 0.70$). Total PCB's correlate

fairly well with the percent clay content ($R = 0.44$). It was generally expected that soil TOC would correlate with the chlorinated hydrocarbons. This was not observed in this study.

215. In general, the dredged material contained higher chlorinated hydrocarbon levels than the off-site soil samples. No special trend was found for the distribution of the species in the on-site dredged material. For the off-site soil samples, concentrations of all species decreased with depth. This was observed in Pinto Island, Sayreville, and Grand Haven. For the Houston site, all samples collected were on-site dredged material, and no special trend was found. Since no soluble species were detected, it is concluded that chlorinated hydrocarbons will not leach out from dredged material disposal sites.

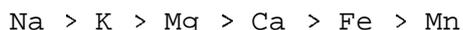
Trace metal analysis

216. Soil and dredged material samples were analyzed for trace metals in the soluble fraction, the exchangeable fraction, and the gross concentrations. This analysis was performed sequentially by shaking with water then ammonium acetate, and by digestion with strong acids. The detailed results are given in Table J5 to J8. Attempts to squeeze out interstitial water from these samples failed because of low moisture content.

217. In general, for each sample, iron was highest in the total analysis followed by the major ions, Na, K, Mg, and Ca. The concentrations of metals followed roughly the order:



218. In the soluble and exchangeable fractions, no particular concentration trends were found other than for manganese. The major ions in the soluble phase generally ranked:



in the soluble phase and



in the exchangeable phase.

219. No apparent relations were found in these soil analyses and the subsequent analyses of water samples. This result is not surprising since bulk analysis is not a good indicator for potential availability. Depending upon the chemical phase of the

species, metals may be totally unavailable (e.g., they may exist in the crystal structure of the soil particles) or readily available (in solution or adsorbed onto the particles).

220. Also, the results confirmed the highly dynamic, complex nature of the soil-dredged material system. The samples excavated from the sites may not represent the actual site conditions after elapsed time.

Characteristics of Leachates/Interstitial Waters

General considerations

221. The composition of the dredged material and interstitial water (leachate) at a disposal site is highly dependent on the dredging and disposal practice. The ambient water quality and the sediment characteristics play an important role because the dredged slurry is mainly composed of the water overlying the dredging site sediments.⁶⁸ The sediment-water ratio and time of contact affect the exchange of chemical species.¹²⁵⁻¹³⁰ Variation of sediment interstitial water composition with depth has been extensively reported.¹³¹⁻¹³⁵ Thus, depth of dredging is also an important factor.

222. Chemical constituents usually are enriched in the interstitial waters of sediments.¹³⁵⁻¹³⁸ Concentration gradients with depth have been observed, and the diffusion of ions along the gradient has been suggested as one of the mechanisms for the transport of the ions.¹³⁹⁻¹⁴² After dredging and disposal, this stratification is disrupted. Instead, an uneven distribution of high constituent concentrations could develop in the disposal site.

223. The size of the site and the quantity and frequency of dredging also affect the fate of pollutants. Recent reports on the influent/effluent studies of certain upland dredged material disposal sites have shown that larger ponded sites generally retain more polluted sediments.^{69,110,111,143} This characteristic is the result of the site providing longer settling times for removal of the finer particles. It is well-known that small particles have greater affinities for trace metals and organic

matter. 2,69,144,145

224. Another factor that influences the leachate composition is the repeated drying and wetting of site sediments due to evaporation, drainage, and precipitation.¹⁴⁶ In a literature review¹¹⁰ it was shown that drying of taconite tailings prior to a leaching test caused a release of copper from the tailings which did not occur if the tailings were maintained in their wet conditions prior to the leaching test.

225. Merz and Stone¹⁴⁷ pointed out that solid waste disposal sites are usually aerobic near the surface and become more anaerobic towards the bottom. However, within unsaturated zones, traces of oxygen are often present so that zones or pockets of anaerobic and aerobic decomposition may exist side by side at any depth.

226. Lu⁹⁴ and Lu and Chen¹⁴⁸ reported that sulfide is usually the controlling solid for most metals in the reducing environment and that oxides and hydroxides are the controlling solids in the oxidizing environment. The solubility of oxides and hydroxides is in general much higher than that of their sulfide counterparts. Thus, the oxidizing forms of most metals are generally more mobile than their reduced forms.

Factors affecting the migration
of constituents through dredged material and soil

227. If there were no attenuation or enrichment mechanisms, contaminants could tend to percolate from sediments under varying environmental conditions and eventually end up in the sea or remain totally unavailable. However, soil is a highly complex, dynamic system. Recent studies on leachates from sanitary landfills indicate that, due to certain properties of the soil, transport of contaminants can be retarded. Nonuniform environments in the ground can develop pockets of varying constituent mobilities.¹⁴⁹⁻¹⁵²

228. Soil and dredged material have very similar characteristics. The following is a list of factors that would affect the migration of constituents in soil and dredged material:¹⁵³⁻¹⁵⁶

- a. Soil texture.
- b. pH.
- c. Oxidation-reduction.

- d. Dilution.
- e. Ion exchange.
- f. Adsorption.
- g. Solubility/complexation.
- h. Diffusion.
- i. Biological effects.

229. Soil texture. The importance of soil texture, pH, Eh, and ion exchange was discussed in the previous section. Soil texture may play a governing role in the migration of trace contaminants. Many attenuation mechanisms involve solid surfaces. The finer the particle, the greater the available surface, and the greater the potential for attenuation by these mechanisms. Water flow may also be retarded in areas possessing high clay contents, thereby allowing greater reaction time between the soluble and solid phases.

230. Redox and pH. pH affects the stability of solid minerals and precipitates. Changes in redox conditions may change the controlling solids. In general, oxidation results in low pH, and reduction increases pH values. Migration of trace contaminants is usually favored in low-pH environments.

231. Dilution is a simple mechanism. Dilution can occur either from percolation of surface drainage and precipitation or from the contaminant reaching the groundwater table. This is the only important mechanism for the attenuation of chloride ions. ^{83,157} Dilution also plays an important role in regulating other major ion concentrations, especially sodium and potassium.

232. Sorption. Adsorption is a very important mechanism for the removal of many soluble metals. Krauskopf ¹⁵⁸ proposed that this is the possible control mechanism for regulating concentrations of Zn, Cu, Pb, Cd, Hg, Ag, and Mo in seawater. Clays, soil organic matter, and iron and manganese oxides and hydroxides are excellent adsorbents for many trace constituents. ¹⁵⁸⁻¹⁶²

233. Organic matter and clay minerals account for most of the ion exchange character of soils. Both ion exchange and adsorption are surface phenomena. Very often, it is impossible to distinguish between the two types of reactions. Ion exchange reactions are

governed by the law of mass action. Since the trace metals such as Cu and Cd are much lower in concentration than the major ions such as Ca^{++} and Na^+ , it is generally assumed that ion exchange is more important for major ions; however, adsorption and exchange reactions may also be important in regulating trace metal concentrations.

234. Solubility and complexation. The solubility effect governs each soluble species through its solubility constant. If the solubility of the species exceeds the solubility product, K_{sp} , precipitation will tend to occur. This may be important for Ca^{++} and Mg^{++} .

235. For most trace metals, it is necessary to consider the complexation effect in addition to the solubility calculation. Most trace metals are known to exist in various complexes with soluble inorganic and organic ligands. In general, complexation increases the soluble metal concentration. However, soil organic matter also has a great affinity for forming complexes with trace metals. In the latter case, trace metals will be immobilized. The solubility and complexation effects can be expressed by the equations below.

236. The concentration of metal ions as governed by the solubility of the solid $M_p X_q$ is given by

$$[M_f] = \left(\frac{(K_{sp}) M_p X_q}{\gamma_M^p \gamma_X^q [X_f]^q} \right)^{1/2}$$

where $[M_f]$ = concentration of free metal ions

$[X_f]$ = concentration of free anions

γ = ion activity coefficient

K_{sp} = solubility product

p, q = positive integers

237. Due to the complexation effect, the concentration of the complexed species is given by

$$\left[M_m L(i)_n \right] = M \beta(i)_{nm} \left[M_f \right]^m \left[L(i)_f \right]^n \frac{\gamma_M^m \gamma_L^n(i)}{\gamma_{M_n L(i)_n}^m}$$

The total metal concentration can then be derived from

$$\begin{aligned} \left[M_t \right] &= \left[M_f \right] + m \sum_{n=1}^k \sum_{i=1}^j \left[M_m L(i)_n \right] \\ &= \left[M_f \right] + m \sum_{n=1}^k \sum_{i=1}^j \beta(i)_{nm} \left[M_f \right]^m \left[L(i)_f \right]^n \frac{\gamma_M^m \gamma_L^n(i)}{\gamma_{M_n L(i)_n}^m} \end{aligned}$$

where M_t = total metal concentration

i = ligand species

j = total number of ligands

$L(i)_f$ = free concentration of i^{th} ligand

n, m = composition of the complex $M_m L(i)_n$

K = Number of ligands (li) coordinated with M_n

$\beta(i)_{nm}$ = overall formation constant of complex $M_m L(i)_n$

238. Biological effects. Biological activities may promote a change of pH (e.g., production of CO_2), change in redox condition (e.g., reduction of sulfate to sulfide), mineralizing of trace metals and nutrients, and modification of organic matter. In short, all of the previous mechanisms discussed can be affected.

239. Diffusion is the net movement of soluble species from a region of high to one of low concentration. This is known to be a very slow process,¹⁴² but could be an important mechanism if the flow rate is small.

Migration of Contaminants and Nutrients in Confined Land Disposal Areas

240. The concentration of constituents in leachate/interstitial water is highly influenced by the factors discussed in the previous section. Soil and dredged material have very similar characteristics. Factors that cause attenuation in one system may

have neutral or even opposite effect in other systems. Because of this, concentration profiles are seldom homogeneous, and the profiles will be different for different elements.

241. A discussion of the results based on each individual parameter is presented in this section. The relative concentration of the on-site leachate and off-site interstitial water was established for each parameter through a statistical analysis of variance. This helps to identify the pollution potential of the parameters. The extent of contamination will be discussed by comparing the background groundwater samples, groundwater directly below the site, and groundwater in the vicinity of the disposal site (off-site monitoring stations).

Total dissolved solids

242. Theoretically, since every solution exists in an electrically neutral state, the sum of the cations (positively charged ions) expressed in meq/100 g should be balanced by the sum of the anions (negatively charged ions) expressed in the same unit. In this study, the major cations measured were sodium, potassium, calcium and magnesium; the major anions analyzed were chloride, sulfate, and alkalinity. The total concentrations (sum of anions and cations) ranged from a few to about 600 meq/l. Figure 72 shows the relationship between the cations and anions and the total cation concentration. Assuming the above ions constitute the bulk of the charge balance, the difference between the cations and anions was below 10 percent of the total cation concentration in most samples. This is an acceptable experimental error considering that, besides analytical error, some ions such as NH_4^+ and NO_3^- were not measured. These ions have been shown to exist in concentrations as high as a few hundred mg/l in various interstitial waters^{88,105} and in groundwater.⁸⁷

243. The major ions also contribute the bulk of total dissolved solids (TDS), the concentrations of which are shown in Table 21. Table 22 sums up the averages of the major ions from each site. Among the sites, the on-site samples closely reflect the salinity of the dredged area. A comparison of the three averages for each site shows that the off-site samples were lower

than the on-site samples but the background samples were lowest of the three. This suggests an increase of TDS caused by leaching from the site. This will be explored further in the discussion of each individual parameter.

Chloride

244. The on-site chloride concentration ranged from an average of 167 mg/l for the Grand Haven site to 8333 mg/l for the Sayreville site, typical values for freshwater and brackish water systems. Both the Pinto Island and Sayreville sites showed significantly higher concentrations for the on-site samples (Table 22), indicating the salinity level of the overlying water of the dredging site. The Houston samples had concentrations between those of the above two sites. For the Grand Haven site, due to the relatively wide spread of concentration, the differences between the two sets of samples are not statistically significant ($P = 0.65$), i.e., there is a 65 percent chance that the two sets of samples will have similar chloride concentrations.

245. The observed ranking among the sites was expected. The dredged material disposed of at the Sayreville, Houston, and Pinto Island sites was from estuarine environments. The dredged material was thus expected to have a higher chloride content than the off-site soil samples. Grand Haven is in the Great Lakes area. Both the dredged material and the surrounding soils are in a freshwater environment. The differences in chloride concentration, if there were any, should therefore have been small.

246. The on-site Sayreville samples exhibited a general pattern showing an initial decrease then increase in concentration with time. About 14.5 in. of precipitation in the area was recorded for the 3 months between the first and the second sampling periods. The dilution effect of the rainfall probably accounts for the relatively low chloride concentration obtained for the second set of samples (Table K2). The sharp increase for the third set was no doubt due to dredging activities that started immediately before the sampling period.

247. Similar trends were observed for the Pinto Island site. It is interesting to note that the samples obtained after dredging

(second set) were actually lower than the ones obtained before dredging. Again, this could be due to a dilution effect from precipitation. More than 3 in. of rain fell in the 3-week period before the second sampling date. Another possible explanation is the location of dredging. As discussed before, predredging water quality is very important when considering the on-site interstitial water characteristics. If the dredging occurred farther upstream from the channel, i.e., farther away from the brackish water compared to the last dredging site, the salinity should decrease.

248. The groundwater chloride concentrations are summarized in Table 23. The general pattern for the chloride concentration was low levels in the background (BG) samples, peaking in samples under the site (US), then decreasing as the groundwater migrated to the monitoring wells (GW).

249. This pattern is supported by the statistics given in Table 23. Considering all the factors previously discussed, dilution is the only plausible attenuation mechanism affecting the migration of chloride ions.^{153,157} It is reasonable to propose that chloride leached into the groundwater table below the sites during leachate migration through the unsaturated zone. It was subsequently diluted by mixing with less saline groundwater. The monitoring well samples were higher in chloride than the background but lower than the samples from under the site. This shows chloride was also migrating laterally from the site. Pinto Island provides the best evidence for this as the monitoring well groundwater was shown to be consistently higher in chloride content than the interstitial water a few feet above it (Table K4).

250. At the Sayreville site, the average values also had a ranking similar to the Pinto Island samples, i.e., groundwater samples under the site were higher than the downstream monitoring samples which in turn were higher than the background groundwater samples. However, in the monitoring well locations, some of the soil interstitial waters were shown to have higher chloride than the groundwater samples directly below them. This is in contrast to the trend observed in the Pinto Island site. Thus it appears that the

lateral migration is not as obvious in Sayreville. Yet, a reconnaissance survey indicated that the monitoring wells were inundated by the 1.5 m (5 ft) tidal range of the Raritan River. This probably disrupted the levels separating groundwater and interstitial water. Chloride retained in the upper locations may be further concentrated through evaporation.

251. In conclusion, dredged material in the Pinto Island and Sayreville sites contained higher soluble chloride than the natural surroundings of the disposal sites. Chloride was observed to leach from the sites, and migrate away from the sites. In the Grand Haven site, no chloride leaching was observed. This is probably due to the fact that both the dredged material and the disposal site are in a freshwater system.

Sodium and potassium

252. Sodium and potassium have very similar chemical properties. A linear regression analysis on their means reaffirmed that the two metal ions were highly correlated ($R = 0.84$). The highest sodium concentration was found in the Sayreville site and averaged 4310 mg/l. The next highest mean value was 2690 mg/l for the Houston site. Pinto Island, with an average of 1485 mg/l, ranked next. Grand Haven, being in a freshwater environment, ranked last with an average of 110 mg/l. This reflected the salinity of the dredged material.

253. Both sodium and potassium are known to form very soluble compounds. The solid forms that exist in the natural environments are mostly complex primary and secondary minerals such as K-feldspars, K-micas, Na-feldspars, and Na-montmorillonite.⁷⁸ The dissolution of these minerals usually leads to the formation of another mineral, i.e., incongruent dissolution, and the dissolution rates are also very slow.⁷⁸ Thus, dissolution/precipitation reactions are expected to have an insignificant effect on the migration of sodium and potassium.

254. As indicated by the low P values, both sodium and potassium were higher in the on-site samples than in the off-site samples (Table 22), suggesting a leaching potential. Neither sodium nor potassium is regarded as a hazardous contaminant in

low concentrations. However, high levels can make drinking water unpalatable, limit the use of water for agriculture, and promote degradation of the structure of aerable soils. The transport of these two ions serves as an indicator of the rate of leachate migration. It has been reported that suspended clay minerals, after being transported by river to the marine environment, exchange magnesium and sodium for calcium and potassium.^{161,162} The evidence provided in these studies was an increase in Na^+ to K^+ and Ca^{++} to Mg^{++} ratios. Both Pinto Island and Sayreville dredged material samples had higher interstitial water salinities than the surrounding native soil. The ratio of Na^+ to K^+ was indeed found to be higher for the on-site than the off-site samples (31.2 and 11.7 for Pinto Island, 28.6 and 16.8 for Sayreville). The ratios in the exchangeable phase were found to be 2.0 and 0.33 for Pinto Island and 2.9 and 1.3 for Sayreville. Therefore, exchange between sodium and potassium may affect the migration of these two ions. However, it was expected that, in comparison to dilution effects, exchange mechanisms would only play a minor role at these two sites. This is especially true for the fresh-water Grand Haven site, where the average ratio of Na^+ to K^+ was very similar for the on-site and the off-site samples. Again, this is probably due to the relatively low salinity concentrations in all samples.

255. The concentration pattern at Houston was quite varied. Certain spots would show an increase in concentration with time or depth, while an opposite trend would be found at another spot. In short, the pattern was very random. This was probably a result of ion exchange and the repeated drying and wetting due to precipitation and evaporation (resulting in downward salt movement with the gravitational water and upward movement with the capillary water).

256. Based on the samples analyzed, it is concluded that sodium behavior was similar to that of potassium and chloride. Dredged material contained higher soluble sodium and potassium than the off-site monitoring samples, thus establishing a leaching potential. Both ions were observed to leach from the sites. Possible mechan-

isms controlling the migration of these two ions included dilution and ion exchange with dilution the dominant mechanism.

Calcium and magnesium

257. The averages and ranges for the calcium concentrations are given in Table 22. For the on-site samples, Houston had the highest average concentration (428 ppm), followed in order by Sayreville (386 ppm) , Grand Haven (356 ppm) , and Pinto Island (140 ppm). For the Pinto Island and Sayreville disposal sites, values of off-site samples were only about half of those of on-site samples. The averages for the on- and off-site Grand Haven samples were quite close: 356 ppm and 321 ppm, respectively. Student's "t" test results suggested that the differences were significant for the Sayreville and Pinto Island sites ($p < 0.01$). For the Grand Haven site, a p value of 0.35 was obtained, meaning that there was a 65 percent chance that the on-site samples were higher than the off-site samples. Since on-site samples were higher, there was a potential for calcium to migrate away from the sites.

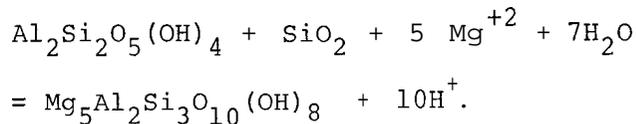
258. A comparison of the samples underneath the site with the off-site monitoring well and background samples indicated that the under-site samples were statistically higher than the other two groups, suggesting either a calcium leaching front or dissolution of calcium solids underneath the disposal sites. In the Grand Haven site, the monitoring well samples were higher than the samples beneath the site (Table 22). This result was probably due to dissolution of calcium carbonate.

259. Concentrations of magnesium correlate fairly well with calcium. The level of magnesium was found to be higher in the on-site than the off-site samples from Pinto Island, Sayreville, and Grand Haven, suggesting a leaching potential. Comparing the averages among the sites indicates that the magnesium concentration followed the order of seawater > brackish water > freshwater. The average seawater magnesium concentration has been reported to be 1296 mg/l, and the average river water concentration has been reported to be 9 mg/l.⁷⁸ The Sayreville site, which had highest relative sediment interstitial water salinity values, also showed the highest average magnesium concentration of 728 mg/l.

Houston, next in relative salinity, had the second highest average, 394 mg/l; Pinto Island, a low-salinity site, had an average of 174 mg/l; and Grand Haven, a freshwater site, had an average of 71 mg/l.

260. Possible mechanisms controlling the transport of calcium and magnesium included dilution, precipitation/dissolution, and ion exchange. Comparing the results with those for K, Na, and Cl, it is evident that dilution cannot solely account for the observed results. Drever¹⁶³ considered several clay mineral transformations and syntheses as mechanisms for the removal of magnesium in the ocean. Possible reactions included:

- a. Transformation involving major changes in the clay lattice, such as the conversion of kaolinite to chlorite:



- b. Transformation involving only the interlayer positions such as "upgrading the degraded lattices," i.e., restoring ions lost due to weathering.

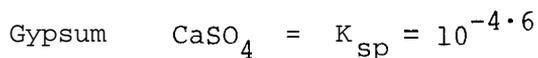
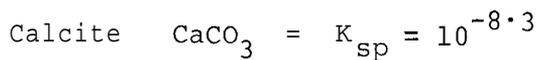
- c. Synthesis of other clay minerals.

However, these reactions were expected to play an unimportant role in the present study due to the very lengthy time frame involved in most clay mineral transformations.

261. The transport of magnesium was probably regulated by the solubility of simple solids such as brucite ($\text{Mg}(\text{OH})_2$), magnesite (MgCO_3), nesquehonite ($\text{MgCO}_3 \cdot 3\text{H}_2\text{O}$), hydromagnesite ($\text{Mg}_4(\text{CO}_3)_3(\text{OH})_2 \cdot 3\text{H}_2\text{O}$), and dolomite ($\text{CaMg}(\text{CO}_3)_2$). An activity ratio diagram for the hydroxide and carbonate solids is shown in Figure 73. At $\text{pH} < 7.2$, nesquehonite ($K_{\text{sp}} = 10^{-5.4}$) is expected to be the controlling solid. From $\text{pH} 7.2$ to 9.7 hydromagnesite ($K_{\text{sp}} = 10^{-29.5}$) will be the controlling solid. At $\text{pH} 9.7$ and above brucite ($K_{\text{sp}} = 10^{-11.6}$) becomes the stable solid. Most analyzed samples were below $\text{pH} 8$. Thus, the solubilities of nesquehonite and hydromagnesite may regulate most of the magnesium mobility and transport.

262. Calcium is known to form stable carbonate and sulfate solids

in sediments. The solubility constants for the two common solids are:

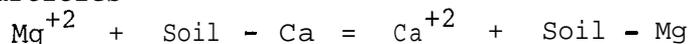


Many of the Sayreville samples had very low pH (3 to 5), with low carbonate and high sulfate concentrations ($7 \times 10^{-3} \text{M}$). It is possible that calcium sulfate was the major controlling solid for the concentrations in many Sayreville samples, while calcium carbonate was the controlling solid for other samples. Figure 74 is an activity ratio diagram for the two solids. It was constructed assuming $C_t = 10^{-2.5} \text{M}$ and $\text{SO}_4^- = 10^{-2.5} \text{M}$. It is seen that calcium sulfate only becomes the controlling solid when pH is below 3.5. The following tabulation is a compilation of the observed calcium ranges and the predicted concentrations, assuming that calcium carbonate solubility is the controlling mechanism:

	<u>Observed (mg/l)</u>	<u>Predicted</u>
Sayreville	50 to 620	200 to 2000
Pinto Island	25 to 440	20 to 2000
Houston	205 to 1020	20 to 2000
Grand Haven	80 to 610	20 to 2000

The observed data were within the range calculated from the calcite solubility, suggesting that this was the major controlling mechanism.

263. One other possible mechanism affecting the migration of calcium is ion exchange with magnesium. As previously discussed for the Pinto Island and Sayreville sites, interstitial water and dredged material samples contained much higher calcium concentrations than the off-site samples. As the leachate percolated away from the site, magnesium may have exchanged with the calcium ions held by soil particles:



The average $\text{Mg}^{+2}/\text{Ca}^{+2}$ ratio changed from 1.25 for the on-site Pinto Island samples to 0.53 for the off-site samples. The change in the $\text{Mg}^{+2}/\text{Ca}^{+2}$ ratio between seawater and river water had been suggested

as evidence for the preferential ion exchange reaction between the two ions.^{193,194,198} The exchange effect (Mg^{+2}/Ca^{+2} ratio) is not as evident in the other sites. The reason for this is not known.

264. In conclusion, it appeared that soluble calcium was higher in the on-site dredged material samples than the off-site soil samples for the Sayreville and Pinto Island sites. The migration is controlled by ion exchange and the dissolution of calcite if pH is greater than 3.5; gypsum if pH is less than 3.5. Based on the samples analyzed, calcium appeared to have leached from the Pinto Island and Sayreville sites.

265. Soluble magnesium concentration was shown to be higher in the on-site samples than the off-site samples (true in three case study sites) i.e., a leaching potential was established. Actual leaching of magnesium was observed in three sites. This was indicated by comparing the groundwater samples below the sites with the groundwater samples downstream from the sites and samples upstream from the sites. Possible mechanisms controlling the migration of magnesium included dissolution of magnesium solids such as nesquehonite and hydromagnesite and ion exchange.

Alkalinity and TOC

266. A wide range of alkalinity was registered in this study. Among the monitored sites, the average alkalinity value was in decreasing order, Houston (1092 mg/l), Grand Haven (589 mg/l), Pinto Island (446 mg/l), and Sayreville (196 mg/l). For individual samples, the values ranged from nil to close to 2000 mg/l.

267. Many of the samples with negligible alkalinity were from the Sayreville site. Alkalinity is a measure of the acid neutralization capacity and is determined by titration with acid down to a pH of 4.3 to 4.5. Many of the Sayreville off-site and background samples had pH levels below 5. This accounts for the low alkalinity values for that site.

268. Alkalinity was found to be higher in on-site samples than off-site samples from the Pinto Island and Grand Haven sites (Table 22), suggesting a leaching potential for these two sites. A comparison of the samples collected beneath the two sites with back-

ground and off-site samples, showed that for both the Pinto Island and the Grand Haven sites, the average values were in decreasing order: under-site, off-site monitoring well, and background. This suggests that an alkalinity leaching front had arrived at the under-site locations and was diluted as it traveled downstream (groundwater) away from the site. By comparing the on-site and off-site monitoring well samples, an attenuation of 48 percent (from 446 to 230 mg/l) was registered at the Pinto Island site, and an attenuation of 45 percent (from 589 to 326 mg/l) was obtained at the Grand Haven site.

269. In most natural waters, alkalinity is due mainly to carbonate and bicarbonate ions and is defined as:

$$\text{Alk} = [\text{HCO}_3^-] + 2 [\text{CO}_3^{2-}] + [\text{OH}^-] - [\text{H}^+]$$

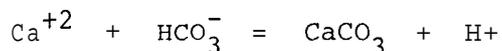
As will be discussed in the later sections, the carbonate concentration is very important because carbonate solids are believed to be the controlling solids for most metals in an oxidizing environment.

270. Mechanisms controlling the levels and transport of alkalinity include dissolution of carbonate solids, weathering reactions, and oxidation-reduction reactions. Weathering reactions were probably too slow to explain the findings in this study. Dissolution of solids such as calcite and hydromagnesite was expected to play an important role and this will be discussed in later sections.

271. Biological activities also play a dominant role. The oxidation of organic matter during sulfate reduction changes alkalinity levels:



Brooks, Presley, and Kaplan postulated that in marine sediments this is followed by another reaction:¹¹⁴



This controls the calcium concentration and buffers the pH.

272. In this study, TOC appeared to be highly correlated with alkalinity among the sites ($R = 0.86$), another indication that biological action might affect alkalinity. Like alkalinity, TOC was potentially leachable from the Pinto Island and Grand Haven sites (Table 22). For these two sites, the samples collected from underneath the sites were higher in TOC than the off-site monitoring well samples, which in turn were higher than the background samples. This trend was similar to that of alkalinity. A TOC attenuation of 27 percent was noted for the Pinto Island site, and a 63 percent attenuation was observed at the Grand Haven site.

273. For the Sayreville site, the TOC level was higher in the off-site than the on-site samples. This is probably due to the fact that the off-site area is in part a salt marsh. The decay of vegetation serves as the source for the TOC. It is well known that organic matter forms stable complexes with many trace metals. The high TOC content may in part account for the higher trace metal levels in many off-site samples at Sayreville. The oxidation of organic matter by sulfate, as previously discussed, may also explain the relatively low pH found in the vicinity sediments. Low pH also favors the dissolution of most trace metals.

274. To sum up, alkalinity and TOC were observed to be higher in the on-site than the off-site Pinto Island and Grand Haven samples. Both were shown to have leached to the groundwater below the sites. The transport of alkalinity is probably regulated by dissolution of calcite and biological oxidation. For the Sayreville site both soluble TOC and alkalinity were higher in the off-site soil samples than the on-site dredged material samples. The reason for this is not clear. It may be due to the decay of vegetation since the vicinity of the site was formerly a salt marsh.

Phosphate

275. The distribution of phosphate is dependent on a highly complex and dynamic system. In a literature review, Patrick and Mahapatra⁸⁶ cited that phosphate availability under submerged conditions was governed mainly by the form and solubility of iron phosphate compounds. In a reducing environment, iron is converted from the ferric to the ferrous state, and phosphate is released.

If aluminum abounds, phosphate will be reprecipitated as aluminum phosphate. The phosphate levels detected in this study were fairly low, ranging from below the detection limit to a high of 0.91 ppm. There was no apparent correlation between the soluble phosphate and total phosphate concentrations. Only the Pinto Island site showed a higher on-site average than the off-site average (0.1 to 0.03 ppm, respectively).

276. Stumm and Leckie plotted the phosphate solubility of various solids versus pH.¹⁶⁵ The following is a summary of the phosphate concentration based on ferric phosphate (dufrenite) and calcium phosphate (apatite) solubility:

pH	Ferric-PO4	Apatite-PO4
3	$10^{-3.4}$ M = 12 ppm	
4	10^{-5} M = 0.31 ppm	
5	$10^{-5.2}$ M = 0.20 ppm	
6	10^{-5} M = 0.31 ppm	
7		$10^{-5.4}$ M = 0.12 ppm
8		$10^{-7.2}$ M = 0.002 ppm

277. At low pH, the predicted value is much higher than the observed values. Sayreville background samples were very acidic, with pH ranging from 2.8 to 7.2. Soluble phosphate ranged from 0 to 0.11 ppm. The highest soluble phosphate concentration was in a sample which had the highest pH (7.2). This was probably due to less phosphate adsorption by clay minerals, since phosphate adsorption is favored by low pH.^{78,166} At other pH values, the predicted concentrations of ferric iron phosphate and calcium phosphate together with adsorption onto clay minerals may have accounted for the phosphate content detected.

278. In conclusion, soluble phosphate was at very low levels. Only the Pinto Island site showed a leaching potential (0.1 ppm on-site versus 0.03 ppm off-site). Actual leaching was not observed. Phosphate can be ruled out as a potential water quality problem.

Trace metals

279. With the exception of iron and manganese, concentrations of trace metals in the leachate samples were mostly in the ppb or sub ppb range. At such low concentrations, precipitation/dissolution, complexation, and adsorption are expected to play dominant roles in regulating their transport.

280. In general, in an aerobic environment, the stable solids that control the solubilities of these metals are oxides, hydroxides, or carbonates. Under reducing conditions, most trace metals may gradually precipitate as sulfides due to the generally much lower solubilities of these sulfides.

281. Acid-soluble sulfide was detected in all of the dredged material and soil samples. However, although hydrogen sulfide could be smelled in a few of the water samples during sampling, no free sulfide was detected in the water samples. The threshold of smell for hydrogen sulfide may be as low as 10^{-9} moles/l, or a few ppb.⁷⁸ It is possible that hydrogen sulfide did exist in the samples but was below the detection limits for the methods used (electrode and methylene blue photometric method).

282. The low sulfide concentrations could have resulted from either of two methods. The first possibility is that the free sulfide was oxidized by oxygen which diffused into the samples during collection. Water samples were collected either from well points or suction lysimeters. It is highly probable that traces of oxygen could have diffused into the water inside the sampling devices. Attempts to improve this condition by flushing the samples with nitrogen were dropped because of the inaccessibilities of the sampling locations and the difficulties in carrying the nitrogen tanks.

283. The second possibility is that the sulfide concentrations were below the detection limits for the methods used. Although large amounts of free sulfide ($\text{H}_2\text{S} + \text{HS}^- + \text{S}^{2-}$) could be produced from the reduction of sulfate by organic matter, the concentration remaining in solution might be small due to the formation of metallic sulfides, mainly FeS and FeS₂.

284. Both possibilities are equally probable. The metal sul-

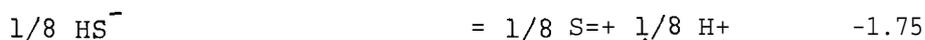
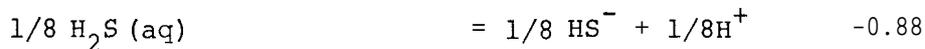
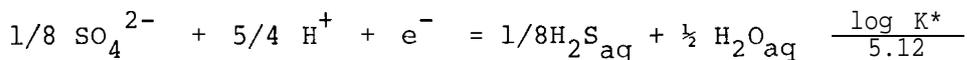
solubilities are orders of magnitude lower than those for metal carbonates, hydroxides, or oxides. Although existing in undetectable concentrations, sulfide could still play a governing role at extremely low concentrations. The following calculation, based on the solubility products of cadmium, illustrates the importance of sulfides.

285. The solubility product for CdS is $10^{-26.96}$ and CdCO₃ is $10^{-13.69}$. The ratio of the sulfide ion concentration and carbonate ion concentration is given by:

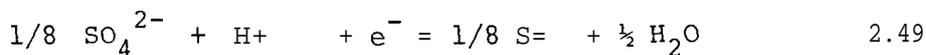
$$R = \frac{[S^{2-}]}{[CO_3^{2-}]} = \frac{(K_{sp})_{CdS}}{(K_{sp})_{CdCO_3}} = \frac{10^{-26.96}}{10^{-13.69}} = 10^{-13.27}$$

286. If R is greater than $10^{-13.27}$, CdS becomes the controlling solid, and vice versa. The carbonate concentration is usually about 10^{-5} to 10^{-7} M. Therefore, if S²⁻ is greater than $10^{-20.27}$ to $10^{-18.27}$ M, CdS will be the controlling solid for cadmium.

287. Obviously, it is not yet possible to detect sulfide at such low concentrations. However, we can estimate the conditions under which sulfide solids become important. Consider the following equations:



Combining the three equations gives:



$$Eh^0 = 2.303 \frac{rt}{n} \log K = 0.059 \log K =$$

$$= 0.147 \text{ V at } 25^\circ\text{C}$$

$$Eh = Eh^0 + 0.059 \log \frac{[SO_4^{2-}]^{1/8}}{[S^{2-}]^{1/8}} - 0.059 \text{ pH}$$

* K's obtained from ref. 78 and 118.

$$= 0.147 + 0.059 \left\{ \frac{1}{8} \log \left[\text{SO}_4^{=}\right] - \text{pH} \right\} + 0.007 \text{ pS}^{=}$$

287. In this study the sulfate ion concentration ranged from $10^{-1.6}$ to $10^{-3.2}$ and most pH values were within the range of 5 to 8. This makes the second term to the right of the equation roughly equal -0.306 to -0.496 and

$$\text{Eh} = -0.160 \text{ to } -0.350 + 0.007 \text{ pS}^{=}$$

where $\text{pS}^{=} = -\log \left[\text{S}^{\cdot} \right]$

Eh = redox potential in Volts

For Cd, CdS becomes dominant when $\left[\text{S}^{\cdot} \right]$ is greater than $10^{-20.27}$ or $\text{pS}^{=} = 20.27$

$$\text{Eh} = -0.160 \text{ to } -0.350 + 0.007 \times (+20.27)$$

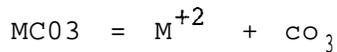
$$= -0.018 \text{ to } -0.208$$

288. Choosing the upper limit, cadmium in any sample with Eh below -18mV may be controlled by the solubility of CdS. Stumm and Morgan estimated that for samples that give a sulfide odor, the partial pressure of H_2S is between 10^{-2} to 10^{-8} atm. or the hydrogen sulfide (H_2S) concentration is around 10^{-3} to 10^{-9} M.⁷⁸ For samples with Eh below -18mV and pH = 5, hydrogen sulfide is given by

$$\begin{aligned} \left[\text{H}_2\text{S} \right] &= \frac{\left[\text{H}^+ \right]^2 \left[\text{S}^{\cdot} \right]}{K_1' K_2'} \\ K_1' &= 10^{-7} \\ K_2' &= 10^{-14} \\ &= \frac{(10^{-5})^2 (10^{-20.27})}{10^{-21}} \\ &= 10^{-9.27} \approx S_t \end{aligned}$$

The value is very close to that estimated by Stumm and Morgan,⁷⁸ and is a plausible value because only some samples had a H_2S smell.

289. In an oxidizing environment, most trace metals could be controlled by the solubility of the metal carbonate solid:



The free metal concentration is given by:

$$M^{+2} = \frac{K_{sp}}{[CO_3^{=}]}$$

$$pM = pK_{sp} + \log C_t + \log \alpha_2$$

where C_t = total carbonate concentration

$$\begin{aligned} &= [H_2CO_3] + [HCO_3^-] + [CO_3^{=}] \\ \alpha_2 &= \frac{H^{+2}}{K_1 K_2} + \frac{H^{+2}}{K_2} + 1^{-1} \end{aligned}$$

K_1, K_2 = first and second dissociation constants of H_2CO_3 , $10^{-6.3}$ and $10^{-10.3}$, respectively.

290. No direct measurement of C_t was performed. However, total carbonate concentration can be estimated from alkalinity and total inorganic carbon data. At $K_1 < pH < K_2$, C_t is roughly equal to alkalinity since the majority of the carbonate species exist as bicarbonate ions. At lower pH values, especially when alkalinity approaches 0, the carbonic acid (H_2CO_3) concentration is expected to increase. TIC measures at low pH values ranged from below the detection limit (5 mg/l) to 20 mg/l. It is reasonable to assume C_t ranged from $10^{-3.5}$ moles to $10^{-1.5}$ moles, with most samples in the neighborhood of 10^{-2} moles (corresponds to 500 mg/l alkalinity).

291. Based on C_t and the previously derived equation derived before, the range of free metal concentrations can then be estimated. Using the K_{sp} listed in Table 24 and assuming $C_t = 10^{-3.5}$ and $10^{-1.5}$ moles, the free metal concentration expected in this study is given by:

$$p_{Cd^{+2}} = 10.1 \text{ or } 12.1 + \log \alpha_2$$

$$\begin{aligned}
p_{\text{Cu}^{+2}} &= 6 \text{ or } 8 + \log a_2 \\
p_{\text{Fe}^{+2}} &= 6.9 \text{ or } 8.9 + \log a_2 \\
p_{\text{Mn}^{+2}} &= 5.7 \text{ or } 7.7 + \log a_2 \\
p_{\text{Ni}^{+2}} &= 4.7 \text{ or } 6.7 + \log a_2 \\
p_{\text{Pb}^{+2}} &= 9.8 \text{ or } 11.8 + \log a_2 \\
p_{\text{Zn}^{+2}} &= 7.2 \text{ or } 9.2 + \log a_2
\end{aligned}$$

Figures 75 and 76 are graphic presentations of the expected metal ranges using pH as the master variable. The diagrams are constructed by assuming:

$$\begin{aligned}
\frac{d \log_2}{d \text{pH}} &= 0 \text{ at } \text{pH} > p^{K_2} \\
&= 1 \text{ at } p^{K_1} < \text{pH} < p^{K_2} \\
&= 2 \text{ at } \text{pH} < p^{K_1}
\end{aligned}$$

Cadmium

292. Soluble cadmium concentrations were usually the lowest among all metals analyzed. The on-site water samples averaged 0.8 ppb for the Grand Haven site to a high of 58 ppb for the Sayreville site. The highest concentration was 200 ppb in a Sayreville leachate. Many of the Sayreville samples were in the 100-ppb range. Samples from other sites were relatively uniform, and were in the low or sub-ppb range. The spread for these samples was so small that a difference of 0.6 ppb between the on- and off-site Grand Haven samples was shown to be statistically significant. In this case, the off-site average was higher than that of the on-site water samples (Table 22).

293. Considering the groundwater conditions (Table 23), the Grand Haven site background and monitoring well waters had slightly higher concentrations than the water samples obtained directly beneath the disposal area (averages of 1.4 and 0.92 ppb compared

to 0.79 ppb). For the Pinto Island samples, one high concentration (46 ppb) was detected in a second set under-site sample. The rest were all about 1 ppb. Hem¹⁷⁰ reported that the median concentration of cadmium in 726 samples of water taken from rivers and lakes of the United States was a little below 1 ppb. The low concentration range found in the Grand Haven and Pinto Island samples indicates that cadmium would pose no potential threat to deterioration of the groundwater quality.

294. The highest cadmium concentrations were found in the Sayreville samples. One of the monitoring wells (NJF 2) had a concentration of about 100 ppb throughout the study (Table K2). The two background wells (NJI and NJJ) also showed consistently high values. The local groundwater flow was a radial pattern flowing away from the site (Figure 69). It was difficult to select a good background well to reflect the impact of the leaching of cadmium from dredged material. The distribution of cadmium was probably regulated by the local environmental conditions, especially the Eh and pH.

295. Krauskopf¹⁵⁸ calculated that seawater is undersaturated with respect to cadmium. He suggested that precipitation as cadmium sulfide is a possible control mechanism in some localized reducing environments where the free sulfide concentrations are high. As discussed above, cadmium sulfide precipitation probably occurred if the Eh values were below -18 mV. The following tabulation shows the range of cadmium concentrations observed in samples with Eh above -18 mV and samples with Eh below -18 mV:

Site	Samples Below -18 mV	Samples Above -18 mV
Sayreville	1 to 8 ppb	1 to 204 ppb
Pinto Island	1.2 to 4 ppb	<1 to 46 ppb
Grand Haven	< 1 ppb	<1 to 4 ppb
Houston	1 to 102 ppb	1 to 8 ppb

It appears that soluble phase cadmium was higher under more oxidizing conditions (above -18 mV) where cadmium carbonate is the controlling solid.^{167,168} The cadmium concentration is given by:

$$Cd^{+2} = \frac{K'_{sp}}{[CO_3^{=}] } = \frac{10^{-13.69}}{[CO_3^{=}] }$$

296. In the reducing environment, where cadmium sulfide is the stable solid, cadmium concentration is given by:

$$Cd^{+2} = \frac{K_{sp}}{[S^{=}]} = \frac{10^{-26.96}}{[S^{=}]}$$

Depending on the sulfide concentration, cadmium can exist in the range from the high ppb level to ten orders of magnitude lower.

297. Cadmium is known to form stable soluble complexes with various ligands, and Lu and Chen,¹⁴⁸ suggested that chloride is the most important ligand in seawater. The total cadmium concentration measured would be:

$$Cd_t = Cd_f \left\{ 1 + B_1 (Cl^-) + B_2 (Cl^-)^2 + B_3 (Cl^-)^3 + B_4 (Cl^-)^4 + B_5 (Cl^-)^5 + B_6 (Cl^-)^6 \right\}$$

Where

$$Cd_f = \frac{K_{sp}^{CdS}}{(S^{=})} \quad \text{in the reducing environment}$$

$$\text{and} \quad = \frac{K_{sp}^{CdCO_3}}{(CO_3^{=})} \quad \text{in the oxidizing environment}$$

298. As discussed previously, cadmium sulfide probably becomes dominant when pS^{2-} is smaller than 20, or pS_t is smaller than 9. Figure 77 is a distribution diagram of the sulfide species assuming $pS_t = 9$. Referring to Figures 75 and 77, the free cadmium concentration range, under either sulfide or carbonate solids control, is calculated for each site to be as follows:

Site	pH Range	CdS Control	CdCO Control
Sayreville	3 to 7	4.5×10^{-4} to 1.8×10^3 ppb	0.7 ppb to 1.1×10^4 ppm
Pinto Island	4.8 to 8.2	1.8×10^{-5} to 3.5 ppb	1.1 ppb to 7.1×10^2 ppm
Grand Haven	5.8 to 7.7	3.5×10^{-5} to 0.06 ppb	7.1 ppb to 4.5 ppm
Houston	5.4 to 7.8	3.5×10^{-5} to 0.28 ppb	5.6 ppb to 35 ppm

299. In an oxidizing environment the predicted values were close to the observed values for samples with high pH. The reverse was true for the reducing environment where the predicted values ranged from 0.06 to 3.5 ppb for samples having pH values from 3 to 5.8. At the other end of the pH scale the observed values were several orders of magnitude lower than the theoretical values.

300. Jenne¹⁵⁹ proposed that cadmium coprecipitates with iron and manganese when the latter two are oxidized. Adsorption on clay minerals and organic matter may be another immobilizing mechanism. It was suggested that in soils, clay minerals and organic matter are the major components involved in adsorptive reactions.^{171,172} Both mechanisms are likely to reduce the cadmium concentration in an oxidizing environment.

301. In summary, there was a potential for cadmium to leach from the Pinto Island and the Sayreville site. However, no actual leaching was observed. It appeared that cadmium transport was regulated to a great extent by the controlling solids and by adsorption onto clay minerals. The average cadmium concentration was very low. It is concluded that soluble cadmium from diked dredged material disposal practice poses no threat to groundwater quality.

Copper

302. A wide range of copper concentrations was found at the Sayreville site. The on-site water samples ranged from 3 ppb to 3 ppm and averaged 231 ppb. The four monitoring wells, which were located from a few to about 100 m away from the site, provided water samples with a slightly higher average concentration of 500 ppb and a wider range (1 ppb to 6.1 ppm). The two background wells were located about 700 m (NJI) and 1500 m (NJJ) away from the Sayreville site. Both background wells had relatively high copper concentra-

tions. The copper concentration of these two wells averaged 2.6 ppm during the 9-month study.

303. Many of the groundwater samples at Sayreville had copper in the ppm range. The highest value, 11.4 ppm, was found for a background well sample (NJJ). The highest concentration in a monitoring well sample was 6.1 ppm, found in NJF. The highest under-site sample was only 2 ppm, found in NJD. All these values were from the third set of samples, which were collected after new disposal activities had resumed at this site. One month later, NJJ and NJF samples decreased to 330 and 492 ppb, respectively. No sample was collected from NJD during that period.

304. Due to the high concentrations found in the background and monitoring wells, it was not possible to assess the copper leaching potential at this site. As discussed before, the groundwater pattern of the Sayreville site is a complex radial flow system. This makes it very difficult to locate a true background well. Locations too close to the site might be already affected by the leachates. Locations too far away from the site might be influenced by pollution sources other than the dredged material disposal site. For example, the National Lead Industries, which manufactures many inorganic and organic chemicals, discharges its industrial waste in the vicinity. The impact of this on the local groundwater quality is not known.

305. The locations with high copper levels (NJJ, NJI, and NJF) had very low pH values (3 to 4) and high Eh. It has been suggested that in the oxidizing environment soluble copper is probably regulated by carbonate hydroxyl solids such as malachite ($\text{Cu}_2\text{CO}_3(\text{OH})_2$).^{115,173} The other important copper solids include copper hydroxide ($\text{Cu}(\text{OH})_2$) and copper carbonate (CuCO_3). At pH 3, the ion ratio is given by the following equations:

$$R_1 = \frac{K_{sp} \text{Cu}(\text{OH})_2}{K_{sp} [\text{Cu}_2\text{CO}_3(\text{OH})_2]^{1/2}} = 10^{-2.7} = \frac{[\text{OH}^-]}{[\text{CO}_3^{=}]^{1/2}} = \frac{10^{-11}}{[\text{CO}_3^{=}]^{1/2}}$$

$$R_2 = \frac{K_{sp} \text{ CuCO}_3}{K_{sp} [\text{CuCO}_3(\text{OH})_2]^{\frac{1}{2}}} = 10^{7.1} = \frac{(\text{CO}_3)^{\frac{1}{2}}}{(\text{OH}^-)^2}$$

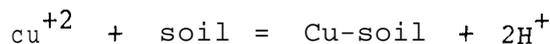
$$= 10^{22} (\text{CO}_3^=)^{\frac{1}{2}}$$

It is reasonable to assume $\text{CO}_3^=$ to be between 10^{-14} to 10^{-16} M, which corresponds to a carbonic acid (H_2CO_3) concentration of 10^{-5} to $10^{-3.4}$ M. By substituting these numbers into the equations for R_1 R_2 , malachite ($\text{Cu}_2\text{CO}_3(\text{OH})_2$) appears to be the logical controlling solid in the above systems. Carbonate and hydroxide solids become unstable under acidic pH conditions. Likewise, as pH increases, soluble phase copper is expected to decrease. This probably partially accounts for the high soluble copper concentrations found in the Sayreville samples. The pH was generally higher for the fourth set of data than for the third set, and the copper showed a corresponding decrease.

306. However, from simple solubility calculations, copper should exist in concentrations orders of magnitude higher than the observed values:

$$\text{Cu}^{+2} = \frac{K_{sp}^{\frac{1}{2}}}{[\text{OH}^-][\text{CO}_3^=]^{\frac{1}{2}}} = \frac{10^{-16.6}}{(\text{OH}^-)(\text{CO}_3^=)^{\frac{1}{2}}} = 2 \times 10^6 \text{ ppm}$$

Copper is known to form stable complexes with chloride, hydroxide, and other inorganic and organic ligands. Though not yet very well understood, the soluble organic complexes are believed to bind the majority of soluble copper. The majority of the soluble copper species are positively charged^{174,175} and are strongly adsorbed by clay minerals.^{158,167,175} Lindsay¹⁷³ posed the following equation to explain the high copper concentrations in some soils:



The K value was found to be $10^{-3.2}$,¹⁷⁶ the copper concentration is given by:

$$\text{Cu}^{+2} = 10^{3.2} (\text{H}^+)^2$$

At pH 3, the copper concentration is calculated to be 99 ppm, much lower than the predicted value from the solubility of malachite.

307. Jenne¹⁵⁹ proposed that iron and manganese oxides provide large surface areas for sorption reactions with copper. It is also known that copper chelates strongly with humic substances.¹⁷⁷ A combination of these mechanisms probably governs the transport of copper in the oxidized environment.

308. Copper sulfide is expected to be the controlling solid in the reducing environments. The solubility product for this solid is very low. Assuming $[S^{2-}]$ to be 20, the copper concentration is given by:

$$c_u^{+2} = \frac{K_{sp}}{S^{2-}} = \frac{10^{-36.4}}{10^{-20}} = 10^{-16.4} M$$

$$= 2 \times 10^{-7} \text{ ppb}$$

309. The following is a tabulation of the ranges of soluble copper concentrations, arranged according to oxidizing and reducing conditions:

Site	pH Range	Oxidizing, CuCO ₃ Control	Reducing, CuS Control
Sayreville	3 to 7	1 ppb to 11.4 ppm	1 to 145 ppb
Pinto Island	4.8 to 8.2	1 to 345 ppb	2 to 24 ppb
Houston	5.8 to 7.7	5 to 165 ppb	4 to 13 ppb
Grand Haven	5.4 to 7.8	1 to 63 ppb	2 to 7 ppb

The copper concentration is generally much lower in a reducing environment than in an oxidizing environment. The observed values are still much higher than the predicted values.

310. Complexation with other ligands can solubilize copper to a much higher total concentration than that calculated from copper sulfide solubility. Copper is known to form highly stable complexes with soluble inorganic and organic molecules. The formation constants of copper with common ligands, such as chloride, hydroxide, and sulfate, have been extensively tabulated in the literature.^{178,179} However, these complexes are not expected to increase the copper concentration by more than 100 fold.

311. The only likely candidates for competing ligands are organic molecules. As reflected by the formation constants, copper organic complexes are much more stable than the inorganic complexes. For example, as compiled by Lu and Chen,¹⁴⁸ the log formation constant for Cu-histidine is 11.71 as compared with 1.58 for CuCl^{+2} . Lerman and Childs¹⁸⁰ found log B for nitrilotriacetates (NTA) to be 13. The nature of soluble organics in natural waters is not very well known. It is generally believed that copper is strongly complexed with organic matter, and this is expected to play an important role in regulating the transport of copper.^{173,181,182}

312. Copper was found to be higher in the Pinto Island and Grand Haven on-site samples than in the off-site samples (Table 22). Monitoring the water quality in the groundwater table indicated that at the Pinto Island site, the wells underneath the site provided samples with the highest concentration, possibly due to leaching from the dredged material in the site. The downgradient monitoring wells had a lower average concentration (10 ppb) but were statistically higher than the background wells (Table 23). This suggests that copper might have migrated to the monitoring wells from on-site sources. Due to the various attenuation mechanisms discussed, the average concentration decreased from 41 ppb in samples obtained from beneath the site to 10 ppb for the monitoring well samples.

313. For the Grand Haven site, the background samples were similar in soluble copper concentration to the samples collected underneath the site (12 and 15 ppb, respectively), suggesting that either copper was not leached out or was greatly attenuated as it left the site.

314. In summary, leaching effects could not be established for the Sayreville site due to the high background concentrations. Both the background and the downstream samples were higher than the on-site samples. This is probably due to the formation of organic complexes. The off-site samples were shown to have higher TOC than the on-site samples.

315. Leaching was observed at the Pinto Island site. However, the concentration was so low that it posed no deterioration threat to the groundwater quality.

Nickel

316. Among the trace metals analyzed, other than iron and manganese, the nickel concentration was usually the highest. This is in accordance with the relatively higher solubility products of the nickel controlling solids: $10^{-8.2}$ for NiCO_3 and $10^{-18.5}$ for a NiS , and $10^{-25.7}$ for γNiS .

317. In the vicinity of the Sayreville site, most samples were in the hundred ppb range. The average off-site sample concentration was 237 ppb, and the average on-site sample concentration was 420 ppb. Both numbers were highest among the case study sites. Both the Grand Haven and Pinto Island sites also had higher on-site averages than the off-site averages: 128 and 27 ppb for Grand Haven, 42 and 10 ppb for Pinto Island. In most natural processes, species migrate from zones of high concentration to low concentration areas. Thus there is a potential that nickel may migrate to the groundwater from the disposal sites.

318. The nickel data for groundwater samples from each site are summarized in Table 23. At Pinto Island, nickel increased from 4.3 ppb in background water samples to 40 ppb in water collected beneath the site, and then decreased to 11 ppb for water in the off-site monitoring wells. The under-site samples average of 40 ppb was as high as the on-site average of 42 ppb, suggesting that groundwater directly below the site was affected. During horizontal migration of leachate (away from the site), nickel was reduced by 75 percent due to various attenuation mechanisms.

319. In the immediate vicinity of the Sayreville site, nickel decreased from an average of 420 ppb for the on-site samples to an average of 325 ppb for the samples collected beneath the site, an average decrease of 22 percent (Tables 22, 23). Nickel was further attenuated down gradient to an average of 237 ppb, a net average reduction of 44 percent.

320. The highest nickel depletion was obtained at the Grand Haven site. Due to the high background concentration, the extent of leaching could not be established. However, by comparing the on-site average in Table 22 with the under-site and monitoring well averages in Table 23, it can be seen nickel decreased from 128 ppb

for the on-site samples to 65 ppb for the under-site samples. The downgradient off-site monitoring samples averaged 22 ppb, a total reduction of 83 percent over on-site values.

321. The nickel migration was probably controlled by a number of mechanisms. As the dredged material was disposed of, nickel was probably transformed from nickel sulfide into nickel carbonate due to the change in the redox conditions, resulting in more nickel release. Wakeman¹⁸³ reported an increase in nickel during dredging and open-water disposal in San Francisco Bay. An increase in the carbonate phase coupled with a decrease in the sulfide and organic phases has been observed in influent-effluent samples from dredged material disposal sites. 69,144

322. In an oxidizing environment, the nickel concentration should be controlled by NiCO_3 , and its theoretical concentration is given by:

$$[\text{Ni}] = \frac{K_{sp}}{[\text{CO}_3^{=}]^2} = \frac{10^{-8.2}}{[\text{CO}_3^{=}]^2} = 37 \text{ ppm to } 4300 \text{ ppm}$$

Nickel also forms stable complexes with chloride, carbonate, and other inorganic and organic ligands. Chen and Rohatgi¹⁸⁴ suggested that the initial release of nickel from suspended particulates upon disposal into the ocean is due to the formation of soluble chloride complexes. Complexation with soluble organic ligands can further increase the theoretical soluble nickel concentration, which is already orders of magnitude higher than the observed values (Table K1 to K4).

323. Soluble nickel was probably adsorbed by iron and manganese oxides in oxidizing environments. Pronina et al.¹⁸⁵ showed that nickel can be scavenged from seawater by naturally occurring hydroxides of iron and manganese. Goldberg¹⁸⁶ reported that nickel is linearly related to the manganese content in Pacific Ocean ferruginous sediments. The scavenging effect of iron and manganese has also been reported by many other authors. 2, 5, 158, 159

324. In a reducing environment, nickel sulfide will be the controlling solid. The ion ratio suggested that sulfide would be the controlling solid when $\text{pS}^=$ reached 16 for $(\text{NiS})\alpha$

$$R = \frac{[S^{=}]}{[CO_3^{=}]} = \frac{(K_{sp}) \alpha NiS}{(K_{sp}) NiCO_3} = \frac{10^{-18.5}}{10^{-8.2}} = 10^{-10.5}$$

or

$$R = \frac{[S]}{[CO_3]} = \frac{(K_{sp}) \gamma NiS}{(K_{sp}) NiCO_3} = \frac{10^{-25.7}}{10^{-8.2}} = 10^{-17.5}$$

As discussed in the cadmium section, if one chooses $pS^{=}$ to be 20, free Ni could be controlled by $(NiS)\gamma$, this is given by:

$$[Ni^{++}] = \frac{(K_{sp}) \gamma}{[S^{=}]} = \frac{10^{-25.7}}{10^{-20}} = 64 \text{ ppb}$$

This concentration is remarkably close to the observed nickel values.

325. In summary, soluble phase nickel was found to exist at relatively high levels in both the dredged material and soil interstitial waters at the Sayreville site. A few of the samples exceeded the NAS Marine Water Quality Standard of 1000 $\mu\text{g/l}$. Due to the high concentration found in the background samples, the extent of leaching cannot be established. It was deduced from the comparison of the on-site, under-site and monitoring well samples, that nickel was leached from the site. Nickel was also observed to have leached from the Pinto Island and Grand Haven sites. The concentrations were greatly attenuated as they traveled away from the sites. However, due to the low concentration, nickel is not anticipated to pose any threat to the groundwater quality at these two sites.

Lead

326. Although lead exists everywhere in the environment, it is extremely insoluble in water. Kopp and Kroner¹⁸⁷ surveyed 876 surface water samples and found a concentration range of 2 to 140 ppb with a mean of 23 ppb lead. About 10 percent of their samples exceeded 10 ppb.

327. Of the samples analyzed for in this study, lead existed only in minute quantities. The concentrations ranged from a low

of below 1 ppb, found for all four sites, to a high of 80 ppb, found in two Houston samples. Most samples were below 10 ppb. For the Grand haven site, 46 of the 60 samples were below 1 ppb. Only 4 of the 306 samples (from all four sites) exceeded the 50- $\mu\text{g}/\text{l}$ drinking water limit set up by EPA.¹⁸⁸⁻¹⁹¹ Compared to sources tested in Kopp and Kroner's study, it appears that dredged material disposal sites pose no danger to the groundwater quality.

328. Lead, like other trace metals, goes through different solids transformations if the redox condition is changed. Wakeman¹⁸³ reported an increase of lead during dredging operations in San Francisco Bay. However, Windom⁵ found no appreciable changes in water quality during and after dredging activities near the Intracoastal Waterway in Georgia.

329. Lead carbonate has been suggested as the controlling solid in oxidizing marine environments.¹⁹² In this study, due to the low pH and high sulfate concentration in certain samples, lead sulfate may have been the controlling solid (e.g., Sayreville). Major lead complexes include carbonate, sulfate, hydroxide and chloride.^{148,192} An activity ratio diagram for lead sulfate, lead carbonate, and lead hydroxide is given in Figure 78. Sulfate was assumed to be $10^{-2.5}$ M and the total carbon concentration to be $10^{-3.3}$ M. It is seen that below pH 6, lead sulfate is the controlling solid. From pH 6 to 11.5, lead carbonate is the controlling solid: lead hydroxide becomes important only when pH exceeds 11.5, which was not detected in any of the samples analyzed. It was calculated for this study, that, due to the ratio of sulfate to carbonate, the free lead concentration ranges would be similar, regardless of whether lead carbonate or lead sulfate was the controlling solid. The following tabulation gives the range of soluble lead under oxidizing conditions for each site and the theoretical calculations that took into account the controlling solid and ligand complexes with sulfate, carbonate, bicarbonate, and chloride:

Site	pH Range	Actual Range Lead	Theoretical Calculation
			PbCO ₃ as Control solid, $K_{sp} = 10^{-13.30}$
Sayreville	3 to 7	1 to 50 ppb	1.3 to 2 X 10 ⁷ ppb
Pinto Island	4.8 to 8.2	< 1 to 7 ppb	6.3 to 1.6 X 10 ⁶ ppb
Houston	5.8 to 7.7	< 1 to 80 ppb	20 to 2 X 10 ⁴ ppb
Grand Haven	5.4 to 7.8	< 1 to 30 ppb	

330. The theoretical values are close to the observed values at high pH. Lead adsorbs strongly with clay minerals. Adsorption of metals on clay minerals was reported to occur in the following order: Cu⁺⁺ > Pb⁺⁺ > Ni⁺⁺ > Co⁺⁺ > Zn⁺⁺. Adsorption by clay, iron, and manganese oxides probably accounted for the low lead content found in this study.

331. In summary, soluble lead was found to be in very low concentration. No leaching was observed in any sites and no leaching potential was found in any sites. It is concluded that dike disposal of dredged material will not significantly increase the soluble lead level in groundwater.

Zinc

332. Zinc is a fairly abundant element. Unlike most other trace metals, small amounts of zinc are essential to life. A large quantity of zinc is used industrially, and this has a significant impact on the distribution of zinc in the environment. Lazarus et al.¹⁹³ reported an average concentration of 107 ppb zinc in rainfall collected at 32 points in the United States from September 1966 to January 1967. Hem¹⁷⁰ surveyed 726 filtered water samples taken from rivers and lakes in the United States and found the median concentration of zinc to be close to 20 ppb,²⁰³ considerably less than the average value reported by Lazarus.

333. In this study, Sayreville had the highest average soluble zinc concentrations of 4.16 ppm in samples from the monitoring wells, 2.44 ppm for the on-site dredged material. interstitial water samples, and 3.8 ppm for the background well water. Grand Haven, being the least industrialized of the four sites, had the lowest soluble zinc average, 0.053 ppm for the monitoring well samples, 0.058 ppm

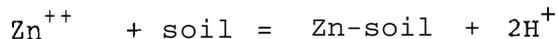
for the on-site samples, and 0.176 ppm for the background well water. Hem¹⁷⁰ suggests that industrial discharge of zinc aerosols could be the major source of zinc in rainfall in the northeastern United States. Comparing the data of Lazarus et al.¹⁹³ and Hem¹⁷⁰ it is possible that rainfall could be a source of zinc in the above sites. One other possibility for the higher off-site and background concentrations, compared to those of the on-site Sayreville samples, is the close proximity of the entire monitored area to two heavily used highways (New Jersey Highway 35 and U.S. Highway 9). Lagerwerff and Specht¹⁷² have shown that zinc, lead, cadmium, nickel, and lead concentrations increase in soil and vegetation adjacent to highways.

334. Pinto Island is the only site that showed a potential for zinc leaching from the site. The on-site average soluble zinc concentration was 0.6 ppm. The off-site monitoring well samples contained 0.072 ppm soluble zinc (Table 22).

335. The average zinc concentration decreased from 0.60 ppm in the on-site dredged material water samples to 0.41 ppm for the groundwater samples underneath the site and to 0.073 ppm for the off-site monitoring well samples. A total decrease of 88 percent was achieved. From a comparison of background, under-site, and monitoring well averages, it appears that the monitoring wells had been affected (Tables 22 and 23).

336. Like other trace metals, a number of mechanisms probably attenuate zinc as it migrates from the disposal site to the surrounding soils. These include dilution, biological effects, solids transformation, complexation and adsorption. Adsorption appeared to be the most important factor.^{173,182,193}

337. Lindsay and Norvell¹⁹⁴ proposed a zinc-soil system:



in which the zinc concentration is given by:

$$\left[\text{Zn}^{++} \right]_1 = 10^6 \left[\text{H}^{+} \right]^2$$

At pH 6, the zinc concentration is calculated to be 0.063 ppm, about five orders of magnitude less than the predicted values from solubility considerations, and is much closer to the observed values from this study.

338. To sum up, at the Sayreville and Grand Haven sites, soluble phase zinc concentrations were lower in the on-site dredged material than in the surrounding native soils. Only the Pinto Island site reflected a leaching potential. The average for the on-site Pinto Island sample was 0.61 ppm. The EPA drinking water standard for zinc is 5 ppm. Thus, it is concluded that zinc will not be a problem at the sites studied.

Iron

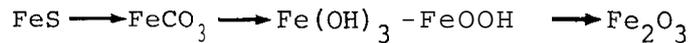
339. Iron is one of the most abundant elements or metals in the earth's crust, having an average concentration of 56,000 ppm.¹⁷⁹ In soils and sediments, iron concentrations range from a few thousand ppm to several percent.^{126,195} Similar concentration ranges were found in the soil and dredged material samples collected for this study (Tables J5 to J8).

340. Although iron is ubiquitous in nature, its availability is usually low. Most of the iron either exists as part of mineral crystal structures or as an oxide coating on the surfaces of particles.^{153,196} In this study, less than 1 percent of the total iron was found to exist in the water-soluble and exchangeable fractions.

341. In the interstitial soil water and leachates, average iron concentrations ranged from a low of 54 ppb for the Pinto Island samples to a high of 3.5 ppm for the Sayreville samples. The statistics for the other sites are given in Table 22. In general, the concentrations correlated well with redox potential and pH. Sayreville samples had relatively low Eh and pH. These conditions are known to favor mobilization of iron.¹⁹⁶⁻¹⁹⁸ Pinto Island and Grand Haven samples had higher Eh and pH values and, consequently, lower iron concentrations.

342. Student's "t" tests showed that the differences in iron concentrations between the on-/off-site Sayreville samples, and between the on-/off-site Pinto Island samples were statistically insignificant (p value of > 0.9 and 0.45, respectively). An average on-site sample was higher than the average off-site sample at Grand Haven by 29 ppb, creating a leaching potential. However, except for the Sayreville samples, all were below the 0.3 ppm drinking water limit set up by EPA.¹⁸⁸⁻¹⁹¹

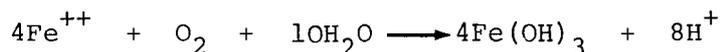
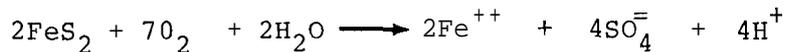
343. Iron solubility is very sensitive to Eh and pH. Gotoh and Patrick¹⁹⁹ and Gambrell et al.¹⁹⁷ demonstrated that, in water-logged soil and sediments at a fixed pH, an increase in soluble iron is associated with a decrease in redox potential. At a fixed redox potential, an increase in soluble iron is associated with a decrease in pH. Lu¹⁴⁸ proposed that iron is transformed during a change from reducing conditions to aerobic conditions through the following stages:



The wide range of soluble iron concentrations found in this study was probably due largely to the various localized conditions signified by different controlling solids. However, simple solubility calculations predict a much lower concentration than the observed values. Organic complexation is the most likely candidate to account for the gap.^{182, 200}

344. A few spots of high iron concentration were found at some monitoring stations at Sayreville. For the first sampling period, samples from background well (NJJ) contained 2500 ppm which gradually decreased to 0.17 ppm during later sampling periods. One of the off-site wells (NJG1) also had a high concentration (71 ppm) in the first sample set, which later decreased to 0.1 ppm. Another background well (NJI) decreased from 39 ppm to 0.3 ppm. An on-site sample (NJA3) and an under-site groundwater sample (NJB4) exhibited similar trends. An increase in pH in these samples was also recorded (NJJ increased from 3 to 7.2, NJG1 increased from 3 to 6.4, and NJI increased from 3 to 4.6).

345. The low pH and high soluble iron levels in the sediments at Sayreville were probably caused by the oxidation of pyrite to sulfate in the poorly buffered sediments. As air infiltrates soil, the oxidation of sulfide to sulfate proceeds as a two-stage process, resulting in an acidic soil solution:



The oxidation process seems plausible since the high iron levels measured during the first sampling could be due to the inclusion of fine particulate ferric hydroxide colloids or ferrous organic complexes. The oxidation process is a very rapid reaction. However, if complexed with organic matter, the oxidation of ferrous to ferric ion could be delayed by days or even months.²⁰⁰

346. In conclusion, iron transport was highly influenced by the Eh-pH of the environment, solid transformation and complexation. Soluble iron levels in the dredged material were either comparable to the surrounding environment (the Sayreville and Pinto Island sites), or were low compared with the EPA drinking water standards (the Pinto Island and Grand Haven sites). It is concluded that diked disposal of dredged material will pose no groundwater iron problem.

Manganese

347. Manganese was the most soluble element among the trace metals studied. Out of the more than 300 samples analyzed, only a few were below 0.05 mg/l, the drinking water limit set up by EPA.¹⁸⁸⁻¹⁹¹ On-site averages for dredged material water samples were 1.2 ppm for the Grand Haven site, 6.4 ppm for the Sayreville site, 9.2 ppm for the Pinto Island site, and 12.3 ppm for the Houston site (Table 22). Average off-site leachate samples were also at the ppm level and ranged from a low of 1.2 ppm for the Pinto Island site to a high of 7.4 ppm for the Sayreville site (Table 22). The highest individual analysis was 68 ppm and the lowest was 0.5 ppb; both samples were found in the Pinto Island vicinity.

348. The chemical behavior of manganese is quite similar to that of iron. Like iron, manganese is almost ubiquitous in soils and sediments, the solubility is highly dependent on the redox potential and pH. As discussed before, both the redox potential and pH are highly site-specific. Although the chemistry and mineralogy of most manganese solids is not well understood, it is generally considered that, under reducing conditions, manganese will exist as sulfides or silicates. Carbonate, hydroxide, and oxide solids tend to form as the redox potential is raised.⁻⁷⁴

The solubility of each solid is unique, and manganese is generally more soluble than its iron counterpart. Thus, the wide range of soluble manganese observed and the nonsignificant difference between the on-/off-site New Jersey and Grand Haven samples were expected. In general, high soluble manganese concentrations were associated with low Eh or high pH. Iron usually precipitates at a lower Eh and/or pH than manganese. It is possible that the case study sites had Eh/pH conditions that promoted the formation of manganese carbonate, which is generally favored by reducing conditions and high pH. However, iron may have still existed in the very poorly soluble oxidized form, Fe(III).

349. Assuming manganese carbonate as the controlling solid, the free manganese concentration is given in Figure 76. It ranged from a few ppm to several thousand ppm. Manganese also forms stable complexes with chloride, bicarbonate and some soluble organic molecules. This will increase the total soluble manganese concentration. Sorption with clay minerals or soil organic matter probably brings the concentration to the observed range.¹⁶⁸

350. The importance of iron and manganese oxides in regulating the transport of trace metals has been mentioned in other sections. In the reduced form neither iron nor manganese is an effective trace metal scavenger. As the conditions become more oxidizing, iron and manganese may eventually be oxidized to ferric oxide and manganese dioxide. This oxidation could occur when reduced sediments are dredged, mixed with overlying oxygen-rich water, and disposed in an upland disposal site where atmospheric oxygen has a better chance for infiltration. These solids are characterized by high surface areas and are effective in scavenging other heavy metals from solution.^{186,197} Freshly precipitated oxides and hydroxides seem to be more effective in scavenging trace metals.¹⁸⁶

351. In conclusion, among the trace metals analyzed manganese was found to be the most soluble element. Most samples exceeded the EPA drinking water standard of 0.05 mg/l. Manganese migration was controlled to a large extent by the Eh-pH of the surrounding environment. This would make manganese a potential groundwater problem.

Mercury

352. Mercury concentration in the samples was determined by the cold vapor method. Compared to the other metals analyzed, the mercury was relatively more uniform in distribution, mostly in the sub-ppb range. Average on-site concentrations ranged from 0.34 ppb for Pinto Island and Sayreville to 0.48 ppb for Houston. The highest concentration detected was 3 ppb, found at Houston. This is slightly higher than the 2 ppb drinking water standard set up by EPA.¹⁸⁸⁻¹⁹¹ Nevertheless, of the 200 samples collected from the four sites, only 2 exceeded this limit. This range is comparable to the findings of the U. S. Geological Survey which reported <0.1 to 6 ppb mercury for selected streams in the U. S.²⁰² It is thus concluded that mercury should not pose any danger if the ground-water is to be used for drinking purposes.

353, The solids controlling the solubility of mercury are mercury sulfide (HgS) in the reduced environment and mercury hydroxide (Hg(OH)₂) in the oxidized environment. The solubility product constants of these two solids are 10^{-53.9} and 10^{-25.4}, respectively. These are about 10 to 20 orders of magnitude lower than the solubility of the controlling solids of other trace metals in the corresponding redox environments. The free mercury level is given by:

$$Hg_f = \frac{10^{-53.9}}{[S_I^-]} \quad \text{or} \quad \frac{10^{-25.4}}{[OH^-]^2}$$

Assuming a total sulfide concentration of 10⁻⁹M, the following tabulation summarizes the theoretical values of free Hg⁺⁺ at various pH levels:

<u>pH</u>	<u>Hg(OH)₂ Control, ppb</u>	<u>HgS Control, ppb</u>
3	8.24 X 10 ⁴	10 ^{-21.6}
4	8.24 X 10 ²	10 ^{-23.6}
5	8.24	10 ^{-25.6}
6	8.24 X 10 ⁻²	10 ^{-27.6}
7	8.24 X 10 ⁻⁴	10 ^{-29.6}
8	8.24 X 10 ⁻⁶	10 ^{-31.6}

354. Mercury forms stable complexes with hydroxide, chloride, and other inorganic and organic ligands. The stability constants for hydroxide complexes have been reported to be

$$\log \beta_1 = 10.8, \quad \log \beta_2 = 22.4, \quad \log \beta_3 = 10^{21.63} \cdot 78$$

The contribution of this ligand alone to the total mercury concentration will be:

$$\left[\text{Hg}^{+2} \right]_{\text{Total}} = \text{Hg}_f \left\{ \beta_1 [\text{OH}] + \beta_2 [\text{OH}^-]^2 + \beta_3 [\text{OH}^-]^3 \right\}$$

Thus, $[\text{Hg}^{+2}]_{\text{total}}$ will be increased more than two orders of magnitude if the pH increases by one unit.

355. Organic ligands are expected to increase the solubility of mercury even further. Fuller¹⁵³ stated that, for the most part, mercury attenuation or movement in soil must relate to organic carbon or sulfur chemistry, either separately or together as humic substances containing sulfur. Lu¹¹⁵ and Lisk¹¹⁸ compiled information on the solubility of several trace metals. The stability constant of Hg(II) - EDTA was reported to be $10^{21.8}$, and $\log \beta_1$ and $\log \beta_2$ of Hg(II) - cysteine were reported to be 46.2 and 20.7, respectively.¹⁰⁵

356. It is impossible to assess the exact effect of soluble organics on metal concentrations because the nature of the organic compounds in natural waters is not yet fully understood. Nevertheless, based on the thermodynamic data on the synthetic organic molecules, it is expected that the metal concentrations will be increased by many orders of magnitude compared to the solubility product constants of the controlling solids.

357. Complexation with soil organic matter and adsorption onto inorganic sediment fractions may account for the low mercury concentrations detected in this study. Jenne¹⁵⁹ proposed that the adsorption of mercury, in the form of mercury-chloride complexes, onto hydrous oxides or iron and manganese may be the controlling mechanism in seawater. The scavenging effect of manganese oxides on mercury was also studied by Lockwood and Chen²⁰³ and Krauskopf.¹⁵⁸ Both reports indicate that adsorption onto hydrous oxides of manganese is an important factor regulating soluble

mercury levels. Lindberg and Harris²⁰⁴ found that mercury was released from resuspended near shore sediments. A peak of 1.6 ppb was observed which decreased to 0.2 ppb. Mercury may be released during dredging operations.⁵ Upon disposal on upland sites, it is expected that mercury will be immobilized by the organic matter and/or scavenged by manganese and iron oxides.

358. In summary, soluble mercury levels observed were generally in the sub-ppb range. The on-site dredged material mercury levels were similar to the off-site soil mercury levels. Hence, there was no leaching potential in the study sites. Adsorption was probably the greatest attenuation mechanism in reducing the mercury levels. It is concluded that diked disposal of dredged material will not make mercury a groundwater problem.

PART IV: CONCLUSIONS AND RECOMMENDATIONS

359. Analytical results of the field leachate study indicate that upland dredged material disposal should be a carefully controlled practice. Under certain conditions, leachates from upland disposal areas may degrade underlying site groundwaters. It has been demonstrated that potential adverse water quality impacts will most likely be due to the increases of chloride, potassium, sodium, calcium, total organic carbon, alkalinity, iron, and manganese. The extent of the potential impact was found to be functions of the physiochemical properties of the disposed dredged material, site-specific groundwater hydrogeological patterns, and environmental conditions of the area surrounding the site. The field monitoring of the case study sites revealed low concentration levels of cadmium, copper, mercury, lead, zinc, phosphate, and nickel may reach groundwaters; however, concentrations of these constituents were detected at levels that should not pose water quality problems.

360. Results of the bulk sediment analysis of dredged material and soil were similar from each of the case study sites. This was not the case, however, with soluble and exchangeable fractions, indicating bulk analysis is probably not a suitable tool for evaluating upland dredged material disposal. In general, the examination of vertical and lateral differentiations of dredged material within each of the case study sites failed to reveal any systematic changes. For any particular parameter, both increases and decreases in values occurred at different locations as well as at different depths within each site. Results of the particle size analysis of the dredged material suggested that the material in upland disposal areas is slightly more sandy than original bottom sediments. The reason for the difference might be due to the fact that finer particles tend to be carried with effluents to receiving waters due to insufficient residence time and/or turbulence.

361. In analysis of the interstitial water of the dredged material at each of the case study sites, no soluble chlorinated hydrocarbons/pesticides were detected. It is likely that these contaminants will probably not migrate from upland dredged material

disposal areas. However, this was not the case for many other parameters. Concentrations in the soluble phase of the water samples obtained from groundwaters below and downgradient from the case study sites showed that chloride, sodium, and potassium could pose problems to water quality. The dilution effect was found to be the major mechanism which controlled concentration of these constituents in leachates. Ion exchange was also found to regulate sodium and potassium levels. High levels of chloride in the leachates from sites containing saline dredged material may present water quality problems should leachates and/or impacted groundwaters be discharged to freshwater environments.

362. Analytical results from the field study indicate that both saline and freshwater upland dredged material disposal sites can increase the concentrations of calcium and magnesium in underlying site groundwaters. It was found that the concentration of calcium was controlled by ion exchange and dissolution of calcite. The possible controlling mechanisms for magnesium migration were dissolution of magnesium solids and ion exchange. The increase of hardness (mostly for calcium and magnesium), will reduce the utility of water for many beneficial uses.

363. Alkalinity levels in leachates were found to be increased, possibly due to dissolution of calcite, as well as biological action. TOC exhibited trends in mobility that were similar to alkalinity. Levels of TOC in leachates were affected by biological action and interactions with clay minerals. High levels of TOC in leachates pose many unknown effects. TOC in leachates may serve to mobilize trace metals from underlying site soils.

364. It can be concluded from data of trace metals that only manganese and possibly iron should pose water quality problems in upland dredged material disposal. Levels of the two constituents in on-site leachate samples and downgradient groundwater samples often exceeded EPA drinking water standards by a wide margin. Both iron and manganese levels were related to Eh and pH values of the various water samples. Eh and pH of the surrounding site environment, solid transformation, and complexation with organic matter all affect the soluble concentrations of iron and manganese.

365. Analytical results indicated that phosphate, cadmium, copper, lead, nickel, mercury, and zinc should not pose potential problems for groundwater as a result of upland dredged material disposal. The controlling mechanisms for phosphate and many of the trace metals was adsorption. Complexation and precipitation/dissolution also played a role in regulating these trace metal concentrations in leachates. From these results, it is felt that native soils in areas to be developed as dredged material disposal sites should have high sorptive capacities. This will help minimize the trace metal mobilization problems.

366. From the preceding discussion, it can be seen that leachates from upland dredged material disposal could have caused degradation of local groundwaters at the case study sites evaluated in this study. Upland dredged material should be a carefully controlled practice. In light of this, it is recommended that topics to be pursued are as follows:

- chronological extension of field leachate study at case study sites.
- ✕✕ determination of the physical area of influence of the leachate plume from actual case study sites.
- monitoring of groundwaters surrounding existing confined disposal sites.
- ✕✕ instigation of leaching studies over extensive time periods.

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TABLE 1. PERCEIVED PHYSICAL CHARACTERISTICS AT GRAND HAVEN, MICHIGAN

Topographical Setting	Hydrological Setting	Dredged Materials		Size Characteristics			
		Material Matrix	Origin	Aquatic Environment	Setting	Size	Depth
Located on the banks of Grand Haven Harbor in Michigan; harbor empties into Lake Michigan \approx 2 mi from the site.	Low gradient groundwaters flowing through the site and into the harbor and low marsh area to NW.	Silts and sands	Harbor at Grand Haven	Freshwater	Wind-blown sands: uniform clay at 6 m (20 ft)	2.42 ha (6 ac)	1.5 m (5 ft) to 3 m (10 ft) prior to 3/77
							2.1 m (7 ft) to 3.9 m (13 ft) after 3/77

TABLE 2. FIELD INVESTIGATIONS AT GRAND HAVEN, MICHIGAN

Date of Field Investigation	Specific Hydrological Studies Performed	Physical Conditions at the Site
November 4, 1976	<p>Initial reconnaissance; surface hydrological features studied (drainage, ditches, phreatophyte study, topographic features, etc.).</p> <ul style="list-style-type: none"> ● Resistivity survey conducted. ● Installation of nine 1-1/4-in metal well points, one on-site/eight off-site; wells developed, labeled, painted, and surveyed for absolute elevation; series of water level readings obtained from each well point and plotted with time vs. water level to define effect of Grand River upon water well measurements. Contours plotted and prospective pumping well locations studied. Boring logs were made and representative samples obtained for laboratory testing. 	<p>Little on-site vegetation; snowing during visit.</p>
December 1, 1976	<ul style="list-style-type: none"> ● Sampling devices placed; four stations on-site/six off-site. Wells developed, labeled, painted, and surveyed for absolute elevation. Series of water level measurements taken in sampling devices and well points. ● One 6 m (50 ft) pumping well (MP) and one 6 m (50 ft) observation well (MO) installed; boring logs recorded. ● Water samples collected from sampling devices. 	<p>Snow and extremely cold temperature.</p>

(continued)

TABLE 2. (continued)

Date of Field Investigation	Specific Hydrological Studies Performed	Physical Conditions at the Site
April 8, 1977	<ul style="list-style-type: none"> ● Pumping test wells and two monitoring well points were installed within the confines of the dredged material. ● Pumping tests attempted within the dredged material, but failed due to clogging of the well by dredged sediments. ● Water level elevations obtained from well points and sampling devices. ● Water samples obtained from sampling devices. ● Extensions to on-site monitoring devices performed 	<p>Dredging onto site was occurring. On-site area completely ponded with water and several feet of sediments.</p>
May 30, 1977	<ul style="list-style-type: none"> ● Water samples obtained along with level elevations recorded from the well points and monitoring wells. 	<p>Site dewatered; dikes bulldozed leaving entire site level.</p>
August 5, 1977	<ul style="list-style-type: none"> ● Water samples obtained along with water level elevations recorded from the well points and monitoring wells. 	<p>Raining during visit: luxuriant on-site vegetation; up to 2.4 m (8 ft) the southern area; entire site covered with vegetation.</p>

TABLE 4. PERCEIVED PHYSICAL CHARACTERISTICS AT SAYREVILLE, NEW JERSEY

Topographical Setting	Hydrological Setting	Material Matrix	Origin	Aquatic Environment	Geologic Setting	Size	Depth
East coast of New Jersey: located at the tip of a small peninsula bordered by the Raritan River, The Raritan River empties into Raritan Bay and then into the Atlantic Ocean: 5 mi to the east.	Groundwaters manifested in standing water in salt marsh. Effect of tide influences the hydraulic gradients and innundates low lying marsh areas. Groundwater may be mounded under the site.	Silts and Clays	Raritan River	Salt water	Quaternary river deposits	17 ha (44 ac)	5.1 m (17 ft) to 7.9 m (26 ft)

TABLE 5. FIELD INVESTIGATIONS OF SAYREVILLE, NEW JERSEY

Date of Field Investigations	Specific Hydrological Studies Performed	Physical Conditions at the Site
November 12, 1976	<p>Initial reconnaissance; surface hydrological features mapped (i.e., streams, drainage ditches, phreatophyte survey, topographic features affecting site).</p> <ul style="list-style-type: none"> ● Ten 1-1/4-in well points (two on-site/eight off-site) installed; wells developed, labeled, painted, and surveyed for absolute elevation; series of water level readings obtained from each well point and plotted with time vs. piezometric level to define effect of tide upon water well measurements. Contours plotted and prospective pumping well locations studied. Boring logs made and representative samples obtained for laboratory testing. 	<p>Wet from recent rain; little on-site vegetation.</p>
November 28, 1976	<ul style="list-style-type: none"> ● On-site sampling devices placed; four stations on-site/six off-site. Wells developed, labeled, painted, and surveyed for absolute elevation. Series of water level measurements taken in sampling devices and well points. ● One 15 m (50 ft) pumping well and one 15 m (50 ft) observation well installed; boring logs recorded; preliminary pumping test performed. ● Water samples collected from sampling devices. 	<p>Snowing and raining during sampling</p>

(continued)

TABLE 5. (continued)

Date of Field Investigations	Specific Hydrological Studies Performed	Physical Conditions at the Site
November 28, 1976 (con'd)	<p>☞ Pumping test wells and two monitoring well points installed within the confines of the dredged material.</p> <p>• Pumping test attempted within the dredged material, but failed due to clogging of well by dredged sediments.</p>	Dredging site being prepared for dredging; dike height increased.
April 6, 1977	<p>☞ Water level elevations obtained from well points and sampling devices.</p> <p>● Water samples obtained from sampling devices.</p> <p>☞ Extensions to on-site monitoring devices performed.</p>	Dredging occurring; several feet of water covering the entire site along with several feet of sediment.
June 2, 1977	<p>☞ Water level elevations obtained from well points and sampling devices.</p> <p>☞ Water samples obtained from sampling devices.</p>	Light rain; no on-site vegetation.
August 5, 1977	<p>☞ Water level elevations obtained from well points and sampling devices.</p> <p>☞ Water samples obtained from sampling devices.</p>	

TABLE 7. PERCEIVED PHYSICAL CHARACTERISTICS AT HOUSTON, TEXAS

Togographical Setting	Hydrological Setting	Dredged Materials		Size Characteristics		
		Material Matrix	Origin	Aquatic Environment	Geologic Setting	Size
Upland area	Essentially an artificial system within the site: disposal pond underlain by native clays: perched water above clays moves through dredged material and collects in surface ponds in the north section.	Clays and sands	Houston Ship Channel	Saline and Freshwater	Geosyn-clinal area; native sediments	111 ha (275 ac) to 10 m (35 ft)
					Quarternary sands and clay; Houston clay predominates at surface in vicinity	

TABLE 8. FIELD INVESTIGATIONS AT HOUSTON, TEXAS

Date of Field Investigation	Specific Hydrological Studies Performed	Physical Conditions at the Site
November 6, 1976	<p>Initial reconnaissance: surface hydrological features mapped (i.e., streams, drainage ditches, phreatophyte survey, topographic features affecting site).</p> <ul style="list-style-type: none"> ● Installation of 10 3.1 cm (1-1/4-in) well points, 2 on-site/8 off-site; well developed, labeled, painted, and surveyed for absolute elevation; series of water level readings obtained from each well point and plotted as time vs. water level to define fluctuations in wells with other site variables (e.g., ponding). Contours plotted and prospective pumping well locations studied. Boring logs were made and representative samples obtained for laboratory testing. 	<p>On-site vegetation scarce; essentially bare; approximately 1/2 site flooded</p>
December 7, 1976	<ul style="list-style-type: none"> ● On-site sampling devices placed; four on-site/six off-site. Well developed, labeled, painted, and surveyed for absolute elevation. Series of water level measurements taken in sampling devices and well points. ● Two 10 m (35 ft) off-site pumping wells and one 10 m (35 ft) observation well installed; boring logs recorded; preliminary pumping test performed. ● Water samples collected from sampling devices. 	<p>Little on-site vegetation; ponded water reduced from previous visit.</p>

(continued)

TABLE 8. (continued)

Date of Field Investigation	Specific Hydrological Studies Performed	Physical Conditions at the Site
December 7, 1976 (con'd)	<p>## Pumping test well and one monitoring well were installed within the confines of the dredged material.</p> <p>## Two pumping test wells and one monitoring well were installed off-site.</p> <p>. Pumping test attempted within the dredged material, but failed due to clogging of the well by dredged sediments.</p>	Conditions unchanged.
March 25, 1977	<p>## Water level elevations obtained from well points and monitoring devices.</p> <p>## Water samples obtained from sampling devices.</p>	<p>On-site vegetation dense; in some areas as much as 7 or 8 ft. On-site wells difficult to locate.</p>
June 12, 1977	<p>## Water level elevations obtained from well points and monitoring wells.</p> <p>## Water samples obtained from sampling devices.</p> <p>## Off-site pumping test conducted.</p>	<p>On-site vegetation extremely humid.</p>
July 30, 1977	<p>## Water level elevations obtained in well points and monitoring wells.</p> <p>## Water samples collected.</p>	

TABLE 10. PERCEIVED PHYSICAL CHARACTERISTICS AT PINTO ISLAND, ALABAMA

Topographical Setting	Hydrological Setting	Dredged Materials		Site Characteristics			
		Material Matrix	Origin	Aquatic Environment	Geologic Setting	Size	Depth
Man-made island	Essentially a radial flow from center of island	Sands and Silts	Mobile Bay	Salt	Sands or Silts	50 ha (125 ac)	4.5 m to 60 m (20 ft)

TABLE 11. FIELD INVESTIGATIONS AT PINTO ISLAND, ALABAMA

Date of Field Investigations	Specific Hydrological Studies Performed	Physical Conditions at the Site
January 17, 1977	<p>Reconnaissance of site's hydrology (drainage ditches, phreatophytes, topography). On-site sampling devices placed; four on-site, six off-site. Wells developed, labeled, painted, and surveyed for absolute elevation. Series of piezometric measurements obtained from sampling devices. Water samples collected from sampling devices.</p>	<p>Vegetation scarce. Snowed during the installation of the monitoring devices.</p>
March 26, 1977	<p>Piezometric elevations obtained from sampling devices. Water samples obtained.</p>	<p>Dredging conducted during visit; on-site wells above ponded waters; discharge pipe located northwest corner of the site; moved to area \approx 200 ft west of DI-D.</p>
June 7, 1977	<p>Piezometric elevations obtained from sampling devices. Water samples obtained.</p>	<p>Site dewatered significantly from previous visit.</p>
August 1, 1977	<p>Piezometric elevations obtained from sampling devices. Water samples obtained. Off-site pumping test conducted.</p>	<p>Light rains; area very dry.</p>

TABLE 13.
SHIPPING/SAMPLING CATEGORIES AND
POTENTIAL METHODOLOGIES EVALUATED

General Categories	Potential Methodologies (Ref.)
A. Dredged Material Sampling	
1. Coring	Post hole digger (22,23,30) Hand auger (22,23,25,30) Power auger (23,24,25,26,50) Truck mounted drilling rig (28,34,35,59) Hydraulic porta-sampler(22,61) Water jetting (29, 36, 50, 57, 56) Excavation (50)
2. Collection	Denison sampler (22,49,50,62) Osterberg piston sampler (22, 49, 50,58) Hand piston sampler (22,49,50,62) Posthole auger (49,65) Split tube sampler (49,61,62) Sand pump sampler (34,48,61) Split-spoon with trap valve(22,36,61,62)
B. Background Soil Sampling	
1. Coring	Posthole digger (22,50) Hand auger (22,25,50) Power auger (23,24,26,50) Truck mounted drilling rig (28, 34, 35,49) Hydraulic porta-sampler (22,61) Excavation (50)
2. Collection	Denison sampler (22,49,60,62) Osterberg piston sampler (49,60,62) Hand piston sampler (22,47,60,62) Posthole auger (49,65) Split tube sampler (22,49,61,62) Sand pump sampler (24,48,61) Split spoon with trap valve (22, 36,61,62)
C. Interstitial and Groundwater Sampling	
1. Interstitial	Pressure/vacuum lysimeter (27,34,38,39,43,46,63)

(Continued)

TABLE 13. (Continued)

General Categories	Potential Methodologies (Ref.)
C. Interstitial and Groundwater Sampling (cont'd)	Soil water sampler (52,55,56) Hand vacuum pump (40,51,64) Gas driven vacuum pump (43,44,51,64)
1. Interstitial Water	Electric vacuum pump (43, 44, 51,64, 67)
2. Groundwater	PVC well point (27,34,37,42,47,55, 56) PVC well with screen (27,37,45,55) Metal well point (37, 45,55) Pitcher pump (32,52,55) Johnson portable sampler (30,31,32, 33,53) Bailing method (48,54,55,64) Pressure/vacuum system (64,67) Gas driven vacuum/pressure pump (43,44,51) Electric vacuum pump (43,44,51, 64, 67)
D. Sample Containers for Soils, Dredged Materials and Water	
1. Selection	
Soils	Glass containers/bottles Plastic bottles Grab bags Soil tubes (PVC metal)
Dredged Material	Grab bags Soil tubes Plastic bottles Glass containers
Water samples	Glass bottles Plastic bottles
2. Preparation	Acid wash Rinsing
E. Shipping Procedures	
1. Soils	Air freight routing Shipping boxes (Styrofoam, wooden ice chests, etc.)

(Continued)

TABLE 13. (Concluded)

General Categories	Potential Methodologies (Ref.)
E. Shipping Procedures (con'd)	
2. Water	Air freight routings Ice chests Styrofoam boxes Wooden boxes

TABLE 14.
SELECTED SHIPPING AND SAMPLING METHODOLOGIES

General Categories	Potential Methodologies
A. Dredged Material Sampling	
1. Coring	Hand Augers
2. Collection	Present techniques inadequate
B. Soil Sampling	
1. Coring	Hand augers
2. Collection	Present techniques inadequate
C. Interstitial and Groundwater Sampling	
1. Interstitial	Pressure/vacuum lysimeter
2. Groundwater	PVC well point
D. Sample Containers for Soil/ Dredged Material & Water	
1. Selection	
Soils	Present techniques inadequate
Dredged Material	Present techniques inadequate
Water Samples	Glass/plastic
2. Preparation	
Soils	Acid wash
Dredged Material	followed with
Water Samples	distilled water
Collection devices	rinse
3. Shipping	
Soil	Air freight plastic sample
Water	tubes in wooden boxes, air
	freight sample bottles in
	ice chest and cardboard, styro-
	foam-lined boxes

TABLE 15. SAMPLE CONTAINERS AND PREPARATION

<u>Water Samples</u>			
Size	Material	Preparation Procedures	Test Performed
250 mL	Polvethvlene bottle	Soaked in 5 per- cent HNO ₃ for 24 hr rinsed with ultra-pure water	Trace metals
125 mL	Polyethylene bottle	Rinsed several times with dis- tilled water; 5ml of zinc acetate added for fixation	Sulfides
500 mL	Glass bottle	Rinsed twice in distilled water	Miscellaneous constituents
<u>Dredged Material</u>			
.9 m X 7 cm (3' X 3") ID Tube	ABS	Acid rinse with 7 percent HCl. Rinsed twice with distilled water	
<u>Soil Samples</u>			
.9 m X 7 cm (3' X 3") ID Tube	ABS	Sames as for dredged materials	

TABLE 16. PREPARATION OF FIELD EQUIPMENT

Item	Function	Preparation Procedures
Pressure/vacuum lysimeter	Collects interstitial water	Soaked in 5 percent HCl solution for 14 hr, rinsed twice with distilled water: once with ultra-pure
Pressure/vacuum lysimeter tubing	Sample water drawn through tubes from lysimeter into collection bottle	Same as for lysimeter preparation
PVC well points	Groundwater collection	Rinsed twice with distilled water
Glass water collection	Water collected from subsurface devices into this bottle	Soaked in 5 percent HCl solution; rinsed twice with distilled water and once with ultra-pure water
Polyethylene tubing	Water drawn through tubing into glass collection bottle	Same as for lysimeter preparation

TABLE 17. PHYSICAL CHARACTERISTICS OF FOUR CASE STUDY SITES

Site	Surface Flow Patterns	Groundwater Flow Patterns	Native Soils & Geologic Age	Topographical Setting	Geographical Location	Dredged Material Origin	Annual Average Precipitation	Dredged Area	Material Depth
Sayreville, N. J.	From NW to ponded area in E. sector; drain-age to Raritan River from NE sector. Porded; flow from effluent river to Raritan River.	Radial flow from site; perched condition; complex model.	Unstratified Quaternary sands & silts (Ref.18)	Upland; adjacent to Raritan River.	East coast	Salt-wedge estuary and river-rine	48" (Ref. 8)	44 ac	25' to 30'
Grand Haven, Mich.	From N to S; drainage to Grand River from SW corner; no ponding-Flows across site and into bay through river	Gentle, gradient flowing thru site & toward river.	Aeolian sands; uniform clay at 20'; fractured Paleozoic sandstone and shale bedrock (Ref.11)	Peninsula	North-east	Freshwater	32" (Ref. 8)	6 ac	5' to 10'

(Continued)

TABLE 17. (Concluded)

Site	Surface Flow Patterns	Groundwater Flow Patterns	Native Soils & Geologic Age	Topographical Setting	Geographical Location	Dredged Material Origin	Annual Average Precipitation	Dredged Area	Material Depth
Houston, Tex.	From S & SE upland to pond in N sector; drainage to ditch thru weirs at N end of site. Flows across site and ponds.	Local isolated system; area underlain by native clays; perched water above clays moves thru dredged material, toward ponded area.	Clays of low permeability, isolating site from regional aquifer. (Ref. 19)	Upland; inland site	South	Mixed brackish & fresh-water conditions (ship channel)	60" (Ref. 8)	275 ac	20' to 35'
Pinto Island, Ala.	From N and NW to shallow ponding along E & S sections; drainage to Mobile Bay from S end of site. Flows across site and ponds.	Essentially a radial flow away from the site.	Interstratified recent sands and silts; mostly sand off-site (Ref. 21)	Island in Mobile Bay	South-east	Salt-wedge estuary & riverine	64" (Ref. 8)	65 ac	15' to 20'

TABLE 18. HYDRAULIC CONDUCTIVITY VALUES

Parameter	Site and Location	Number of Samples	Range	Mean	Standard Deviation
Grand Haven	BG	2	9.1×10^{-4} - 1.4×10^{-3}	1.2×10^{-3}	
	OS	12	1.2×10^{-6} - 3.0×10^{-3}	2.7×10^{-4}	8.6×10^{-4}
	Mw	8	6.6×10^{-6} - 5.2×10^{-3}	1.8×10^{-3}	2.2×10^{-4}
Sayreville	BG	2	7.3×10^{-5} - 4.5×10^{-3}	2.3×10^{-3}	
	OS	12	2.5×10^{-7} - 2.1×10^{-5}	5.1×10^{-6}	5.7×10^{-6}
	Mw	8	3.2×10^{-7} - 1.4×10^{-4}	3.3×10^{-5}	4.5×10^{-6}
Houston	OS	26	1.5×10^{-8} - 2.1×10^{-4}	1.8×10^{-5}	4.4×10^{-5}
	BG	1	-----	3.6×10^{-5}	
	OS	12	8.6×10^{-7} - 1.4×10^{-4}	7.1×10^{-5}	1.0×10^{-4}
Pinto Island	OS	12	5.4×10^{-7} - 9×10^{-5}	3.7×10^{-5}	3.5×10^{-5}
	Mw	9			

TABLE 19. STATISTICAL CHARACTER OF
DREDGED MATERIAL/SOIL SAMPLES

Parameter	Site and Location	Number of Samples	Range	Mean	Standard Deviation		
pH	Grand Haven	BG	1		6.8		
		OS	12	4.7-8.0	6.7	0.9	
		MW	7	4.6-7.4	6.5	1.0	
	Sayreville	BG	21		7.3		
		OS	10	5.7-.76	6.8	0.8	
		Mw	7	6.0-7.5	6.6	0.6	
	Houston	BG	26	6.3-7.2	6.7	0.4	
	Pinto Island	BG	1		7.6		
		OS	12	5.1-7.2	6.5	0.8	
		Mw	9	6.4-7.6	7.0	0.4	
	Eh, mV	Grand Haven	BG	21		185	
			OS	12	-249-+290		
Mw			8	177-+253			
Sayreville		BG	1		350		
		OS	11	-360-+284			
		MW	7	-260-+346			
Houston		OS	26	-254-+102			
Pinto Island		BG	1		+214		
		OS	12	-232-+353			
		Mw	9	- 82-+368			
Cation exchange capacity meq/100 g		Grand Haven	BG	2	1-2	1.5	
			OS	12	8-84	42	27
	Mw		8	1-58	19	19	
	Sayreville	BG	2	6-61	33		
		OS	12	7-77	55	25	
		Mw	8	9-66	47	18	
	Houston	OS	26	1.9-21	14	11	
	Pinto Island	BG	1		1.8		
		OS	12	0.54-51	11	18	
		Mw	9	0.45-29	8.9	11	

(Continued)

TABLE 19. (Continued)

Parameter	Site and Location		Number of Samples	Range	Mean	Standard Deviation
Oil and grease, mg/kg	Grand Haven	BG	2	456-481	469	
		OS	12	279-3891	1747	
		Mw	8	122-1759	766	870
	Sayreville	BG	2	224-2961	1592	
		OS	12	247-5460	2327	1650
		Mw	8	400-5252	3070	1679
	Houston	OS	26	169-4505	1131	1116
	Pinto Island	BG	1		555	
		OS	12	351-4370	1358	2109
		Mw	9	382-938	512	169
	Grand Haven	BG	2	405-721	536	
		OS	12	272-5078	1718	1478
Mw		8	135-2028	923	642	
Grand Haven	BG	2	405-721	563		
	OS	12	272-5078	1718	1478	
	Mw	8	135-2028	923	642	
Total phosphorus, mg/kg	Sayreville	BG	2	1580-1642	1611	
		OS	12	395-2336	1490	787
		Mw	8	202-3493	1662	1245
	Houston	OS	26	379-3142	1281	864
	Pinto Island	BG	1		555	
		OS	12	351-4370	1358	2109
Mw		9	382-938	512	169	
Moisture equivalent (percent)	Grand Haven	BG	2	3-7	5	
		OS	12	8-86	43	33
		Mw	8	2-72	24	31
	Sayreville	BG	2	5-58	32	
		OS	12	4-83	65	22
		Mw	8	45-87	74	14
	Houston	OS	26	6-38	20	9
	Pinto Island	BG	1		3	
		OS	12	3-38	14	13
		Mw	9	3-47	16	16

(Continued)

TABLE 19 . (Continued)

Parameter	Site and Location	Number of Samples	Range	Mean	Standard Deviation		
Total organic carbon (percent)	Grand Haven	A	2	0.23-0-61	0.42		
		B	12	0.60-11.3	3.8	3.3	
		C	8	0.01-8.5	2.5	3.3	
	Sayreville	A	2	0-48-1.4	0.94		
		B	12	0.02-2.8	1.4	0.95	
		C	8				
	Houston	B	26	0.01-1.1	0.27	0.27	
	Pinto Island	A	1		0.63		
		B	12	0.22-2.71	0.97	0.71	
		C	9	0.08-.085	0.53	0.31	
	Total Kjeldahl nitrogen, mg/kg	Grand Haven	A	2	72-160	116	
			B	12	918-5481	2586	1689
c			8	504-5808	2890	2385	
Sayreville		A	2	411-7686	4345		
		B	12	1883-4911	3170	1004	
		C	8	1188-3800	2630	1005	
Houston		B	26	51-1033	363	262	
Pinto Island		A	1		134		
		B	12	38-963	269	284	
		C	9	80-522	222	156	
Acid-soluble sulfide, mg/kg		Grand Haven	A	2	-19	9.8	
			B	12	7-200	53	52
	C		8	5-33	18	11	
	Sayreville	A	2	15-67	41		
		B	12	33-445	169	128	
		C	8	-2357	551	815	
	Houston	B	26	12-670	100	151	
	Pinto Island	A	1		9		
		B	12	4-144	35	41	
		C	9	2-147	22	47	

(Continued)

TABLE 19. (Concluded)

Parameter	Site and Location		Number of Samples	Range	Mean	Standard Deviation	
Bulk density, gm/c.c.	Grand Haven	BG	2	1.6-1.7	1.7		
		OS	12	1.5-2.2	1.7	0.21	
		Mw	a	1.3-2.0	1.7	0.23	
	Sayreville	BG	2				
		OS	12	1.2-1.9	1.6	0.20	
		Mw	a	1.3-1.8	1.5	0.18	
	Houston	OS	26	1.6-2.2	1.9	0.14	
	Pinto Island	BG	1				
		OS	12	1.3-2.1	1.7	0.25	
		Mw	9	1-4-2.1	1.8	0.21	

TABLE 20. Chlorinated Hydrocarbons in Dredged/Material/Soil Samples

Parameter	Site & Location	Number of Samples	Range	Mean	S. D	
Total UDT, ppb	Pinto Island	BG	--	0.8	--	
		OS	10.6 - 512.5	78.0	139.8	
		GW	0 - 69.7	10.6	22.4	
	Sayerville	BG	2	6.34 - 30.0	18.17	--
		OS	12	15.89 - 242.0	96.1	89.9
		GW	8	42.2 - 627.0	196.9	200.3
	Grand Haven	BG	2	5.8 - 16.3	10.8	--
		OS	12	5.7 - 143	44.2	38
		GW	8	4.0 - 60.3	29.6	23
	Houston	OS	22	0 - 851.2	67.2	179.5
	Total PCB, ppb	Pinto Island	BG	--	0	--
			OS	0.011 - 2.7	0.36	0.78
GW			0 - 0.024	0.01	0.01	
Sayerville		BG	2	0 - 0.021	0.011	--
		OS	12	0.022 - 2.21	0.58	0.54
		GW	8	0 - 1.01	0.316	0.371
Grand Haven		BG	2	0.13 - 0.13	0.13	--
		OS	12		0.14	--
		GW	8		0.09	--
Houston	OS	22	0 - 288	0.22	0.61	

(Continued)

TABLE 20. (Concluded)

Parameter	Site & Location	Number of Samples	Range	Mean	S. D.
Dieldrin, ppb	Pinto Island	1		0.4	--
		12	0 - 2.2	0.82	0.
		9	0 - 0.6	0.07	
	Sayerville	2	0.2 - 0.7	0.45	--
		12	1.2 - 5.0	2.26	1.19
		a	0.3 - 8.1	2.71	2.35
	Grand Haven	2	0.2 - 0.2	0.2	--
		12	0.5 -	1.18	0.91
		a	0.4 - 3.7	1.53	
	Houston	22	0 - 4.2	0.83	1.35

TABLE 21.

CONCENTRATION OF TOTAL DISSOLVED SOLIDS

SITE	LOCATION	TDS, mg/l
Pinto Island	Background	274
	On-Site	6182
	Off-Site	1164
Sayreville	Background	4388
	On-Site	17027
	Off-Site	5417
Grand Haven	Background	848
	On-Site	1866
	Off-Site	1675
Houston	On-site	9973

TABLE 22. STATISTICAL CHARACTER OF LEACHATE/INTERSTITIAL WATER

Parameter	Site and Location	Number of Samples	Range	Mean	Standard Deviation	Probability p Value On-site vs. Off-site	
Calcium, mg/l	Grand Haven	BG	7-560	188	252	0.35	
		OS	80-610	356	134		
		Mw	140-530	321	99		
	Sayreville	BG	2-140	27	47	<0.01	
		OS	50-623	386	140		
		Mw	9-754	141	161		
	Houston	OS	250-1020	428	185	<0.01	
		Pinto Island	BG	31-81	56		25
			OS	25-440	140		108
	Magnesium, mg/l	Grand Haven	Mw	2-166	74	50	<0.01
			BG	8-75	31	26	
			OS	47-112	71	17	
Sayreville		Mw	13-90	43	18	co.01	
		BG	4-362	98	117		
		OS	195-1040	728	184		
Houston		Mw	7-734	237	199	co.01	
		OS	100-845	394	128		
		Pinto Island	BG	1-40	14		22
		Pinto Island	OS	10-950	174	192	co.01
			Mw	2-140	39	46	

(Continued)

TABLE 22. (Continued)

Parameter	Site and Location	Number of Samples	Range	Mean	Standard Deviation	Probability	
						P Value	On-site vs. Off-site
Potassium, mg/l	Grand Haven	BG	3-39	13	14		
		OS	5-110	29	28		< 0.01
		Mw	1-30	11	7		
	Sayreville	BG	1-923	127	322		
		OS	99-959	256	152		< 0.04
		Mw	12-680	168	188		
	Houston	OS	13-677	168	180		
	Pinto Island	BG	1-3	2	1		
		OS	6-330	81	70		< 0.01
Mw		3-180	32	45			
Grand Haven	BG	9-20	13	4			
	OS	32-790	110	177		0.25	
	Mw	6-500	60	96			
Sayreville	BG	25-1700	520	597			
	OS	2000-5000	4310	1262		< 0.01	
	Mw	75-3490	1664	1433			
Houston	OS	650-4850	2690	850			
Pinto Island	BG	5-30	14	14			
	OS	19-5800	1485	1490		< 0.01	
	Mw	2-1500	221	345			

(Continued)

TABLE 22. (Continued)

Parameter	Site and Location	Number of Samples	Range	Mean	Standard Deviation	Probability p Value On-site vs. Off-site
Chloride, mg/l	Grand Haven	BG	21-104	52	36	0.65
		OS	69-1000	154	221	
		Mw	16-125	129	144	
	Sayreville	BG	70-1407	403	520	<0.01
		OS	4511-11520	8333	2111	
		Mw	61-9572	2150	2250	
Houston	OS	1198-8963	4847	1569		
Pinto Island	BG	3	15-48	31	17	co.01
	OS	29	82-6514	2970	2706	
	Mw	20	24-625	180	175	
Grand Haven	BG	5	39-1400	328	600	co.01
	OS	24	9-1238	557	344	
	Mw	19	136-1900	825	571	
Sayreville	BG	7	75-8550	3210	3453	0.06
	OS	30	313-4213	2818	781	
	Mw	23	225-2600	798	774	
Houston	OS	67	10-1388	354	318	
Pinto Island	BG	3	35-131	72	52	co.01
	OS	29	170-2288	886	635	
	Mw	19	38-1300	408	414	

(Continued)

TABLE 22 (Continued)

Parameter	Site and Location	Number of Samples	Range	Mean	Standard Deviation	Probability p Value vs. Off-site	
ALK, mg/l	Grand Haven	BG	24-715	223	279	< 0.01	
		OS	180-1127	589	278		
		Mw	ND-569	286	146		
	Sayreville	BG	ND-10	2.5	4.6	0.45	
		OS	4-672	196	219		
		Mw	ND-1276	259	400		
	Houston	OS	250-2275	1092	538		
	Pinto Island	BG	3	40-120	85	55	< 0.01
		OS	29	48-1066	446	336	
		Mw	19	62-479	210	122	
	Grand Haven	BG	6	30-345	102	126	< 0.01
		OS	24	35-610	244	173	
Mw		19	20-160	87	48		
Sayreville	BG	8	ND-90	20	29	0.12	
	OS	32	15-280	85	72		
	Mw	23	1-780	141	191		
Houston	OS	70	30-1190	304	278		
Pinto Island	BG	2	10-20	15	73	0.03	
	OS	29	5-310	73	73		
	Mw	16	2-110	29	25		

(Continued)

TABLE 22. (Continued)

Parameter	Site and Location	Number of Samples	Range	Mean	Standard Deviation	Probability p Value On-site vs. Off-site
Cadmium, $\mu\text{g/l}$	Grand Haven	BG	0.1-4	1.4	1.7	0.24
		OS	0.3-1.0	0.8	1.63	
		Mw	0.3-4	1.4	1.33	
	Sayreville	BG	ND-147	50	56	0.04
		OS	1-203	58	61	
		Mw	ND-154	22	43	
	Houston	OS		1.3	1.4	
	Pinto Island	BG	ND-1.2	0.57	0.60	0.24
OS		0.2-40	2.7	6.5		
Mw		ND-5.3	0.59	1.1		
Grand Haven	BG	ND-0.03	0.015	0.014		
	OS	ND-0.8	0.03	0.04		
	Mw	ND-0.03	0.015	0.014		
Sayreville	BG	ND-0.11	0.035	0.046		
	OS	ND-0.02	0.007	0.007		
	Mw	ND-0.01.	0.004	0.005		
Houston	OS	ND-6.95	0.11	0.17		
Phosphate, mg/l	Pinto Island	BG	0.002-0.08	0.032	0.038	
		OS	0.005-0.5	0.087	0.147	
		Mw	0.004-0.09	0.04	0.049	

(Continued)

TABLE 22. (Continued)

Parameter	Site and Location	Number of Samples	Range	Mean	Standard Deviation	Probability p Value On-site vs. Off-site
Nickel, mg/l	Grand Haven	BG	ND-412	170	160	< 0.01
		OS	24-342	128	93	
		MW	3092	27	23	
	Sayreville	BG	100-1790	515	544	0.01
		OS	30-1200	420	322	
		Mw	7-920	237	223	
	Houston	OS	2-1000	59	158	
	Pinto Island	BG	ND-11	4	3	0.02
		OS	2-300	42	66	
		Mw	2-40	10	9	
	Grand Haven	BG	0.01-5.9	1.91	2.35	0.85
		OS	0.001-4.68	1.21	1.31	
Mw		0.012-3.64	1.30	1.51		
Sayreville	BG	0.5-36	12	12	0.55	
	OS	0.7-9	6.4	2.8		
	Mw	0.6-22	7.4	9.8		
Houston	OS	0.2-47.5	12.3	10.9		
Pinto Island	BG	0.0005-0.07	0.27	0.38	0.01	
	OS	0.066-68.2	9.1	15.2		
	Mw	0.0005-5.13	1.2	1.8		

(Continued)

TABLE 22 (Continued)

Parameter	Site and Location	Number of Samples	Range	Mean	Standard Deviation	Probability p Value On-site vs. Off-site	
Iron, mg/l	Grand Haven	BG	0.008-0.32	0.157	0.119	0.24	
		OS	0-0.31	0.005	0.095		
		Mw	0.004-0.188	0.026	0.039		
	Sayreville	BG	0-166-2500	538	988	0.9	
		OS	0.011-49.6	3.5	12		
		Mw	0.004-71.6	3.7	14		
	Houston	OS	0.003-1.1	0.147	0.213		
	Pinto Island	BG	3	0.015-0.07	0.038	0.029	0.45
		OS	40	0.003-0.8	0.054	0.131	
Mw		26	0.002-0.52	0.078	0.131		
Copper, µg/l	Grand Haven	BG	2-22	12	7	0.02	
		OS	2-62	19	17		
		Mw	0.3-33	10	9		
	Sayreville	BG	20-11400	2616	3740	0.3	
		OS	3-3000	231	540		
		Mw	1-6100	500	1400		
	Houston	OS	3-165	26	29		
	Pinto Island	BG	3	1-2	1	0.6	cc.01
		OS	39	0.5-345	61	86	
Mw		26	1-46	11	12		

(Continued)

TABLE 22 (Continued)

Parameter	Site and Location	Number of Samples	Range	Mean	Standard Deviation	Probability p Value On-site vs. Off-site	
Zinc, mg/l	Grand Haven	BG	0.030-0.640	0.176	0.235	0.45	
		OS	0.001-0.230	0.037	0.058		
		Mw	0.002-0.126	0.053	0.075		
	Sayreville	BG	0-23-7.6	3.8	3.3	0.48	
		OS	0.18-6.48	2.44	1.94		
		Mw	0.002-77.3	4.16	1.4		
	Houston	BG	0.006-1-2	0.084	0.153		
	Pinto Island	BG	3	0.021-0.030	0.024	0.005	<0.01
		OS	40	0.002-3.22	0.60	0.91	
		Mw	25	0.007-0.24	0.072	0.065	
	Grand Haven	BG	6	0.3-1.1	0.63	0.29	>0.8
OS		10	0-1.0	0.45	0.36		
Mw		11	0.1-0.9	0.44	0.27		
Sayreville	BG	8	ND-0.32	0.13	0.14	>0.8	
	OS	12	ND-1.6	0.34	0.45		
	Mw	12	ND-9	0.34	0.31		
Houston	OS	56	ND-3	0.48	0.31		
Pinto Island	BG	2	ND-0.2	0.1	0.34	0.53	
	OS	21	ND-1.1	0.34	0.34		
	Mw	15	ND-0.8	0.28	0.24		

(Continued)

TABLE 22 (Continued)

Parameter	Site and Location	Number of Samples	Range	Mean	Standard Deviation	Probability p Value vs. Off-site	
Lead, $\mu\text{g/l}$	Grand Haven	BG	1 to 2	-	-	-	
		OS	1 to 3	-	-	-	
		Mw	1 to 2	-	-	-	
	Sayreville	BG	4-32	12	10	>0.9	
		OS	1-39	14	10		
		Mw	1-50	9	10		
	Houston	OS	0.6-80	8	11		
	Pinto Island	BG	0.5-2	1.1	0.77	0.8	
		OS	0-6.4	1.9	1.6		
		Mw	0-5	1.8	1.5		
	Eh, mV	Grand Haven	BG	-75 to +70	6	74	< 0.01
			OS	43 to +300	205	106	
Mw			-80 to +190	28	85		
Sayreville		BG	+210 to +380	280	70	0.02	
		OS	-90 to +350	131	126		
		Mw	-120 to +180	52	112		
Houston	OS	-100 to +200	24	85			
Pinto Island	BG	+90 to +210	166	59	0.63		
	OS	-20 to +390	163	100			
	Mw	-83 to +270	149	95			

(Continued)

TABLE 22. (Concluded)

Parameter	Site and Location	Number of Samples	Range	Mean	Standard Deviation	Probability p Value vs. Off-site
pH	Grand Haven	BG	5	6.2-7.3	6.7	0.4
		OS	8	5.8-7.7	6.6	0.6
		Mw	12	6.1-7.3	6.8	0.42
	Sayreville	BG	68	2.8-7.2	3.9	1.5
		OS	34	5.1-6.8	5.9	0.6
		Mw	30	3.0-7.2	5.8	0.9
	Houston	OS	82	5.6-8.0	6.9	0.5
	Pinto Island	BG	3	6.1-8.2	7.2	0.4
		OS	38	4.8-8.0	6.7	0.8
		Mw	24	5.7-8.2	7.2	0.5

TABLE 23. STATISTICAL CHARACTER OF GROUNDWATER

Parameter	Site and Location	Number of Samples	Range	Mean	s. D.	Probability p Values	
						BG vs. GW	US vs. GW
Potassium, mg/l	Grand Haven	BG	3-39	13	14		
		us	7-110	34	32	0.15	0.02*
		GW	1-20	10	5		
	Sayreville	BG	1-923	127	322		
		US	99-959	413	307	> 0.9*	0.07*
		GW	12.2-650	120	195		0.015*
Pinto Island	BG	1-3	2	1			
	us	17-200	108	55	0.27	< 0.01	
	GW	3-165	31	40		< 0.01*	
Sodium, mg/l	Grand Haven	BG	9-20	13	4		
		us	31-680	114	188	< 0.01	0.2
		GW	6075	40	18		0.18
	Sayreville	BG	25-1700	520	597		
		us	2770-6200	4025	925	0.33*	< 0.01*
		GW	30-2670	841	765		< 0.01*
Pinto Island	BG	5-30	14	14			
	US	20-5800	2121	1459	0.25	0.01*	
	GW	2-1061	198	260		< 0.01	
Calcium, mg/l	Grand Haven	BG	7-560	188	252		
		us	50-480	261	161	0.12	0.5*
		GW	170-530	331	107		0.23*
	Sayreville	BG	2-140	27	47		
		us	92-670	300	187	0.15	< 0.01
		GW	170-530	331	107		< 0.01*
Pinto Island	BG	31-81	56	25			
	us	29-350	173	108	0.45	0.01*	
	GW	8-166	72	47		0.01	

(Continued)

TABLE 23. (Continued)

Parameter	Site and Location	Number of Samples	Range	Mean	S.D.	BG vs. GW	Probability p Values	
							BG vs. US	US vs. GW
Magnesium, mg/l	Grand Haven	BG	8-75	31	26			
		US	20-93	66	21			0.01
		GW	13-65	43	15	0.35*	0.02*	
Sayreville	Sayreville	BG	3-362	98	117			
		US	440-1050	651	175			<0.01*
		GW	7-504	170	184	0.28*	<0.01*	
Pinto Island	Pinto Island	BG	1-40	14	22			
		US	12-550	237	161			co.01
		GW	2-140	39	48	0.2*	0.04	
Grand Haven	Grand Haven	BG	39-1400	328	600			
		US	9-1115	417	306			0.12
		GW	136-1700	743	591	0.22*	0.68	
Sayreville	Sayreville	BG	70-1407	403	520			
		US	4819-12188	8226	1785			<0.01*
		GW	61-2059	971	814	0.12	0.01	
Pinto Island	Pinto Island	BG	21-104	52	36			
		US	64-1051	185	289			0.25
		GW	40-109	91	27	0.08	0.15	
Grand Haven	Grand Haven	BG	24-715	223	279			
		us	264-1120	734	330			co.01
		GW	141-569	326	142	0.31	<0.01*	
Sayreville	Sayreville	BG	ND-10	2.5	4.6			
		us	48-816	360	271			0.04
		GW	24-343	104	129	0.04	<0.01	
Pinto Island	Pinto Island	BG	40-120	85	55			
		us	45-977	484	290			co.01
		GW	62-479	230	126	0.07	0.015*	

(Continued)

TABLE 23. (Continued)

parameter	Site and Location	Number of Samples	Range	Mean	S.D.	BG vs. GW	Probability P Values	
							BG vs. US	US vs. GW
Total organic carbon	Grand Haven	6	30-345	102	126			
	us	9	50-370	211	103			
	GW	10	30-160	89	46	0.75	0.12*	<0.01
Sayreville	BG	8	ND-90	20	29			
	US	13	15-490	191	161	0.24	<0.01	0.02
	GW	10	1-165	49	60			
Pinto Island	BG	2	10-20	15	7			
	US	15	0-240	79	67			
	GW	13	2-235	53	63	0.07*	<0.01*	0.3*
Cadmium, µg/l	Grand Haven	6	0.3-4	1.4	1.7			
	US	11	0.7-1.0	0.79	0.44	0.35	0.20	0.49*
	GW	12	0.3-2	0.92	0.45			
Sayreville	BG	8	ND-147	50	56			
	us	12	ND-129	22	39	0.8*	0.23*	0.32*
	GW	12	ND-154	43	60			
Pinto Island	BG	3	ND-1.2	0.57	0.60			
	us	16	0.1-46	4	11.3	0.86	0.60	0.30
	GW	17	ND-5.3	0.7	1.3			
Nickel, mg/l	Grand Haven	6	ND-412	170	164			
	US	11	1-190	65	59	co.01	0.07	0.03
	GW	12	7-77	22	20			
Sayreville	BG	8	80-1790	515	545			
	US	12	30-890	325	292	0.1	0.3	0.38
	GW	13	E-490	237	172			
Pinto Island	BG	3	ND-11	4.3	5.9			
	US	16	3-270	40	67	0.18*	0.27	0.1
	GW	17	ND-40	11	10			

(Continued)

TABLE 23. (Continued)

Parameter	Site and Location	Number of Samples	Range	Mean	S.D.	BG	"s. GW	Probability p Values		
								BG vs. Us	Us vs. GW	
Manganese, mg/l	Grand Haven	BG	0.5-5.9	1.91	2.35					
		US	0.002-2.7	0.76	0.90					
		GW	0.016-4.8	1.50	1.69	0.75*	0.19	0.4*		
	Sayreville	BG	0.5-36	12	12					
		US	1.3-16.2	6	4					
		GW	1.1-20	8	7	0.35	0.12	0.4		
	Pinto Island	BG	0.0005-0.07	0.027	0.038					
		US	0.4-53.6	17	14.6					
		BG	0.001-4.5	1.2	1.7	0.25	0.25	<0.01		
		GW								
	Iron, mg/l	Grand Haven	BG	0.008-0.320	0.157	0.119				
			us	ND-0.830	0.125	0.247	co.01	0.75*	0.15	
GW			0.008-0.045	0.018	0.015					
Sayreville		BG	0.5-36	12	12					
		us	1.3-16.2	6	4					
		GW	1.1-20	8	7	0.35	0.12	0.4		
Pinto Island	BG	0.015-0.070	0.038	0.029						
	US	0.003-0.210	0.030	0.056	0.5*	0.75*	0.08*			
	GW	0.002-0.510	0.101	0.154						
Copper, µg/l	Grand Haven	BG	2-22	12	7					
		US	1-59	15	18					
		GW	0.3-12	6	4	0.09*	0.7	0.1		
	Sayreville	BG	20-11400	2616	3740					
		US	3-2050	321	673	0.23	0.05	0.31		
		GW	1-6100	1035	2055					
Pinto Island	BG	1-2	1	0.6						
	us	1-225	41	54	0.13	0.25	0.02			
	GW	1-33	9.9	9.5						

(Continued)

TABLE 23. (Continued)

Parameter	Site and Location	Number of Samples	Range	Mean	S.D.	BG Vs. GW	Probability p Values		
							BG Vs. US	US Vs. GW	
Zinc, mg/l	Grand Haven	BG	0.030-0.640	0.176	0.235				
		US	0.001-0.080	0.019	0.022	0.03	0.32		
		GW	0.002-0.126	0.032	0.042				
	Sayreville	BG	0.23-7.6	3.8	3.3				
		us	0.14-4.16	1	1	0.59	0.24		
		GW	0.002-77.3	8	20				
	Pinto Island	BG	0.021-0.030	0.024	0.005				
		us	0.006-3.51	0.41	0.97	0.9	0.15		
		GW	0.008-0.24	0-073	0.066				
	Mercury, µg/l	Grand Haven	BG	0.3-1.1	0.64	0.32			
			US	0-1.0	0.41	0.37	>0.9	0.87	
GW			0.1-0.9	0.44	0.28				
Sayreville	BG	0-032	0.13	0.14					
	us	0.08-1.6	0.37	0.46	0.36	0.9			
	GW	0.004-0.68	0.33	0.3					
	BG	ND-0.2	0.1						
	US	ND-1.0	0.3	0.3					
Pinto Island	BG	ND-0.6	0.3	0.2					
	US								
	GW								
Lead, µg/l	Grand Haven	BG	1-20	7	8				
		US	1-30	8	11	0.05	0.1		
		GW	1	1	0				
	Sayreville	BG	4-32	12	10				
		US	1-34	18	11	0.07	co.01		
		GW	1-16	5	5				
	Pinto Island	BG	0.5-Z	1.1	0.77				
		us	ND-3.1	1.4	1.2	0.39	>0.9		
GW	ND-5	1.9	1.5						

(Continued)

TABLE 23. (Concluded)

Parameter	Site and Location	Number of Samples	Range	Mean	S.D.	Probability p Values		
						BG vs. GW	BG vs. US	US vs. GW
Chloride, mg/l	Grand Haven	BG	21-104	52	36			
		us	64-1051	185	289			0.25
	Sayreville	GW	40-109	91	27		0.08*	
		BG	70-1407	403	520			
		US	4819-12188	8226	1785		0.01	co.01
		GW	61-2059	971	814			
Pinto Island	BG	15-48	31	17				
	US	16-9224	3193	2524		0.05	co.01	
	GW	24-1153	238	309				
pH	Grand Haven	BG	6.2-7.3	6.7	0.4			
		US	6.3-7.2	6.9	0.4			
	Sayreville	GW	6.4-7.3	6.7	0.4			
		BG	2.8-7.2	3.9	1.5			
		US	4.1-6.7	6	0.7			-
		GW	4.2-6.8	6	0.7			
Pinto Island	BG	6.1-8.2	7.2	0.4				
	US	5.6-8.3	7.0	0.7				
	GW	5.7-8.2	7.1	0.5				
Eh, mV	Grand Haven	BG	-75 to 70	6	74			
		US	90 to 140	115	35			
	Sayreville	GW	2 to 190	39	83			
		BG	210 to 380	280	70			
		US	6 to 290	112	85			
		GW	61 to 230	136	62			
Pinto Island	BG	90 to 210	166	59				
	us	-31 to +300	129	85				
	GW	-3 to +270	158	84				

Legend: BG: Background sample GW: Monitoring well sample * : Samples from two populations,
us: Under-site sample ND: Not detected special "t" test applied (for details see text)

TABLE 24. IMPORTANT SOLUBILITY PRODUCTS (K_{sp}) OF TRACE METALS*

Metal	Oxide	Hydroxide	Carbonate	Sulfide	chloride	Phosphate	Silicate
Cd(II)		13.6	13.6	26.1			
Ca(II)		5.26	8.32 (calcite), a.22 (argonite), 16.7** (dolomite)	2.94		6.25 (CaHPO ₄) 26 (Ca ₃ (PO ₄) ₂) 1.14 (CaH ₂ (PO ₄) ₂) 6.4 (CaHPO ₄ (H ₂ O) ₂) 40.9 (Ca ₄ H(PO ₄) ₃) 44.6 (Ca ₅ OH(PO ₄) ₃) 120.8 (Ca ₁₀ (PO ₄) ₆ ·F ₂)	3.7 (CaSiO ₃) 52.3** (anorthite), 585 (Ca-montmorillonite)
Cu(II)	20.4	18.6	9.63 (CuCO ₃), 33.2 (Cu ₂ CO ₃ (OH) ₂)	35.2		37.7	
Fe(II)		15.3	10.2	16.9(FeS)		33.3	18.9**
Fe(III)	80** (Fe ₂ O ₃)	39.3		18.2 (Fe ₃ S ₄)		25.8	
Pb(II)	15.4 (PbO)	16.1 18.8 (Pb ₃ (OH) ₂ (CO ₃) ₂)	13.1	26.6	4.79	43.5, 12.6** (PhHPO ₄)	
Mn(II)		9.2 (active) 11.6 (brucite)	4.9 (magnesite), 5.4 (nesquehonite), 16.7 (MgCa(CO ₃) ₂)**		4.44** (MgCl ₂ (H ₂ O) ₆), 4** (KMgCl ₃ (H ₂ O) ₃)	28.4 (Mg ₃ (PO ₄) ₂) 12.6** (mgNH ₄ (PO ₄)) 13.2** (MgNH ₄ PO ₄ (H ₂ O) ₆) 5.0** (MgHPO ₄ (H ₂ O) ₃)	

(Continued)

TABLE 24. (Continued)

Metal	Oxide	Hydroxide	Carbonate	Sulfide	Chloride	Phosphate	Silicate
Mn(II)	0.92**	12.7	9.3	12.9 (crystalline), 15.7 (precipitated)		22	13.2**
Hg(II)	25.7**	25.4		52.2 (meta-cinnabar) 53.6 (cinnabar)	13.8		
K(I)			-4.11				76** (orthoclase) 124** (muscovite)
Na(I)							40.6** (albite) 294** (Na-montmorillonite)
Ni(II)		14.81 (fresh) 17.31 (aged)		18.5(α) 25.7(β)			
Zn(II)		15.7 (Amorphous), 16 (Amorphous, aged), 16.9 (cryst. aged)	10.8	25.2 (sphaerite), 22.8 (wurzite), 22.1 (precipitated)	36.7	21.03**	

TABLE 24. (Concluded)

*Values in pK_{sp} (log K_{sp}) when I (ionic temperature) = 0, T (temperature) = 25°C.

**NaAlSi₃O₈(s, albite) + 7H₂O + H⁺ = Al³⁺ + Na⁺ + 3H₄SiO₄ + 3OH⁻;
 CaAl₂Si₂O₈(s, anorthite) + 8H₂O = 2Al³⁺ + 2H₄SiO₄ + 8OH⁻ + Ca²⁺;
 1 1/2 KAlSi₃O₈(s, orthoclase) + 12H₂O = 1 1/2 Al³⁺ + 1 1/2 K⁺ + 4 1/2 H₄SiO₄ + 6OH⁻;
 KAl₃Si₃O₁₀(OH)₂(s, muscovite) + 10H₂O = 3Al³⁺ + K⁺ + 3H₄SiO₄ + 10OH⁻;
 3Na_{0.33}Al_{2.33}Si_{3.67}O₁₀(OH)₂(s, Na-montmorillonite) + 30H₂O = 7Al³⁺ + 11H₄SiO₄ + 22OH⁻ + Na⁺;
 3Ca_{0.33}Al_{4.67}Si_{7.33}O₂₀(OH)₄(s, Ca-montmorillonite) + 60H₂O = 14Al³⁺ + 22H₄SiO₄ + 44OH⁻ + Ca²⁺;
 CaMg(CO₃)₂(s, dolomite) = Ca²⁺ + Mg²⁺ + 2CO₃²⁻;
 Fe₂O₃(s) + 3H₂O = 2Fe³⁺ + 6OH⁻;
 FeSiO₃(s) + H₂O = Fe²⁺ + 2OH⁻ + SiO₂(s);
 Pb₃(OH)₂(CO₃)₂(s) = 3Pb²⁺ + 2OH⁻ + 2CO₃²⁻;
 PbO(s) + H₂O = Pb²⁺ + 2OH⁻;
 PbHPO₄(s) = Pb²⁺ + HPO₄²⁻;
 MgNH₄(PO₄)(s) = Mg²⁺ + NH₄⁺ + PO₄³⁻;
 MgNH₄(PO₄)(H₂O)₆(s) = Mg²⁺ + NH₄⁺ + PO₄³⁻ + 6H₂O;
 MgHPO₄(H₂O)₃(s) = Mg²⁺ + HPO₄²⁻ + 3H₂O;
 MgCl₂(H₂O)₆(s, bischofite) = Mg²⁺ + 2Cl⁻ + 6H₂O;
 KMgCl₃(H₂O)₃(s, carnallite) = K⁺ + Mg²⁺ + 3Cl⁻ + 3H₂O;
 MnO₂(s) + 2H⁺ = Mn²⁺ + 1/2 O₂ + H₂O;
 MnSiO₃(s) + H₂O = Mn²⁺ + 2OH⁻ + SiO₂(s);
 HgO(s) + H₂O = Hg²⁺ + 2OH⁻;
 ZnSiO₃(s) + H₂O = Zn²⁺ + 2OH⁻ + SiO₂(s)

FIGURES 1-78

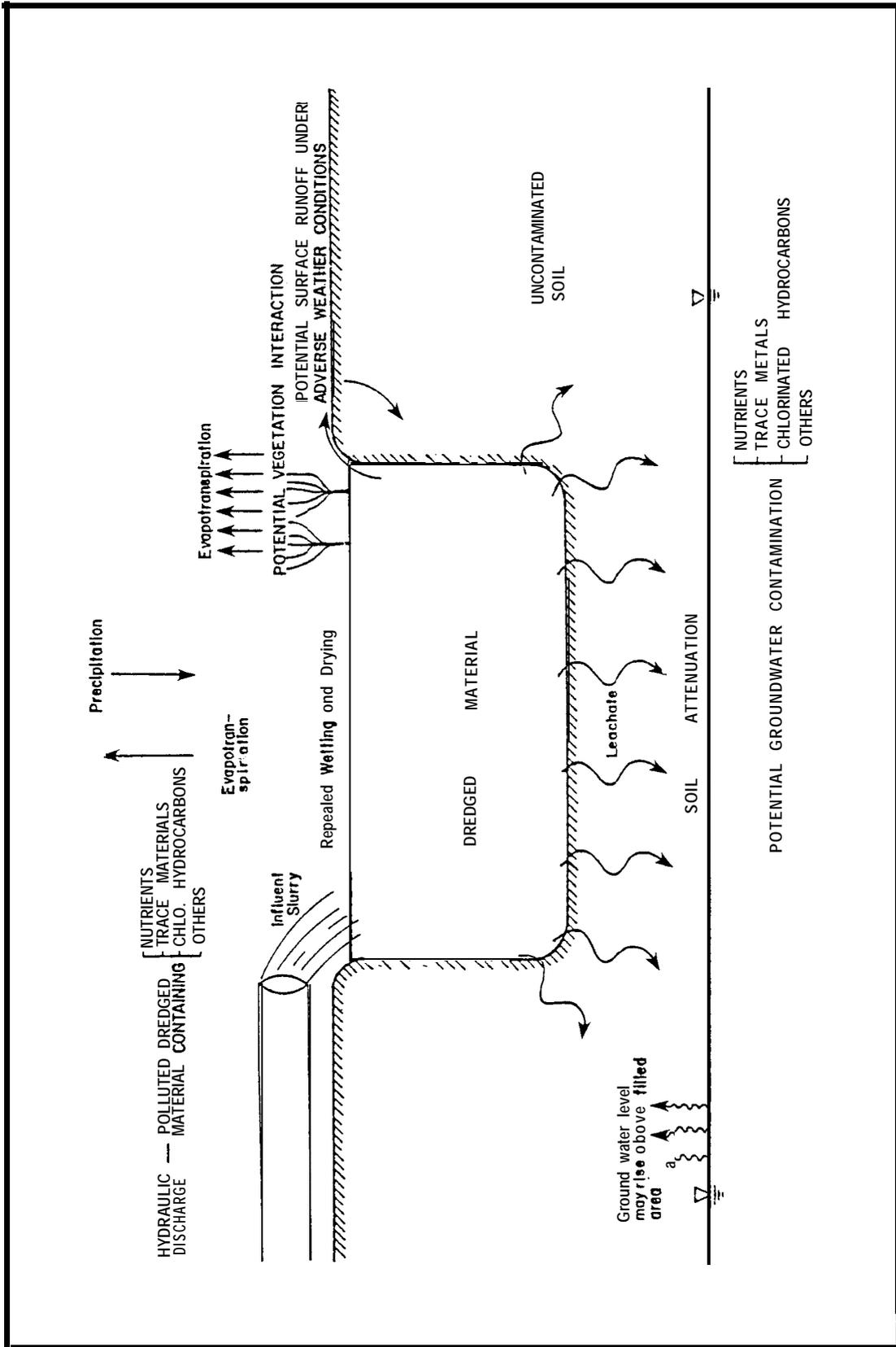


Figure 1. Conception of land disposal of dredged material and associated problems

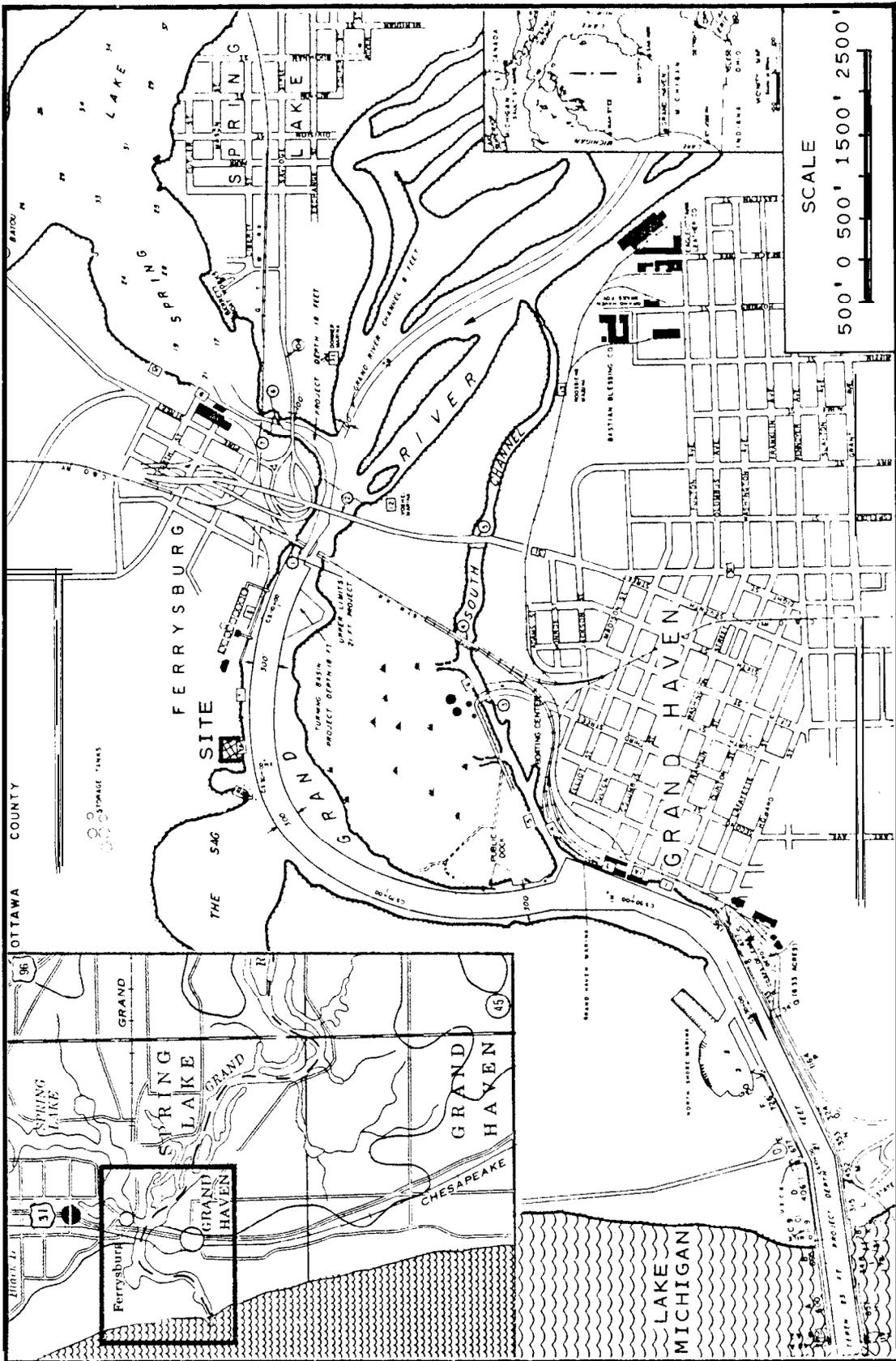


Figure 2. Regional map for Grand Haven site

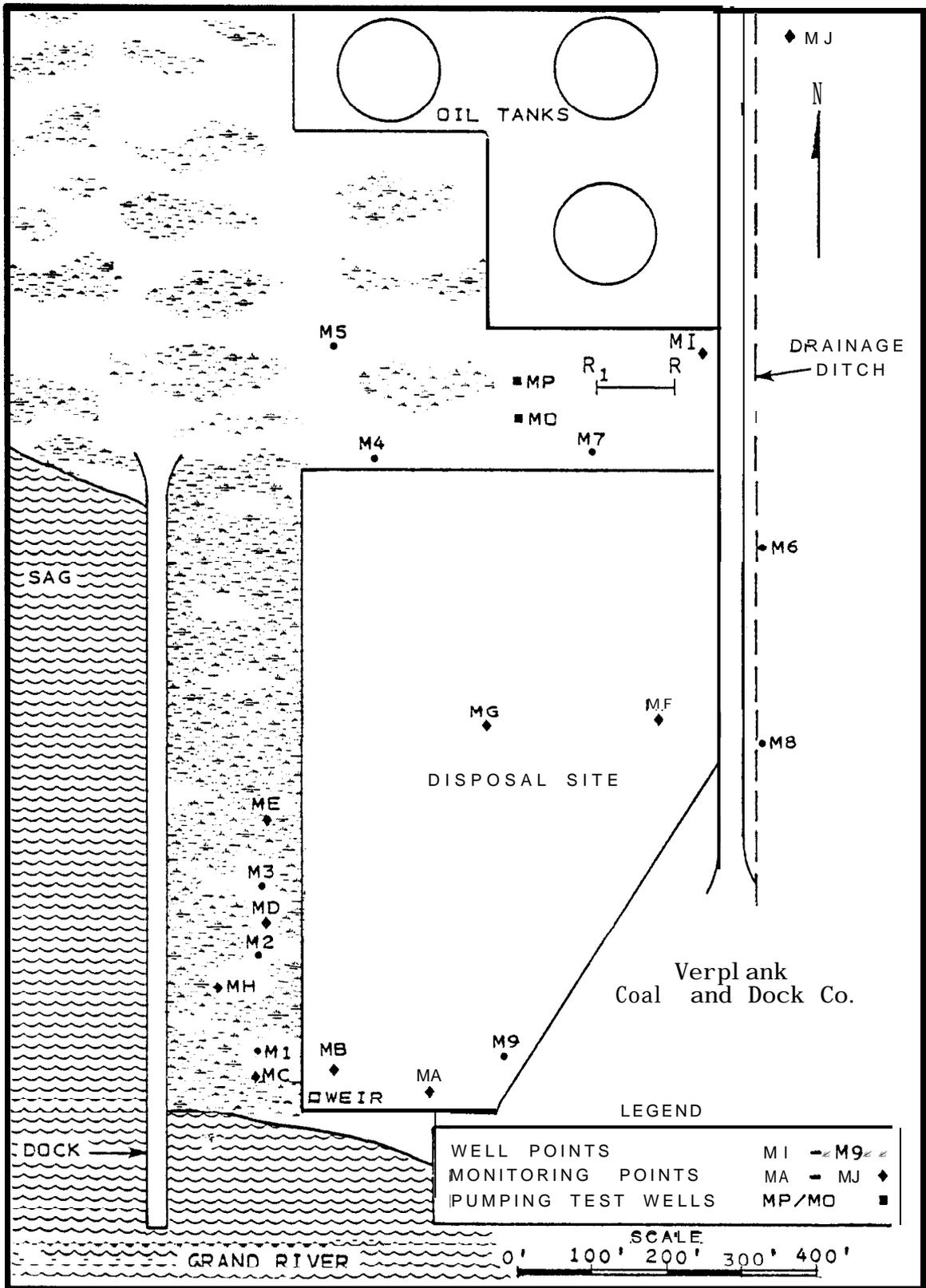


Figure 3. Grand Haven site

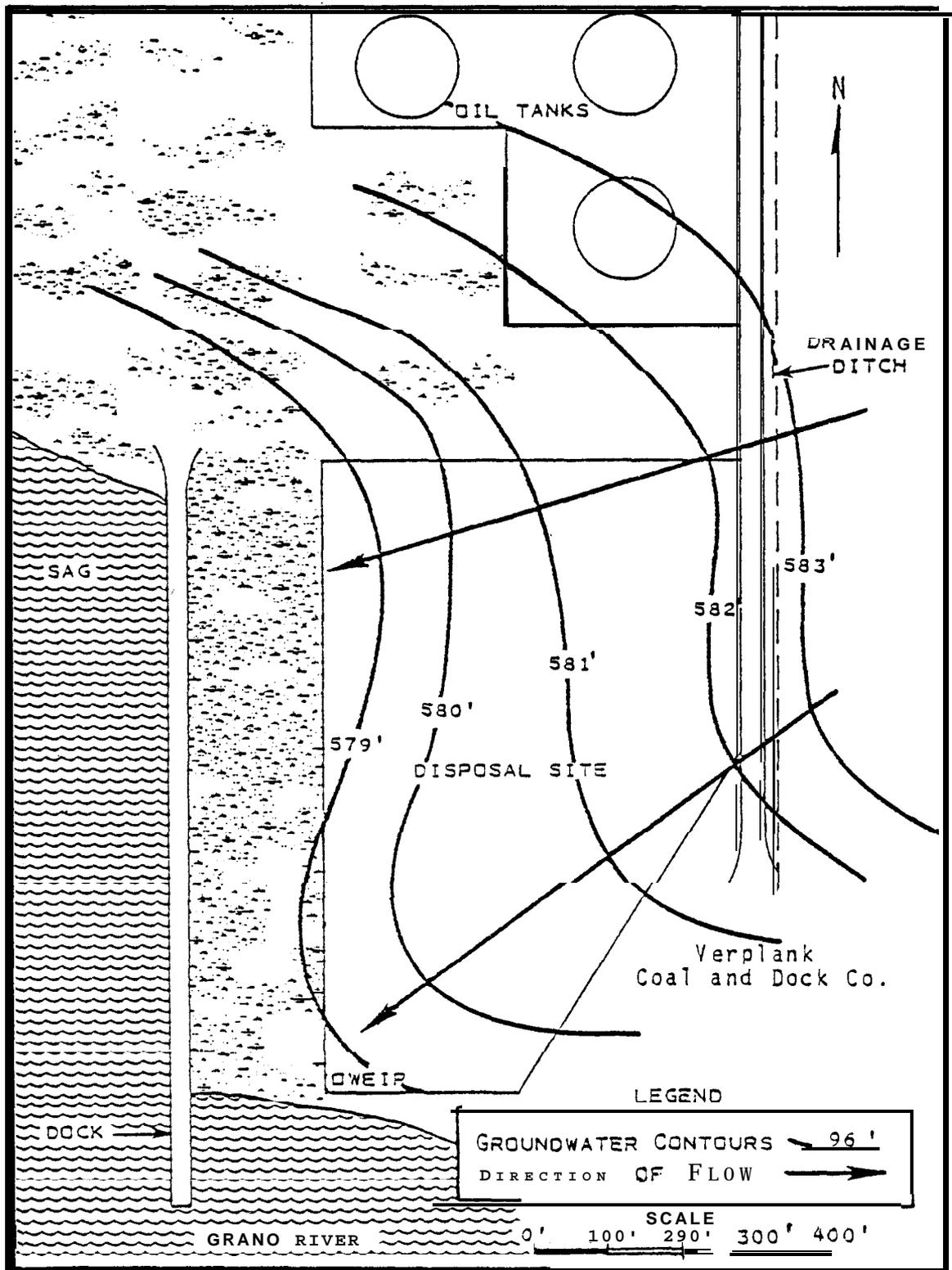


Figure 4. Water level contours on November '2, 1976, Grand Haven site

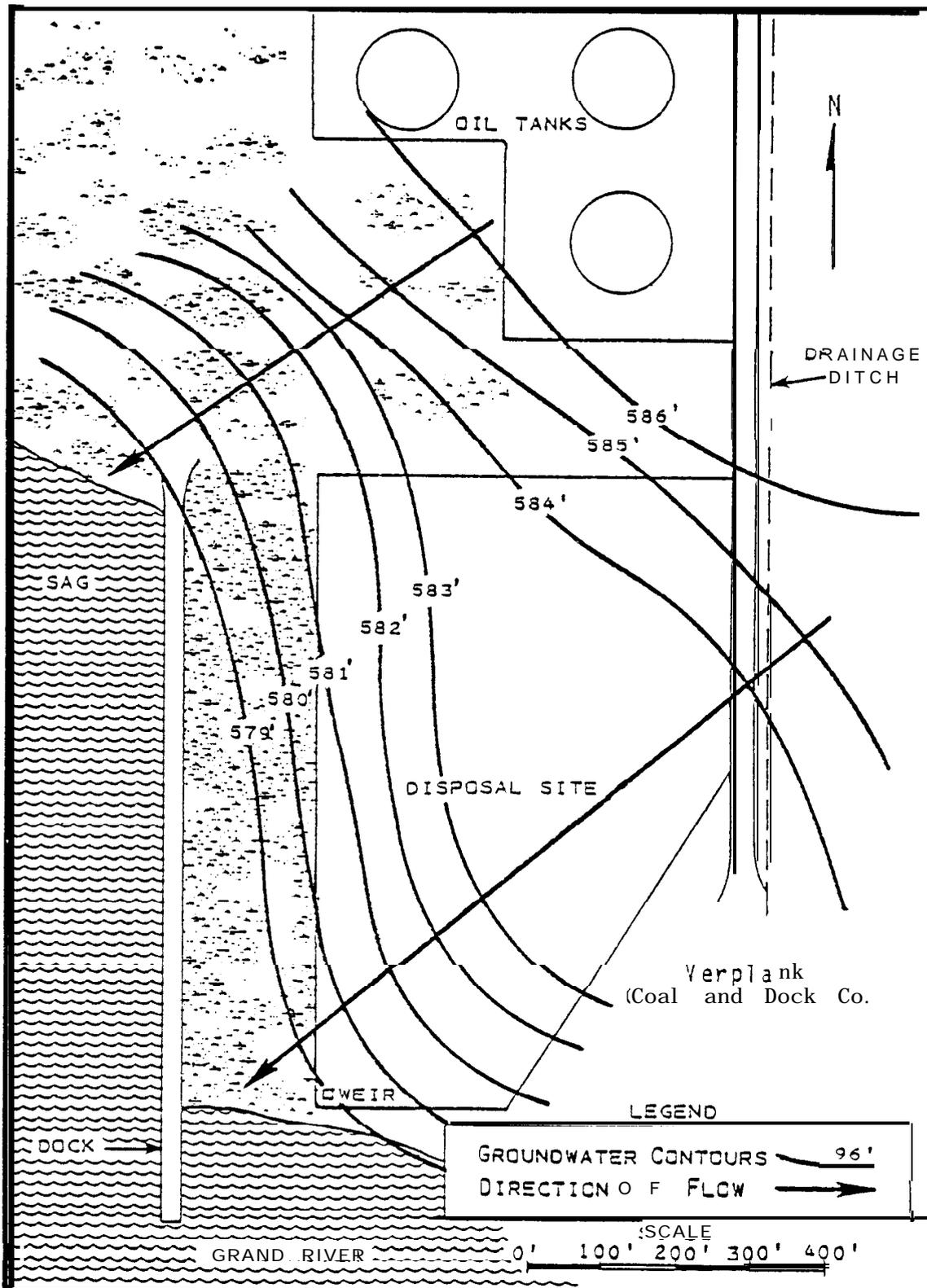


Figure 5. Water level contours on December 4, 1976, Grand Haven site

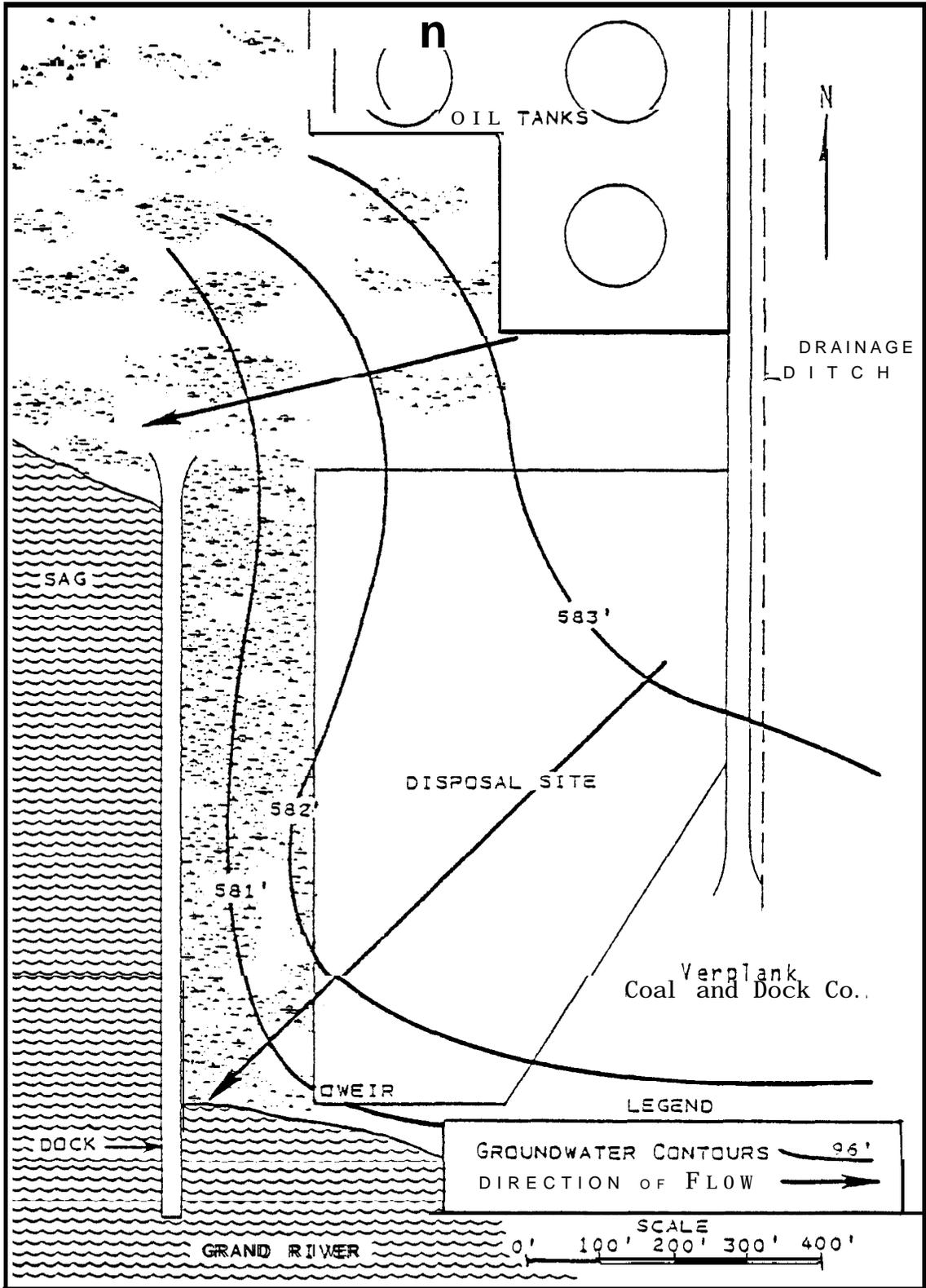


Figure 6. Water level contours on April 8, 1977, Grand Haven site

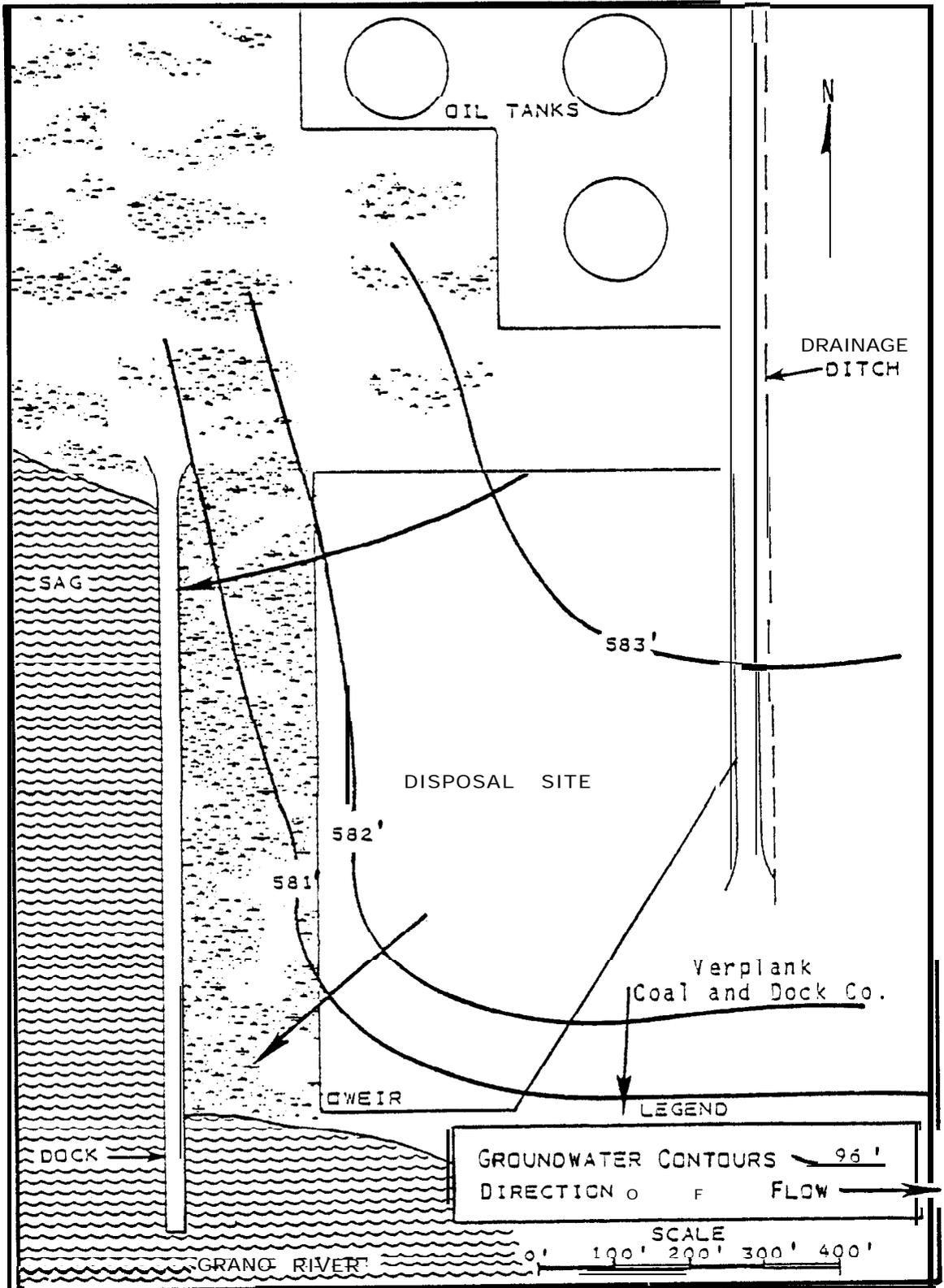


Figure 7. Water level contours on May 30, 1977, Grand Haven site

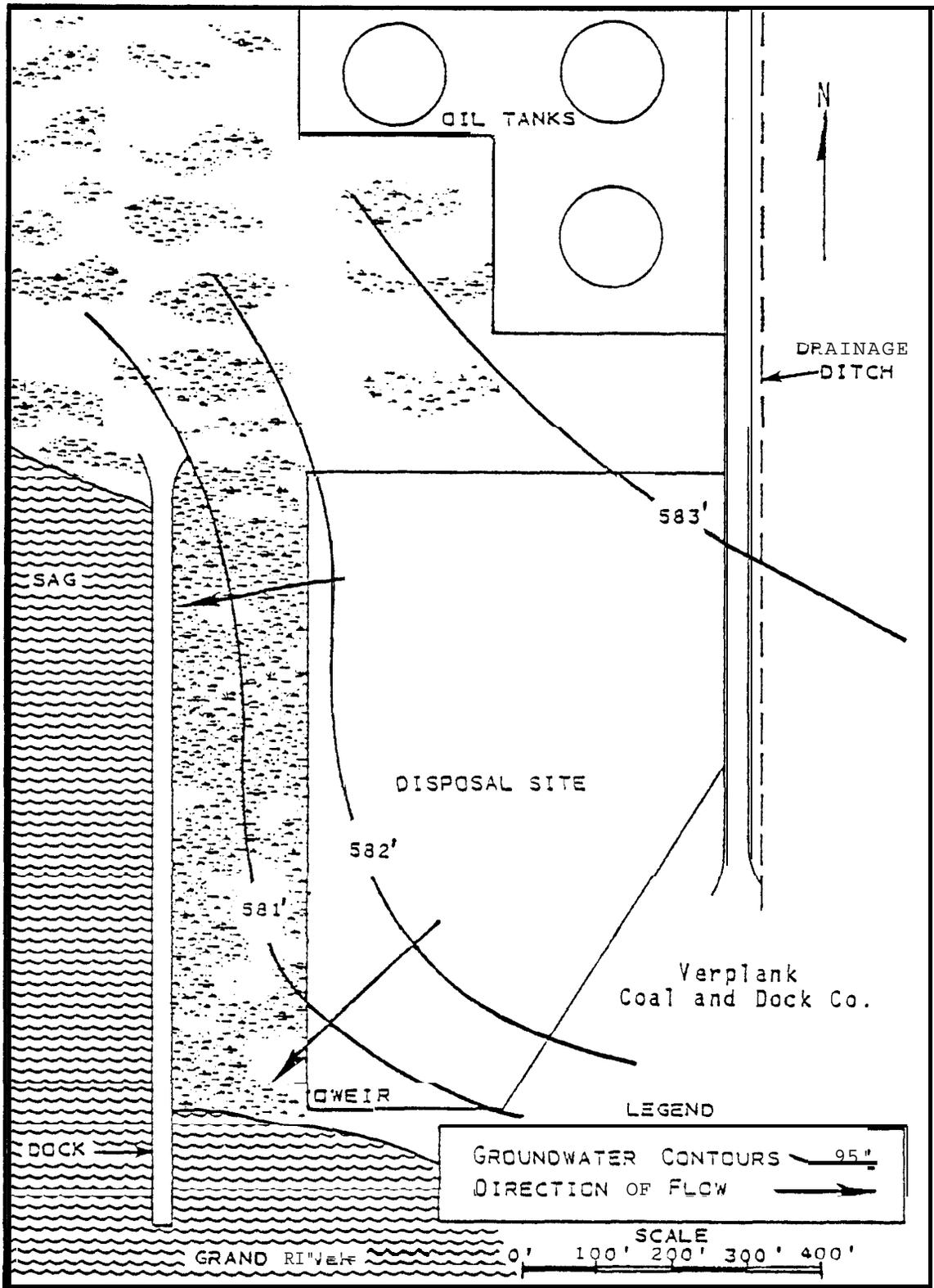


Figure 8. Water level contours on August 5, 1977, Grand Haven site

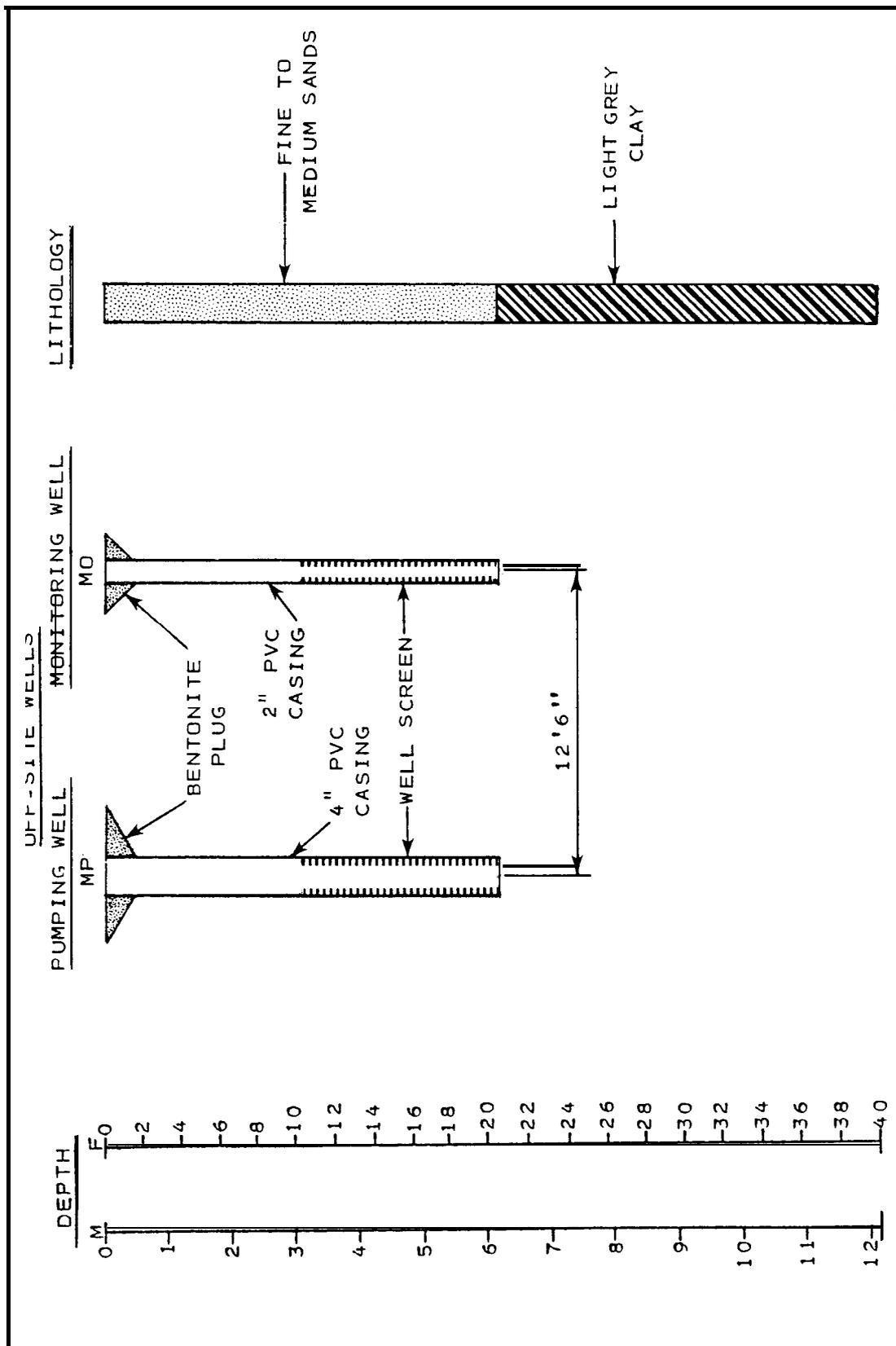


Figure 9. Off-site pumping and monitoring wells at Grand Haven site

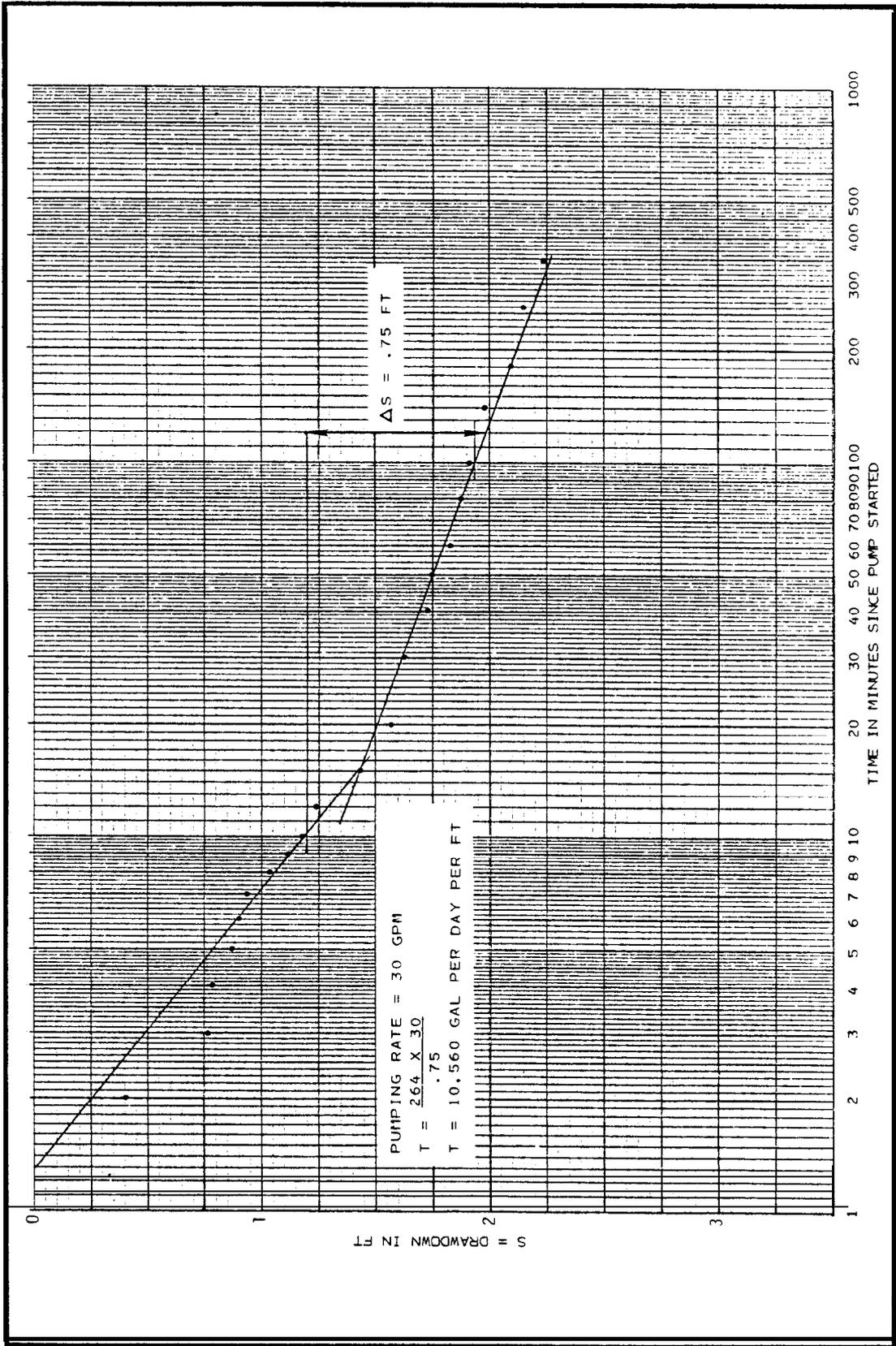


Figure 10. Drawdown curve for off-site well MP

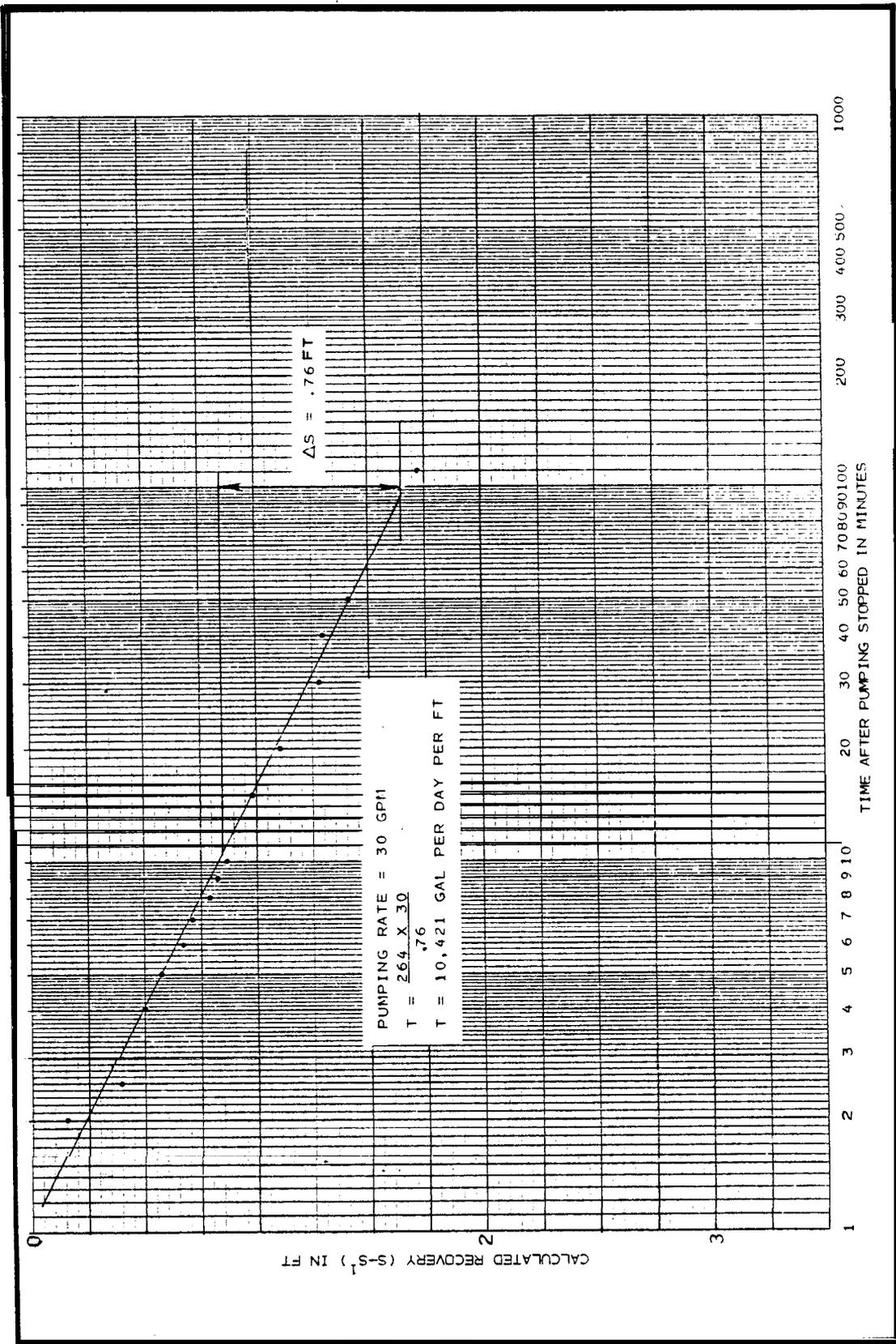


Figure 11. Recovery curve for off-site well MP

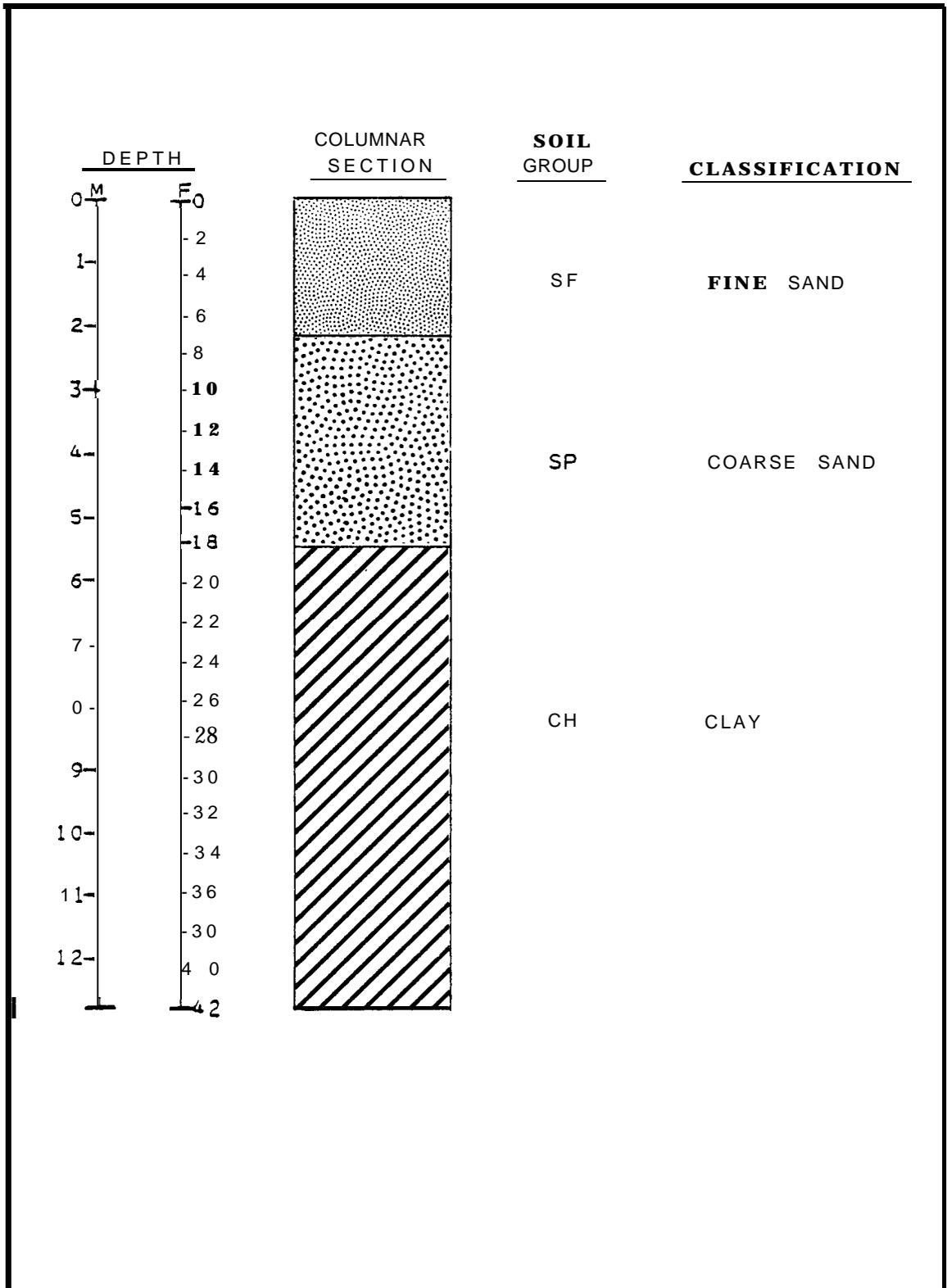


Figure 13. Generalized soil profile, Grand Haven site

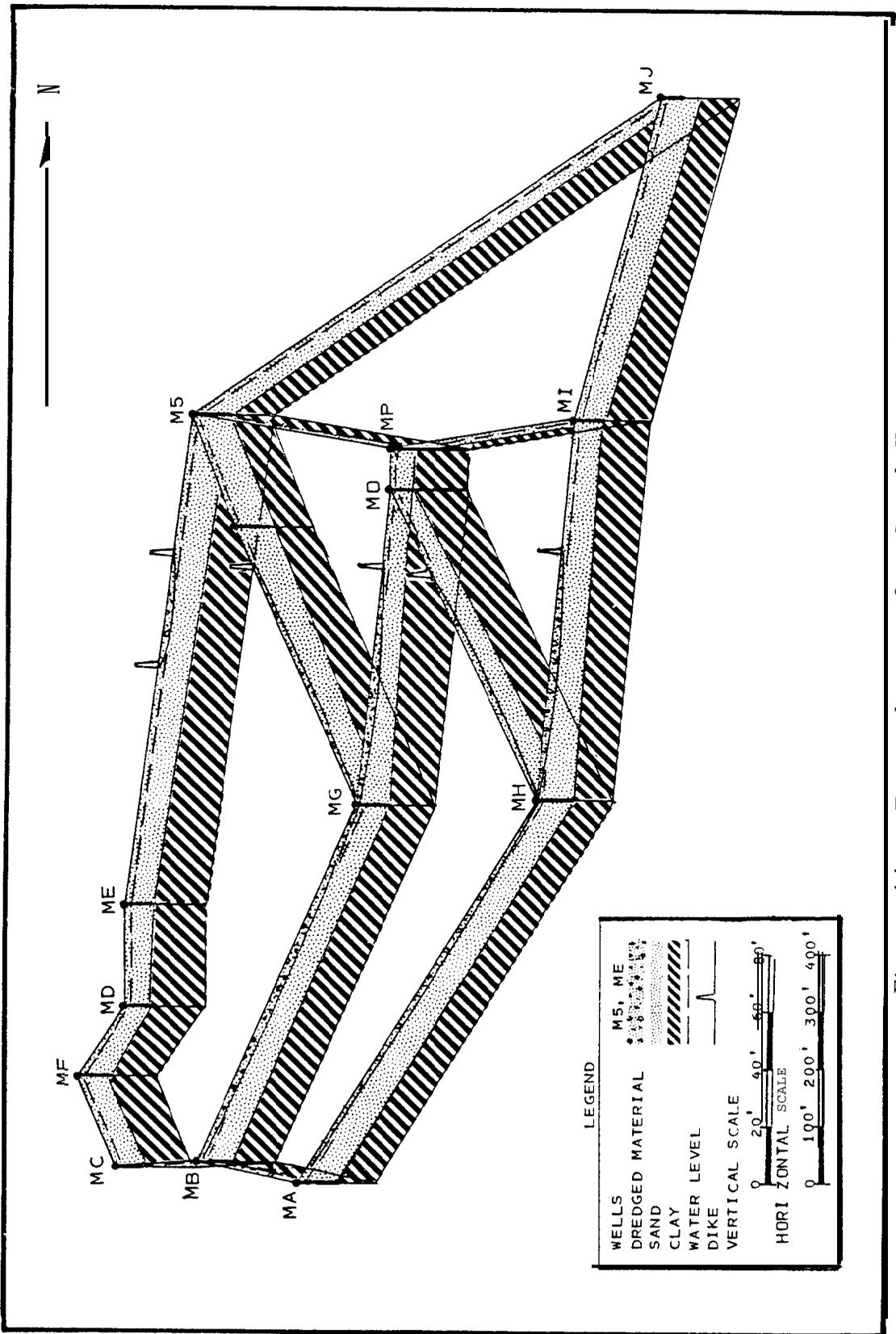


Figure 14. Fence diagram for Grand Haven site

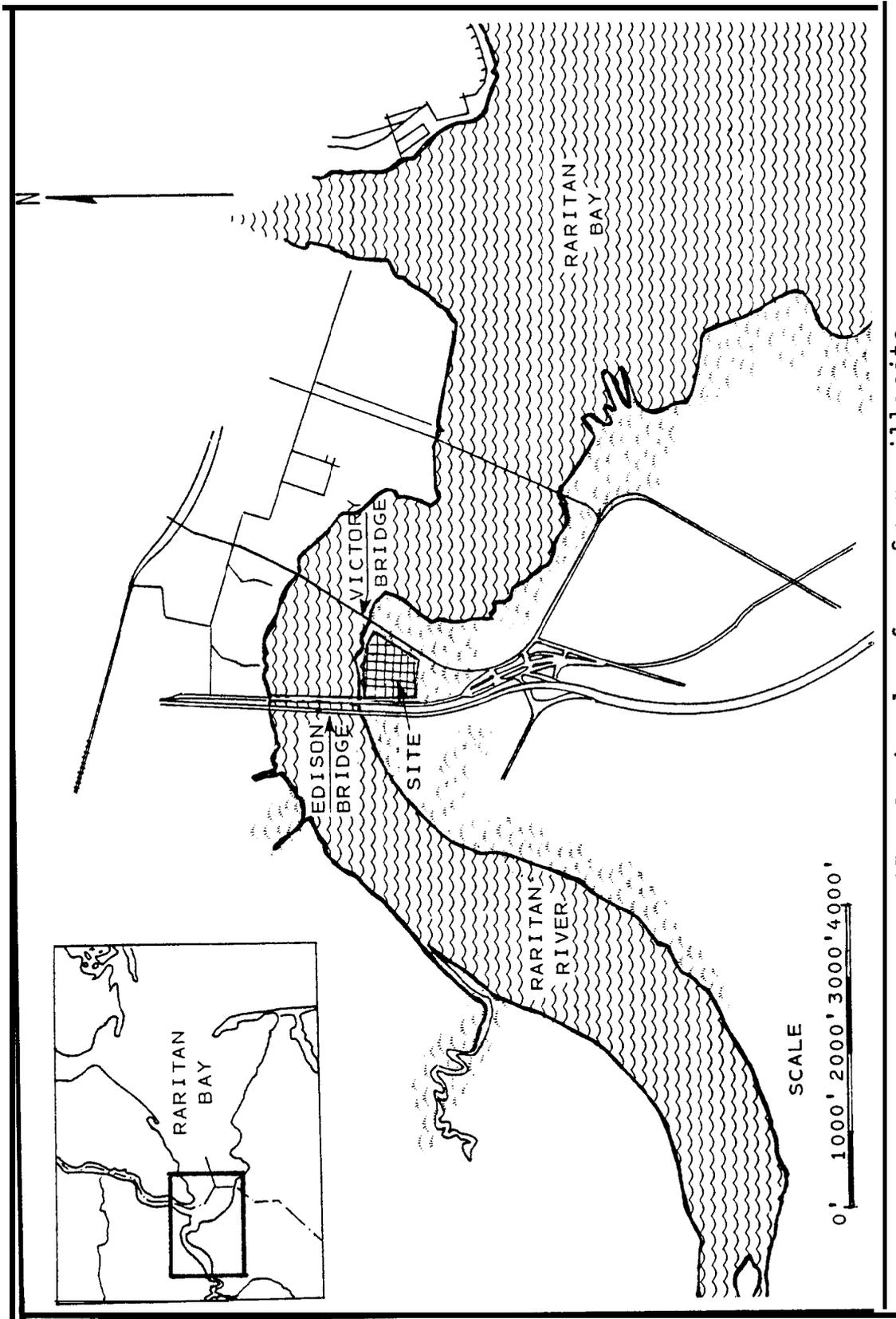


Figure 15. Regional map for Sayreville site

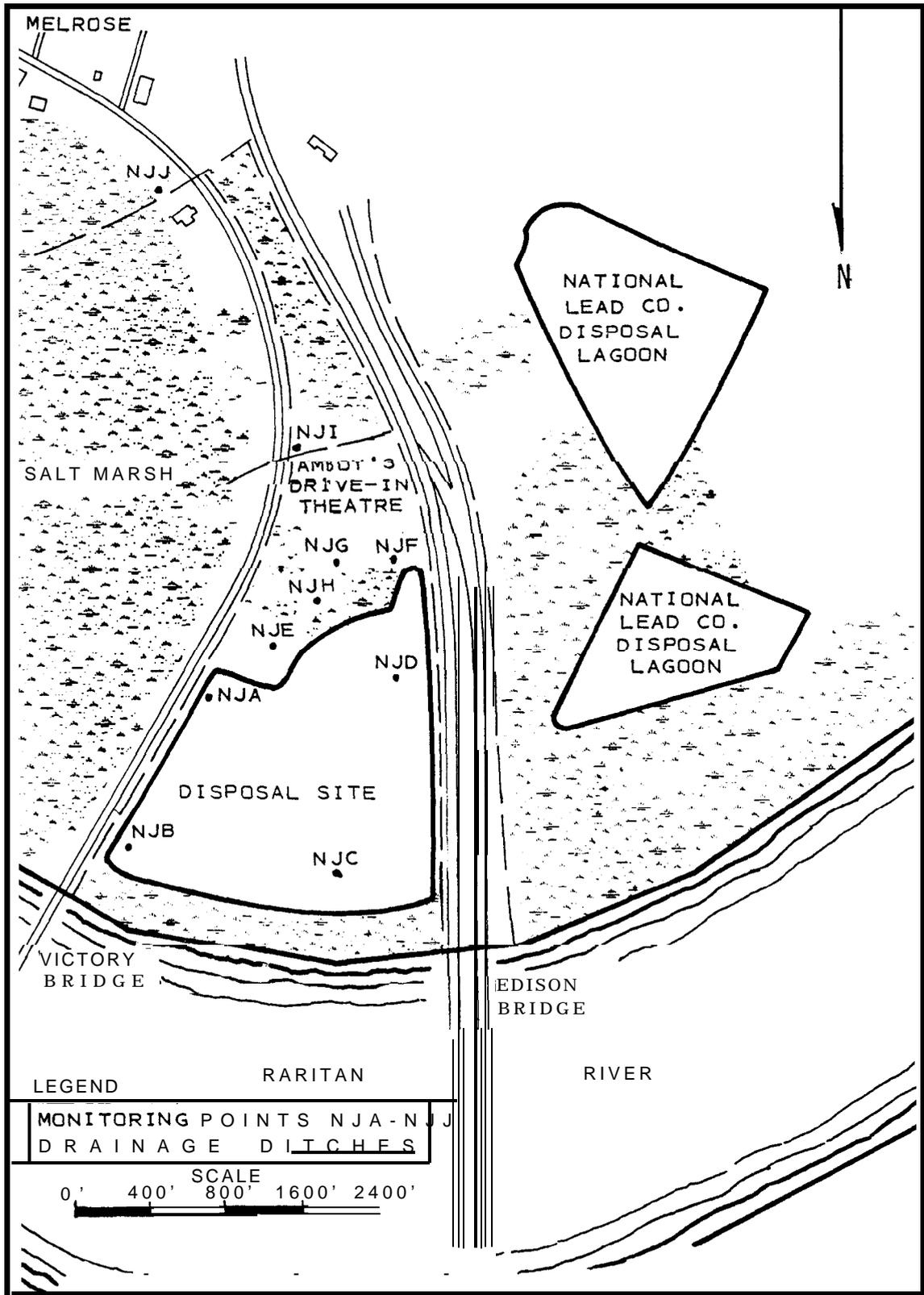


Figure 16. Area map for Sayreville site

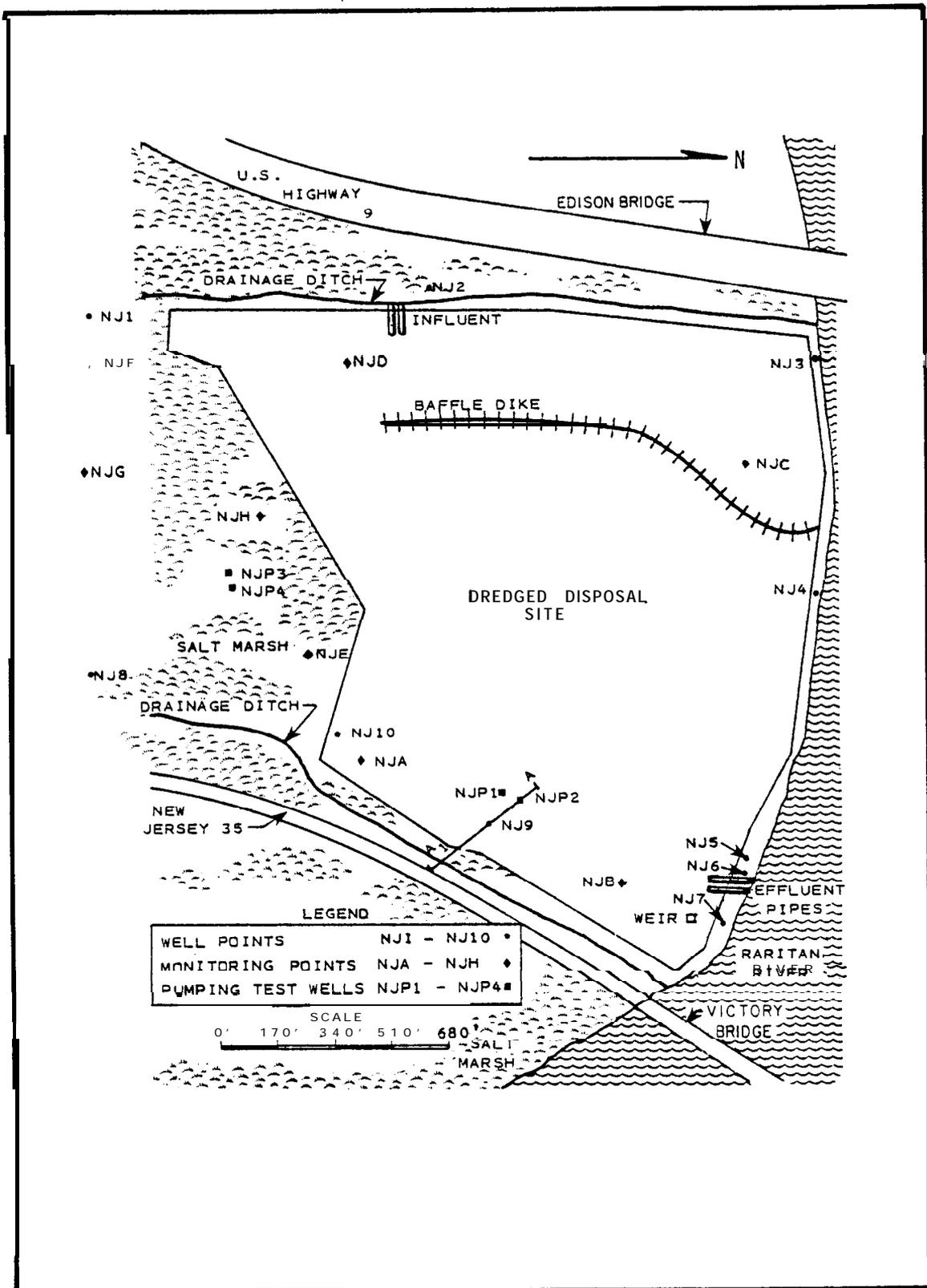


Figure 17. Sayreville site

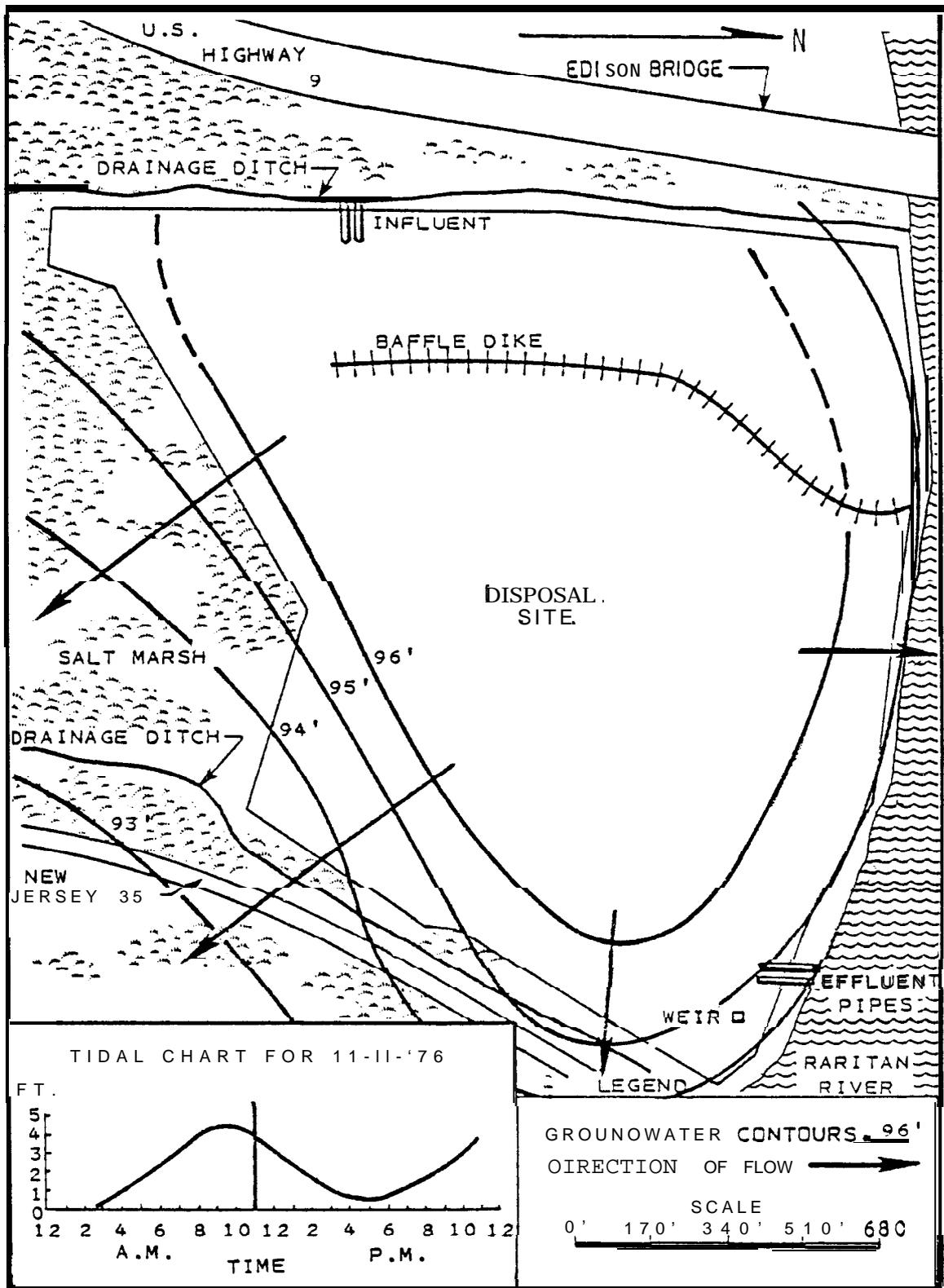


Figure 18. Groundwater contours at 11:00 a.m., November 11, 1976, Sayreville site

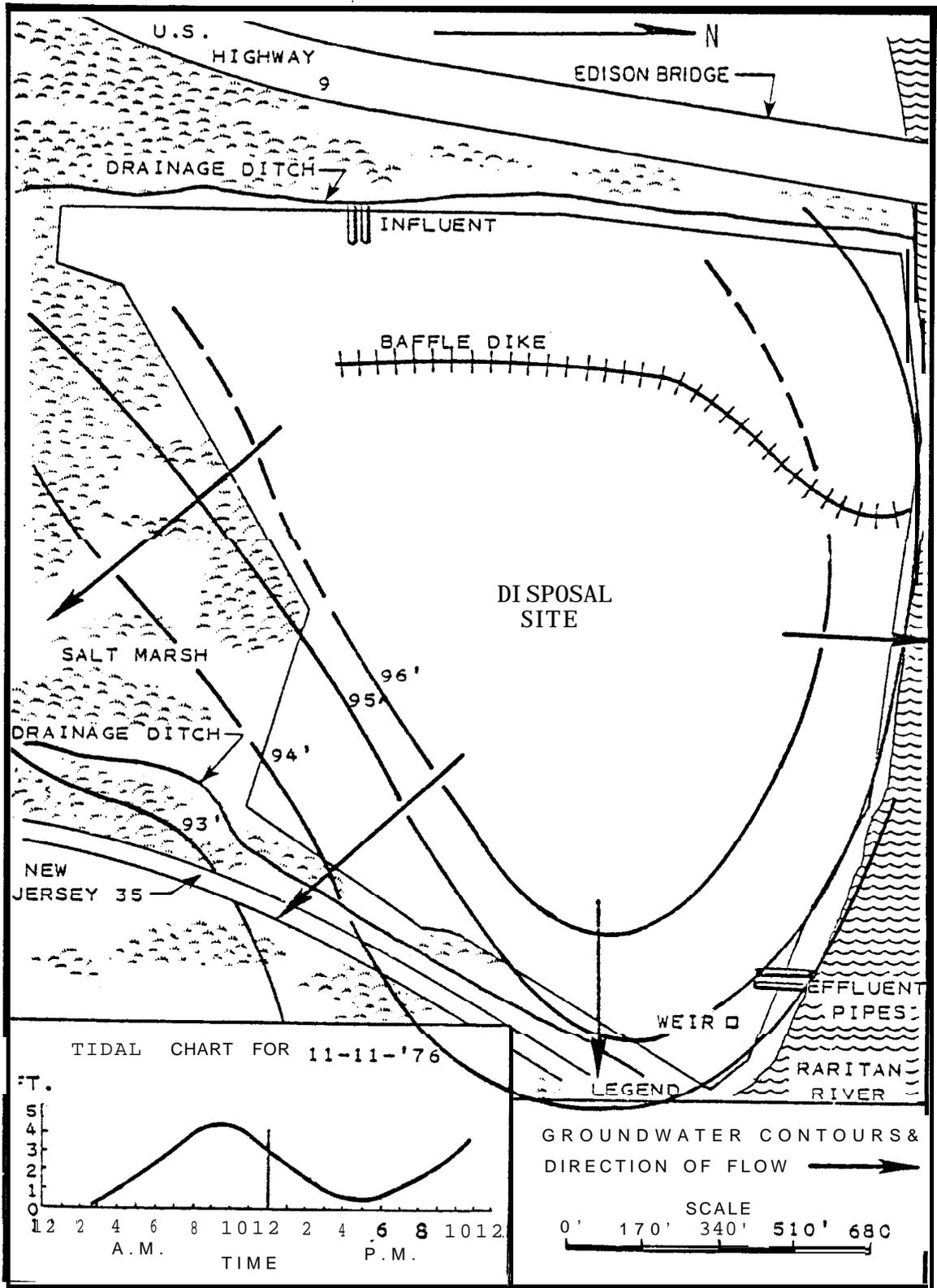


Figure 19. Groundwater contours at 12:00 p.m., November 11, 1976, Sayreville site

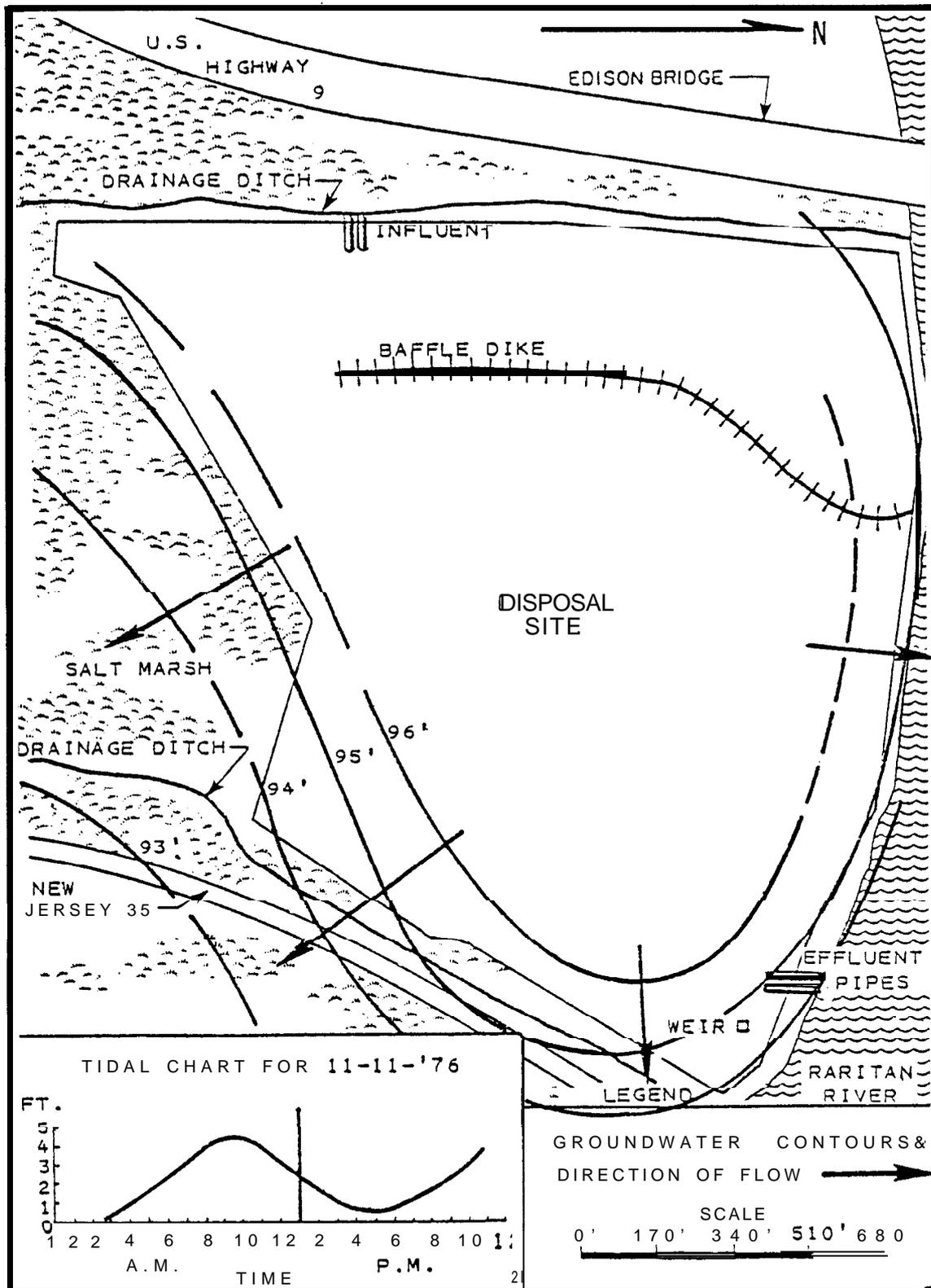


Figure 20. Groundwater contours at 1:00 p.m., November 11, 1976, Sayreville site

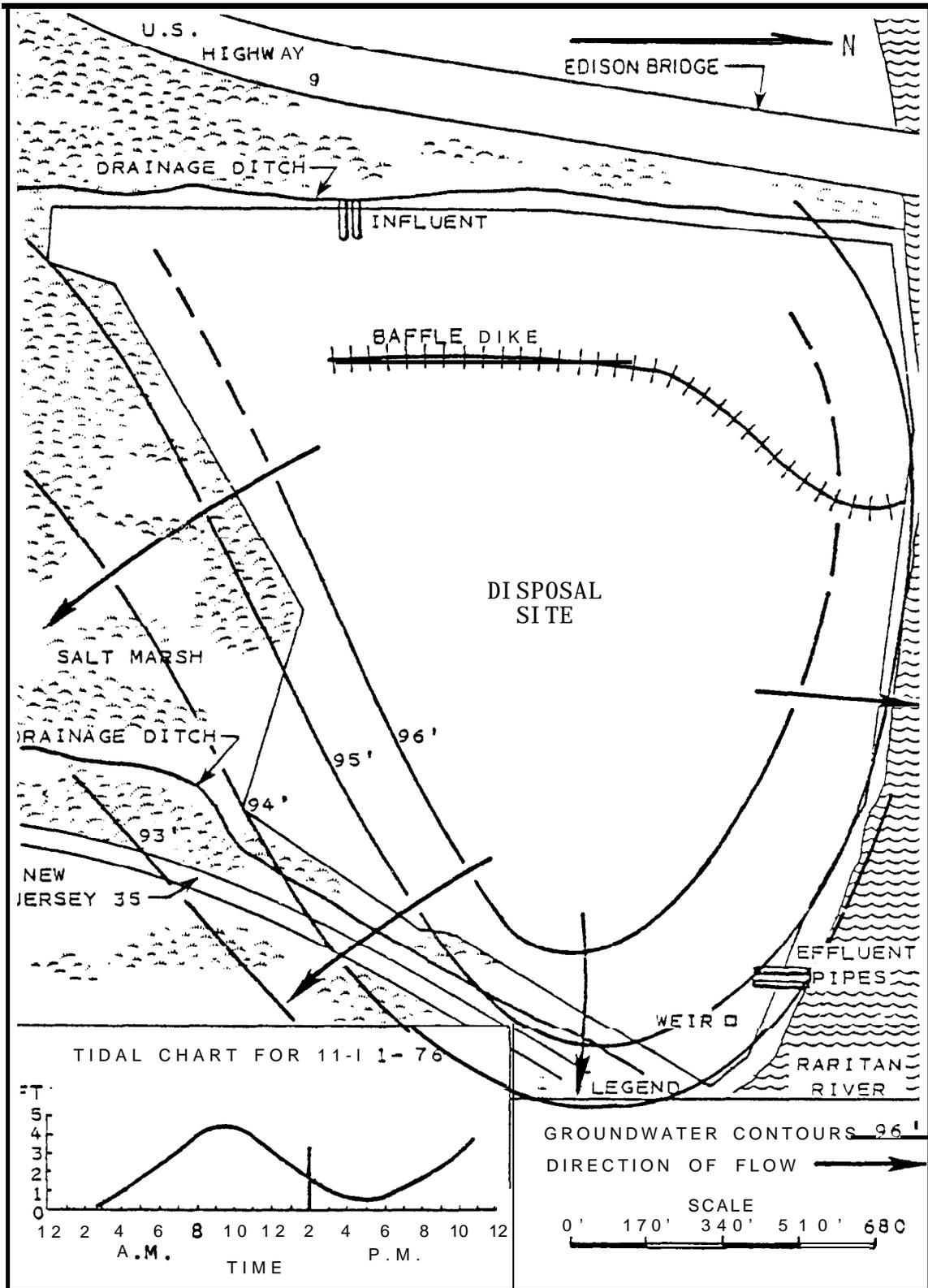


Figure 21. Groundwater contours at 2:00 p.m., November 11, 1976, Sayreville site

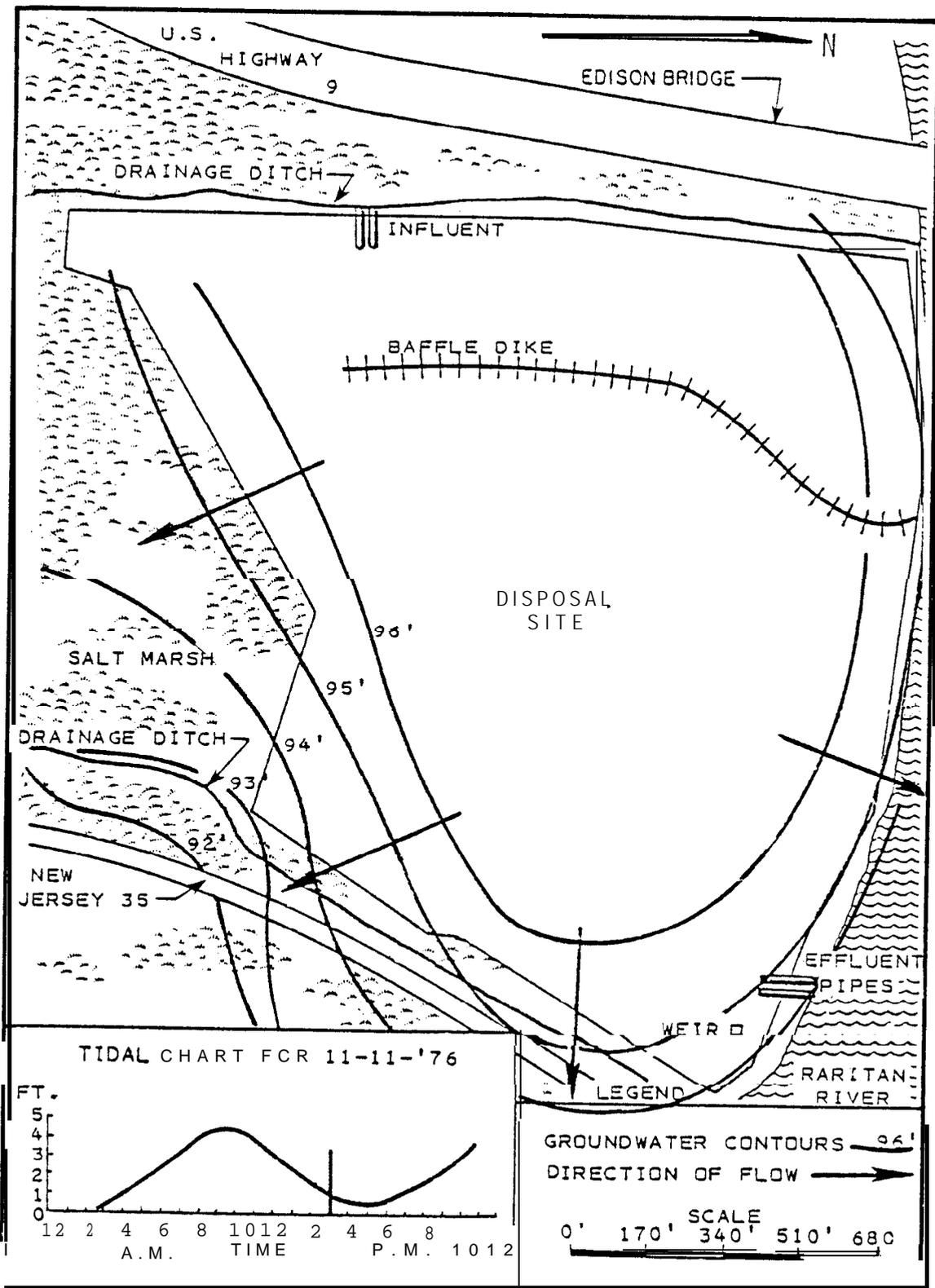


Figure 22. Groundwater contours at 3:00 p.m., November 11, 1976, Sayreville site

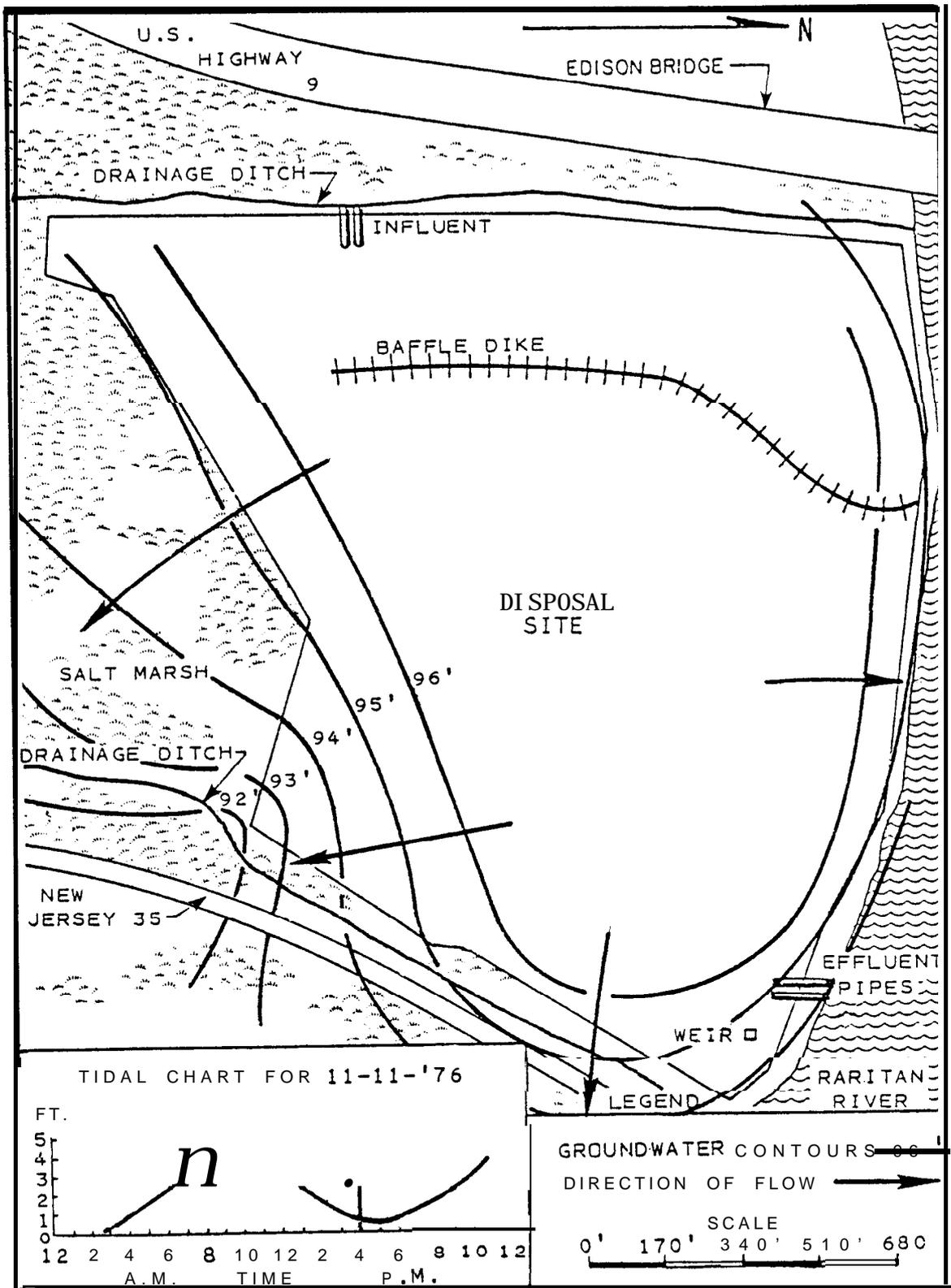


Figure 23. Groundwater contours at 4:00 p.m., November 11, 1976, Sayreville site

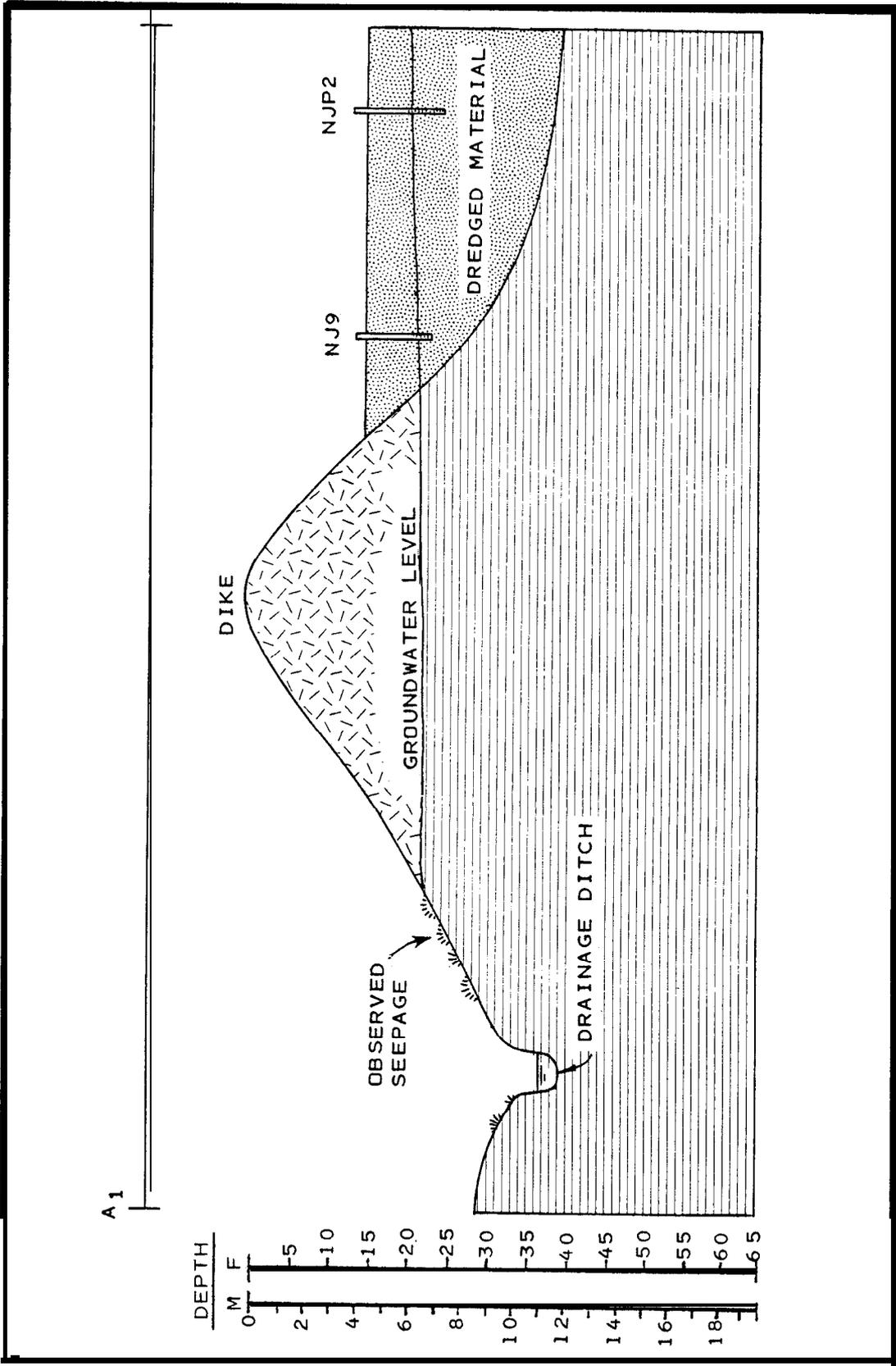


Figure 24. Cross section A₁-A

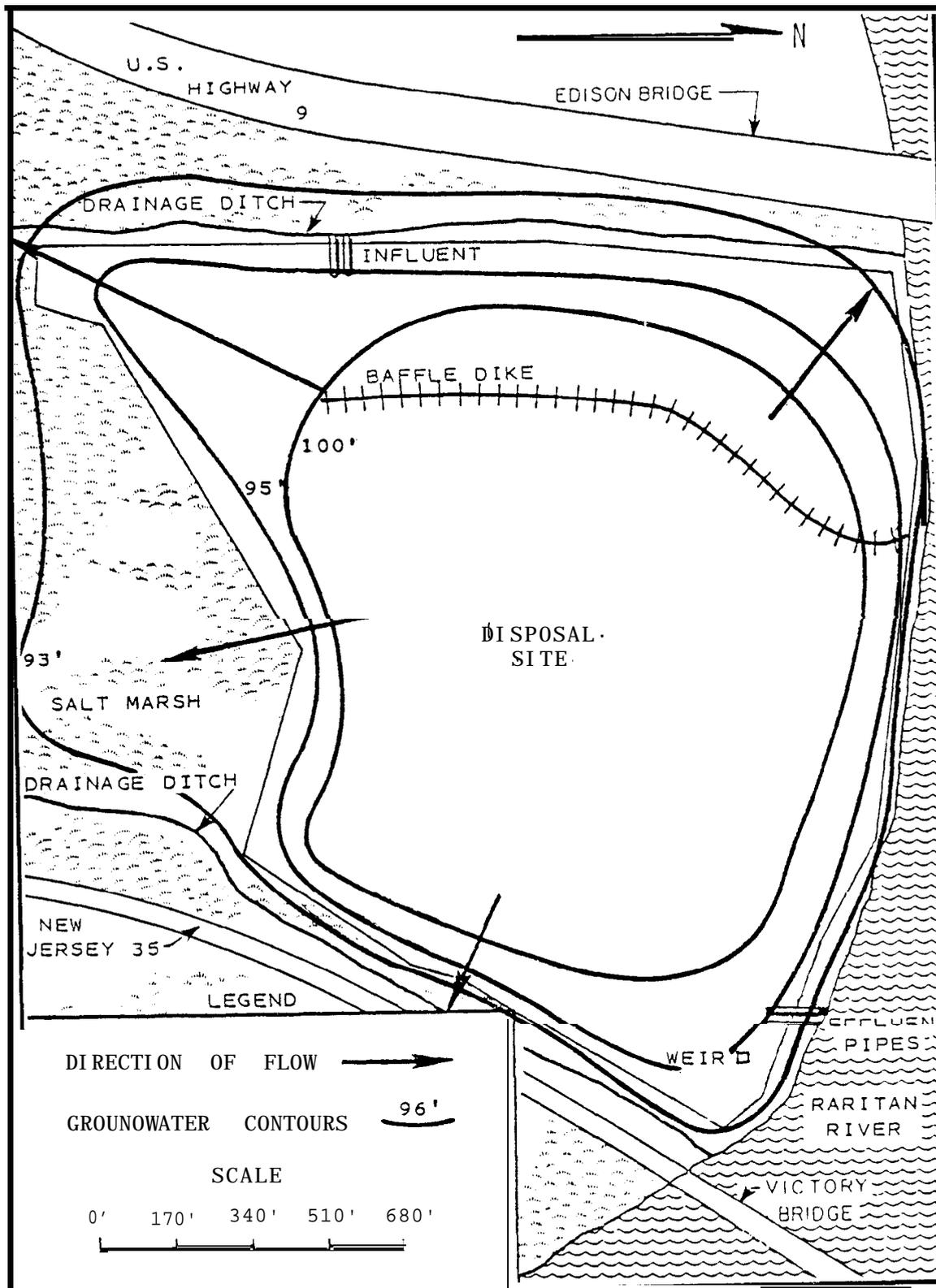


Figure 25. Water level contours on November 28, 1976, Sajreville site

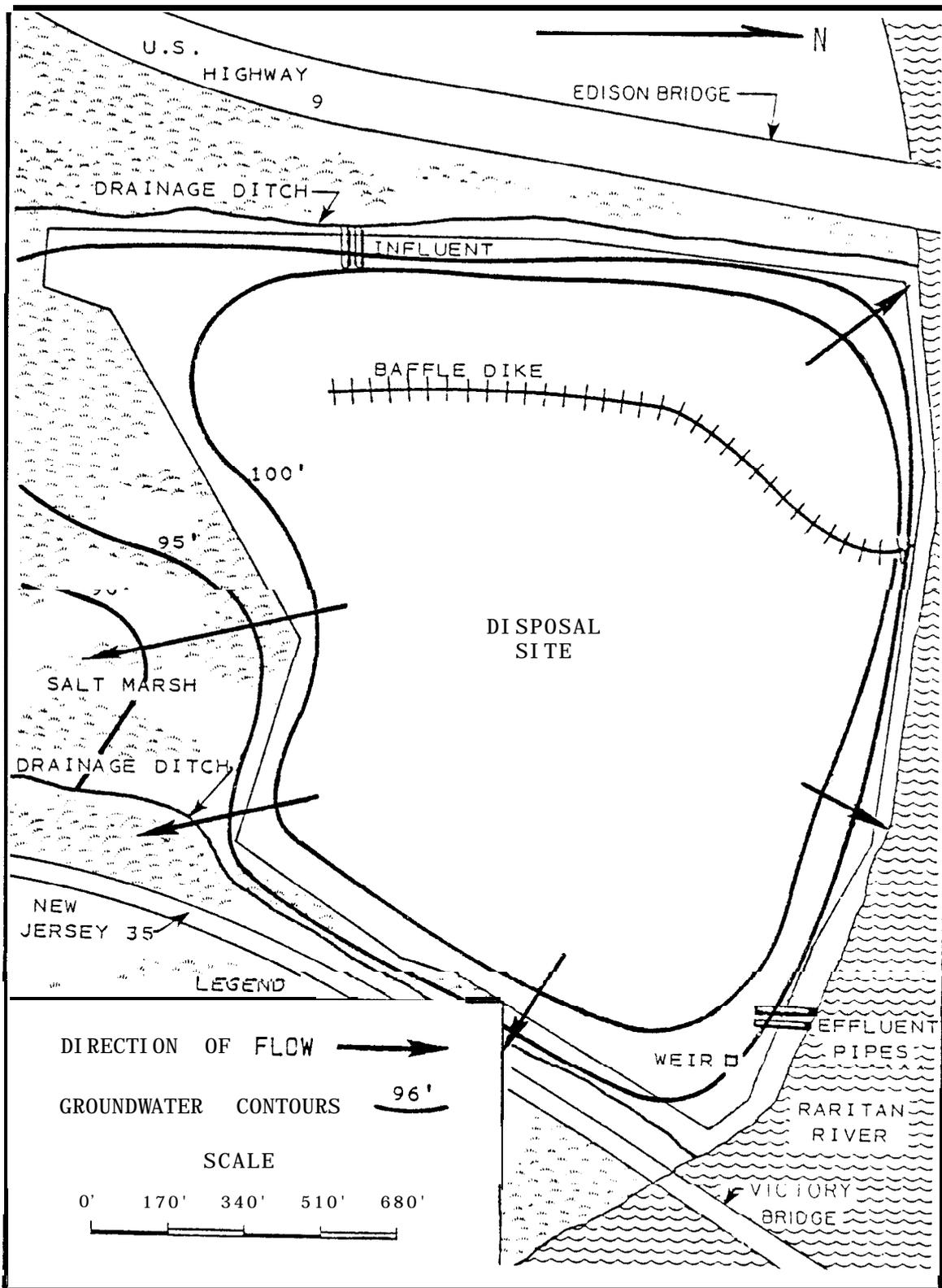


Figure 26. Water level contours on April 6, 1977, Sayreville site

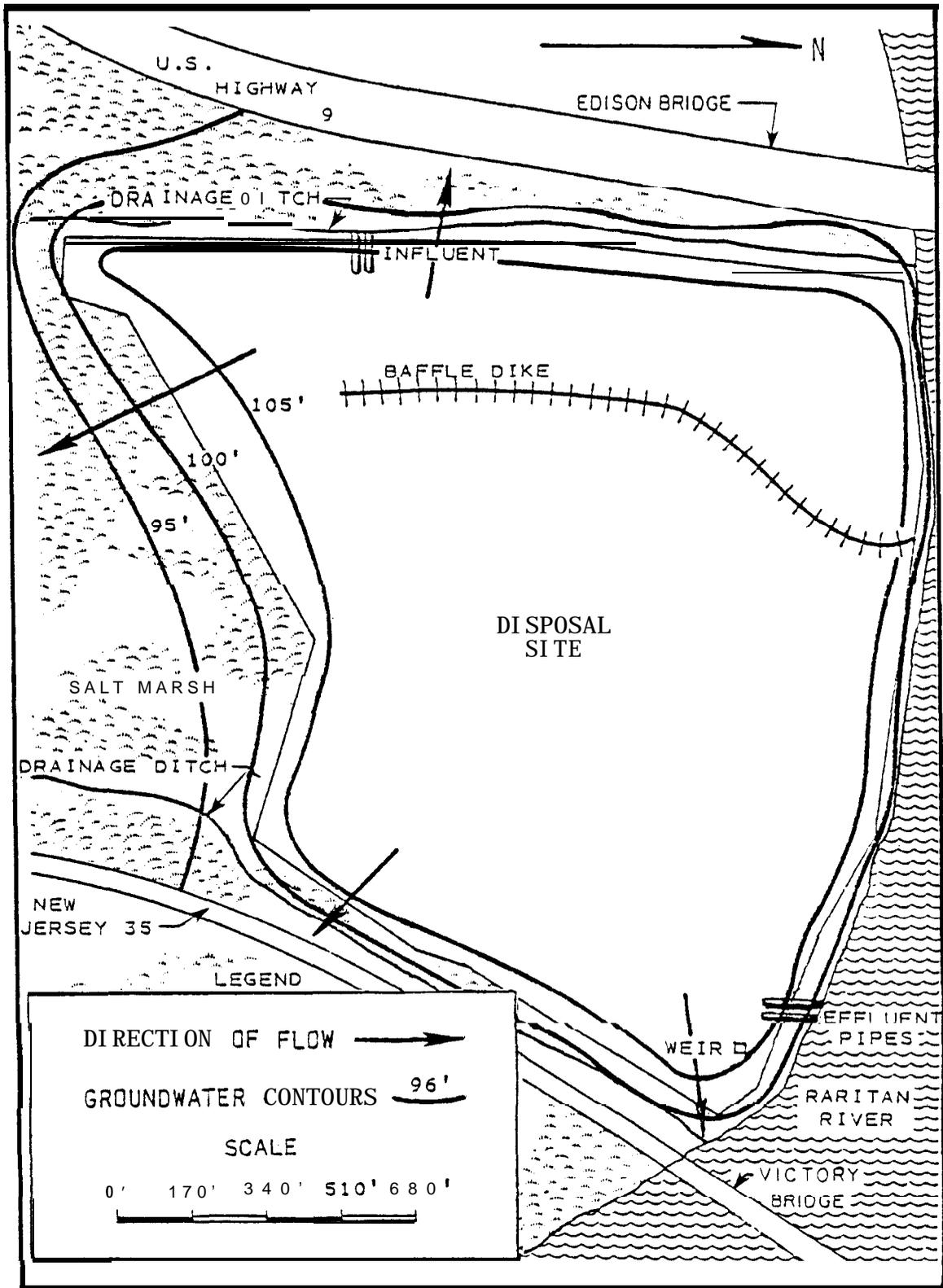


Figure 27. Water level contours on June 2, 1977, Sayreville site

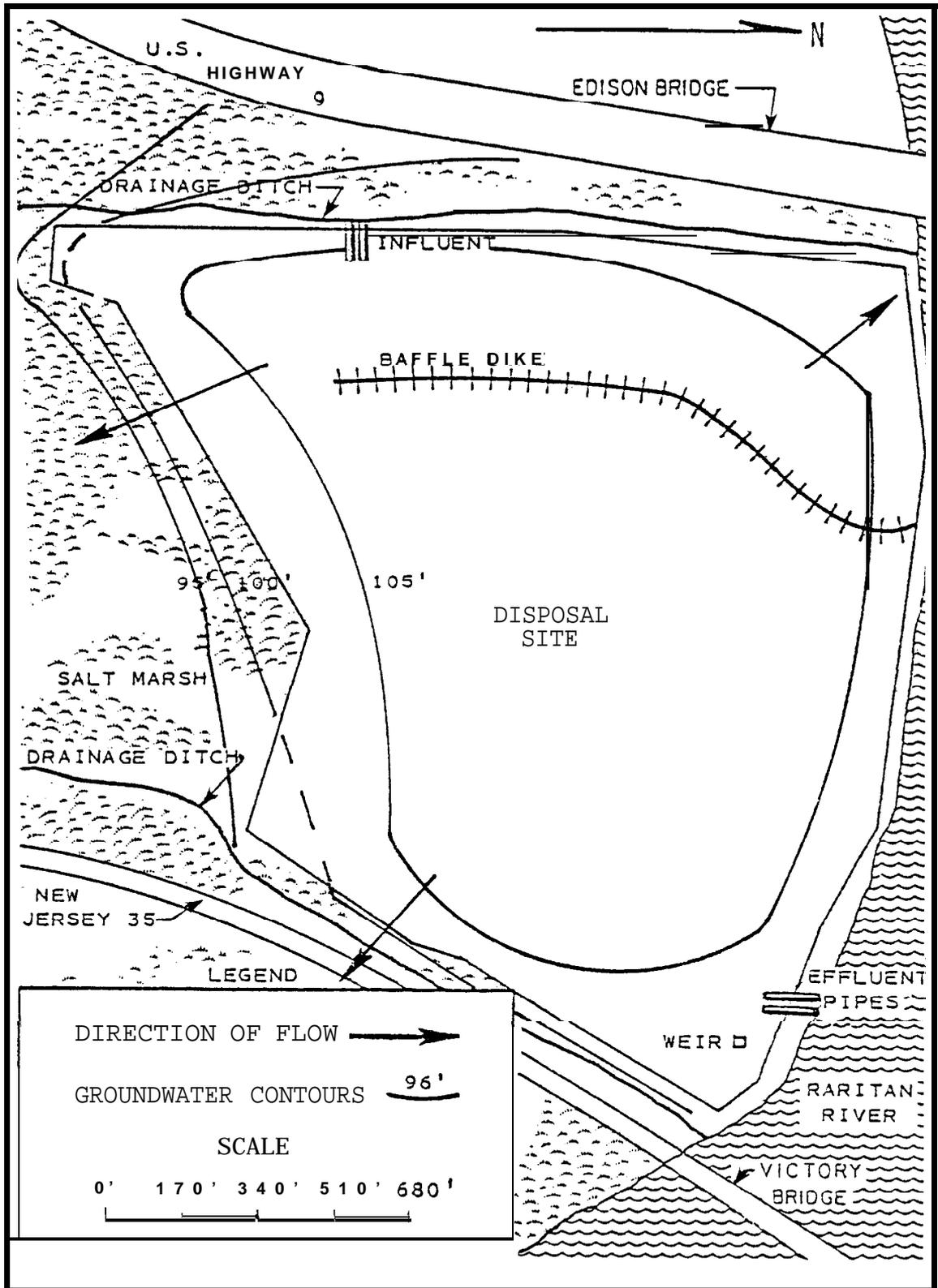


Figure 28. Water level contours on August 3, 1977, Sayreville site

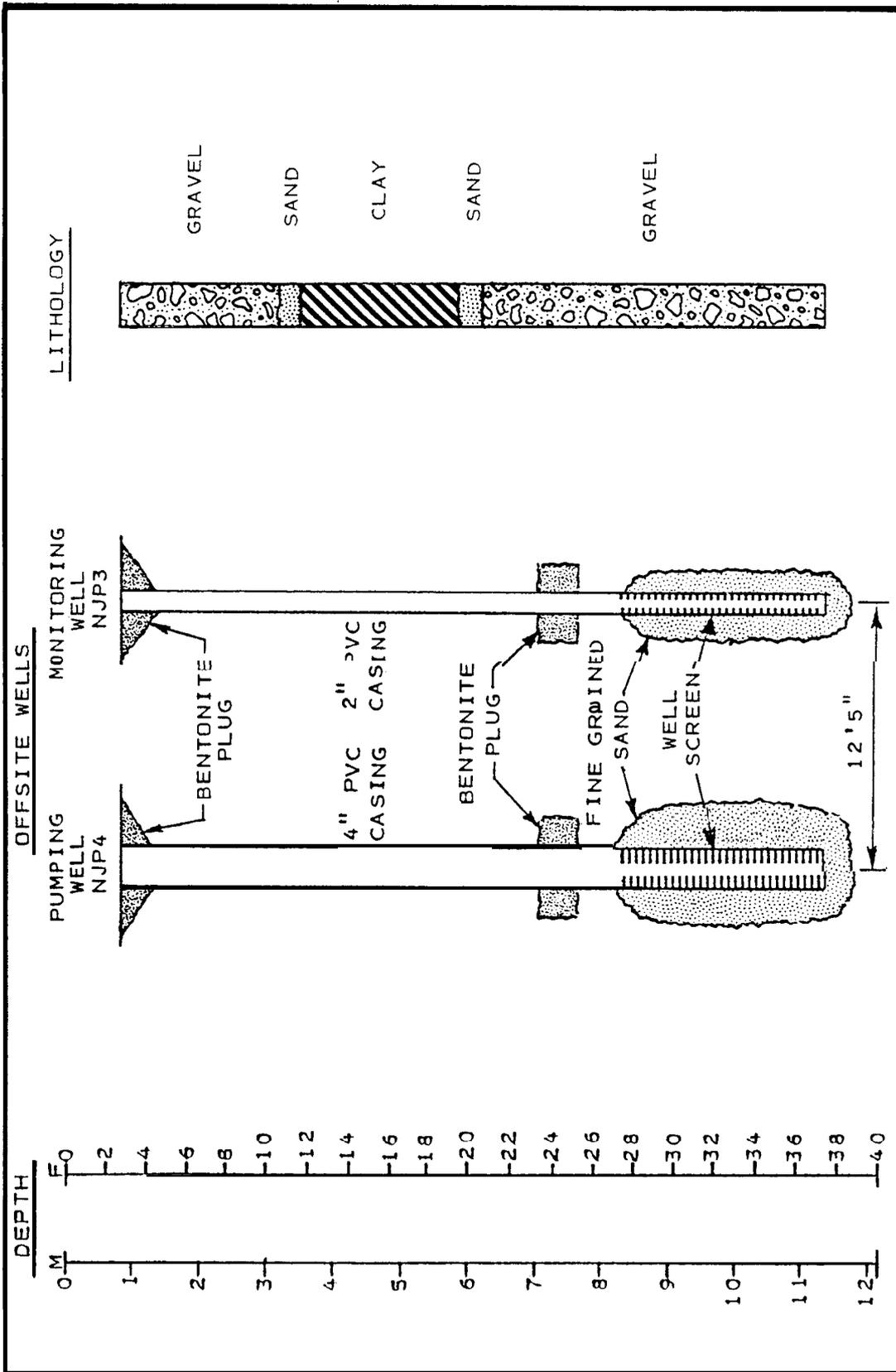


Figure 29. Offsite pumping and monitoring wells at Sayreville site.

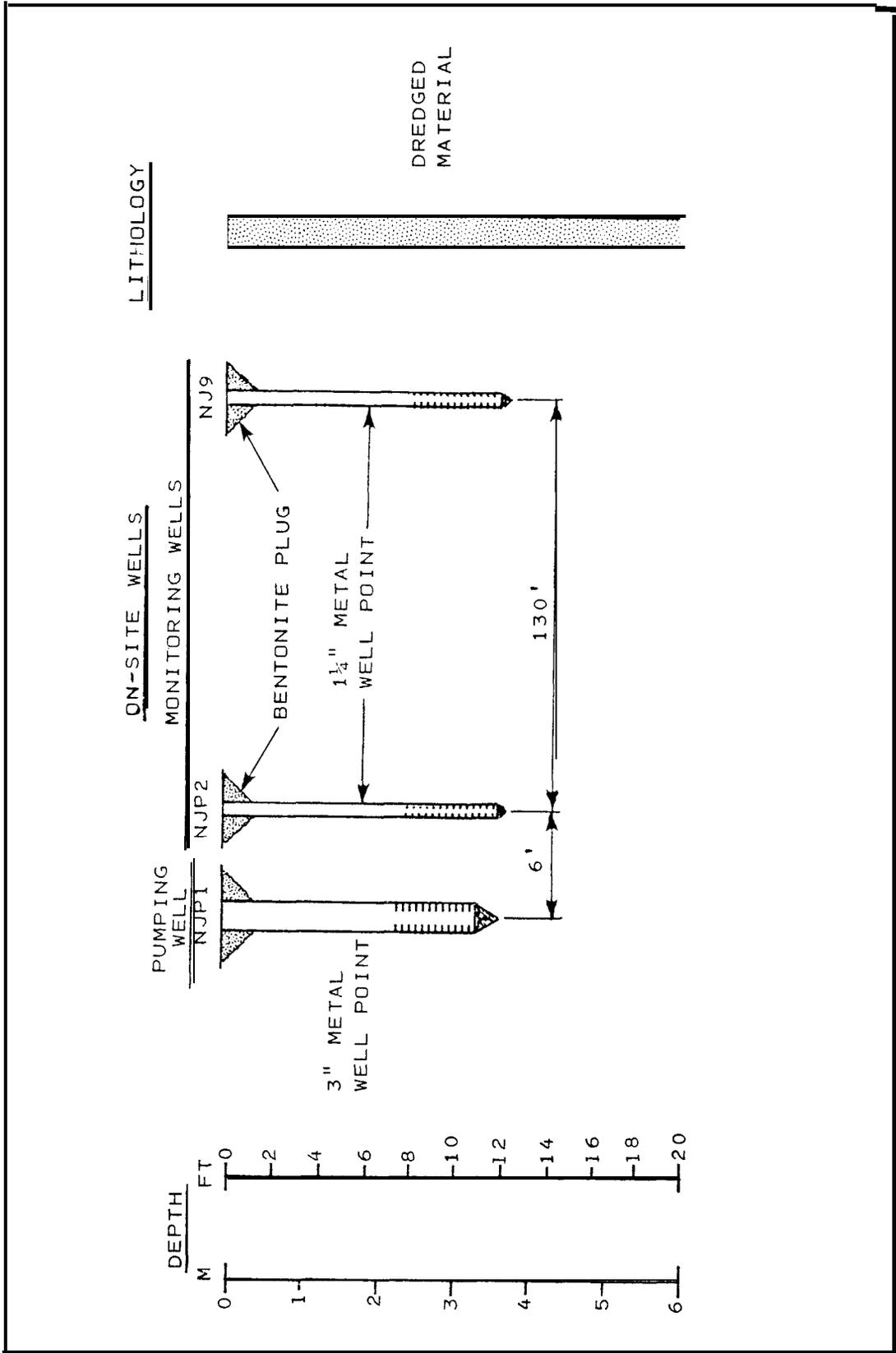
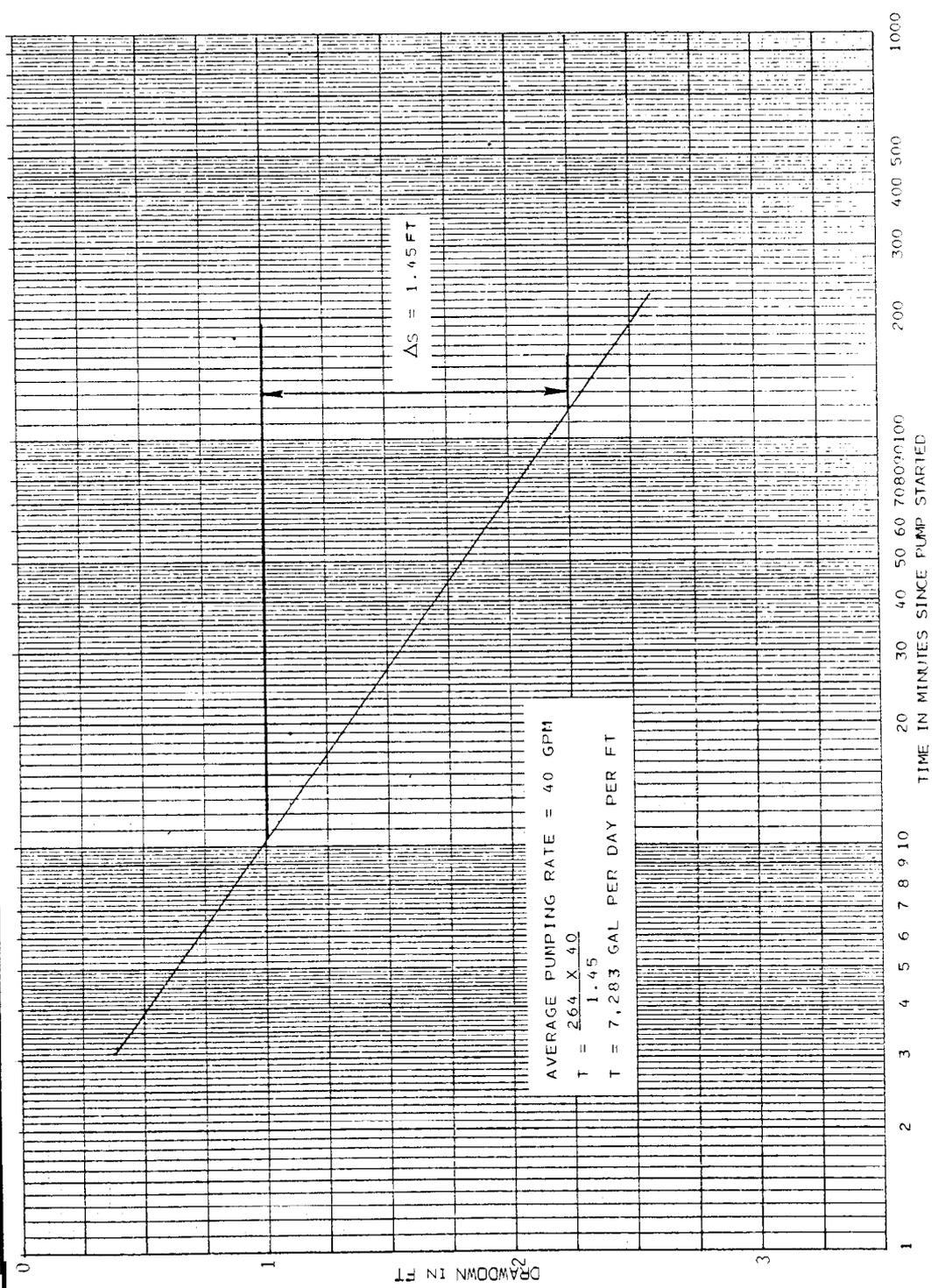


Figure 3U. Un-site pumping and monitoring wells at Sayreville site



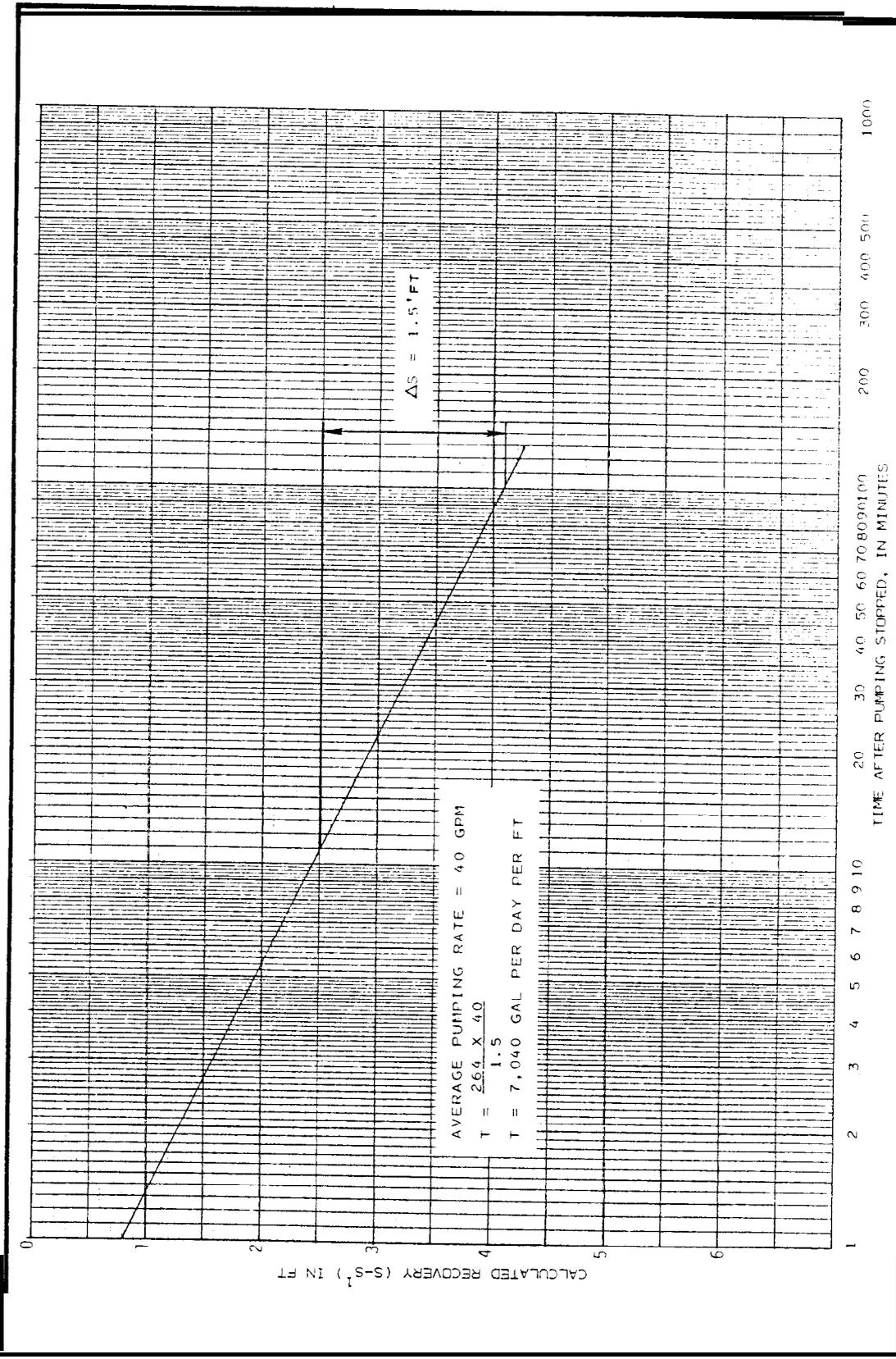


Figure 32. Recovery curve for off-site well NJP4

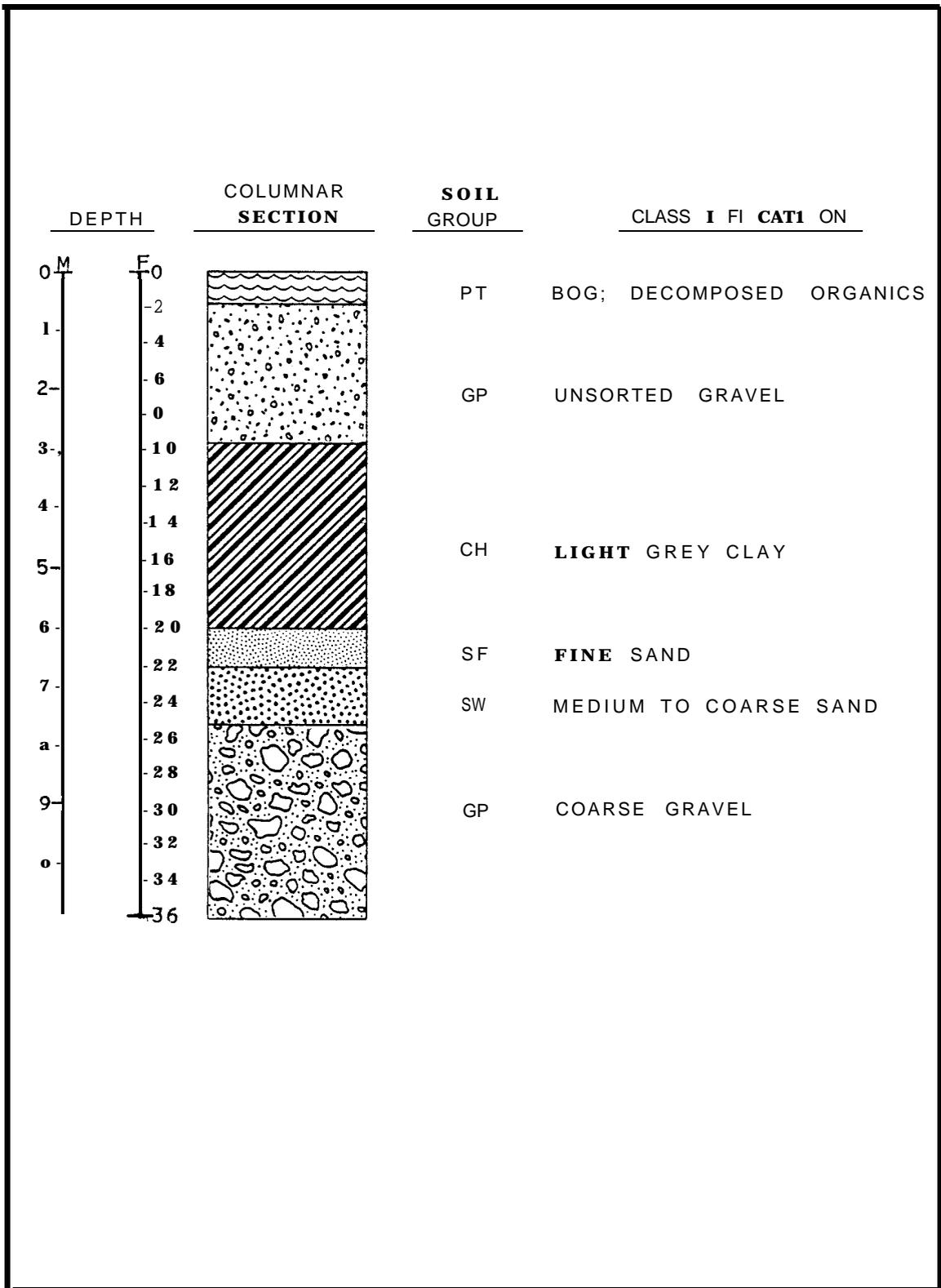


Figure 34 Generalized soil profile for Sayreville site

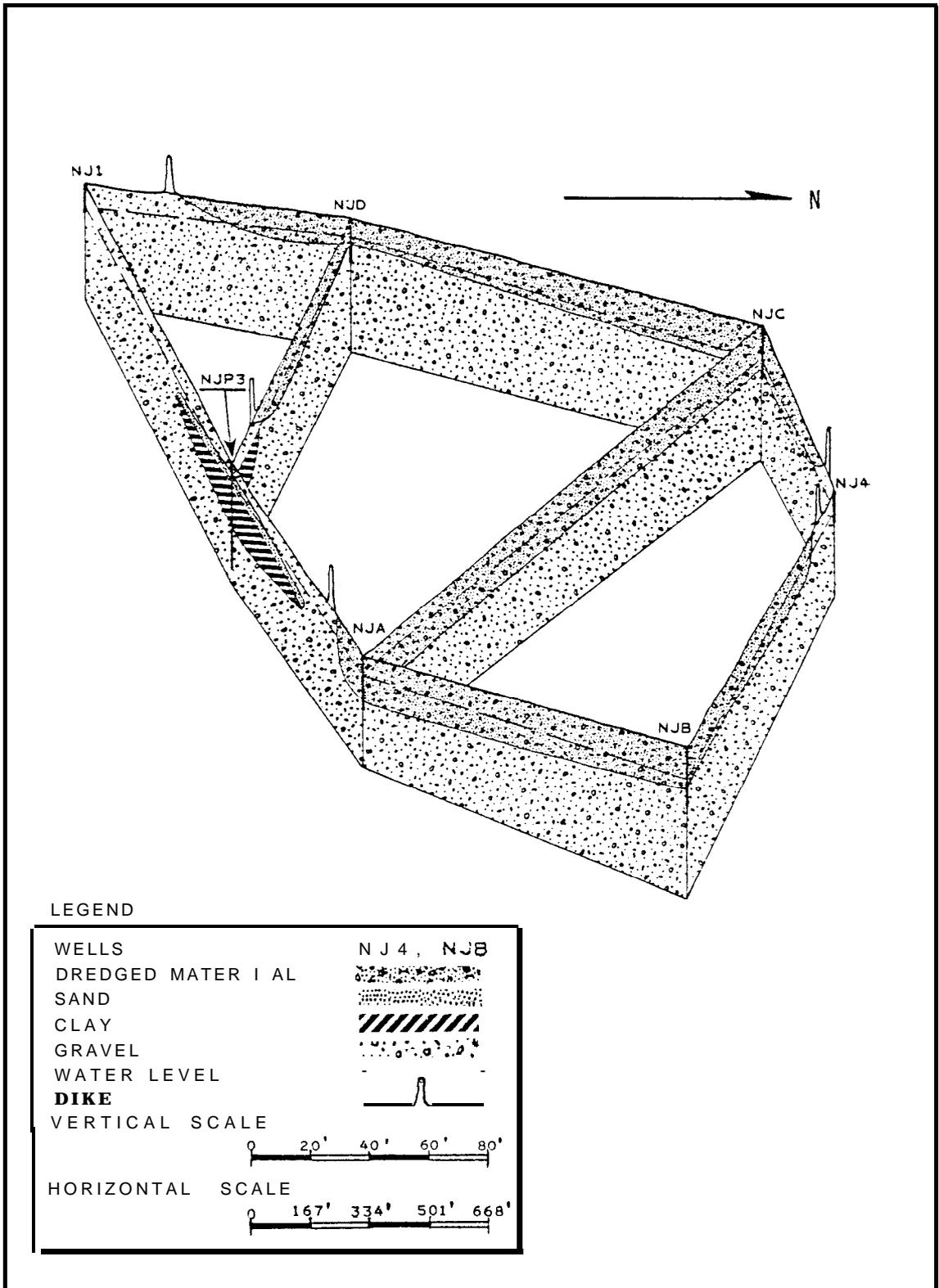


Figure 35. Fence diagram for Sayreville site



Figure 36. Regional map for Houston site

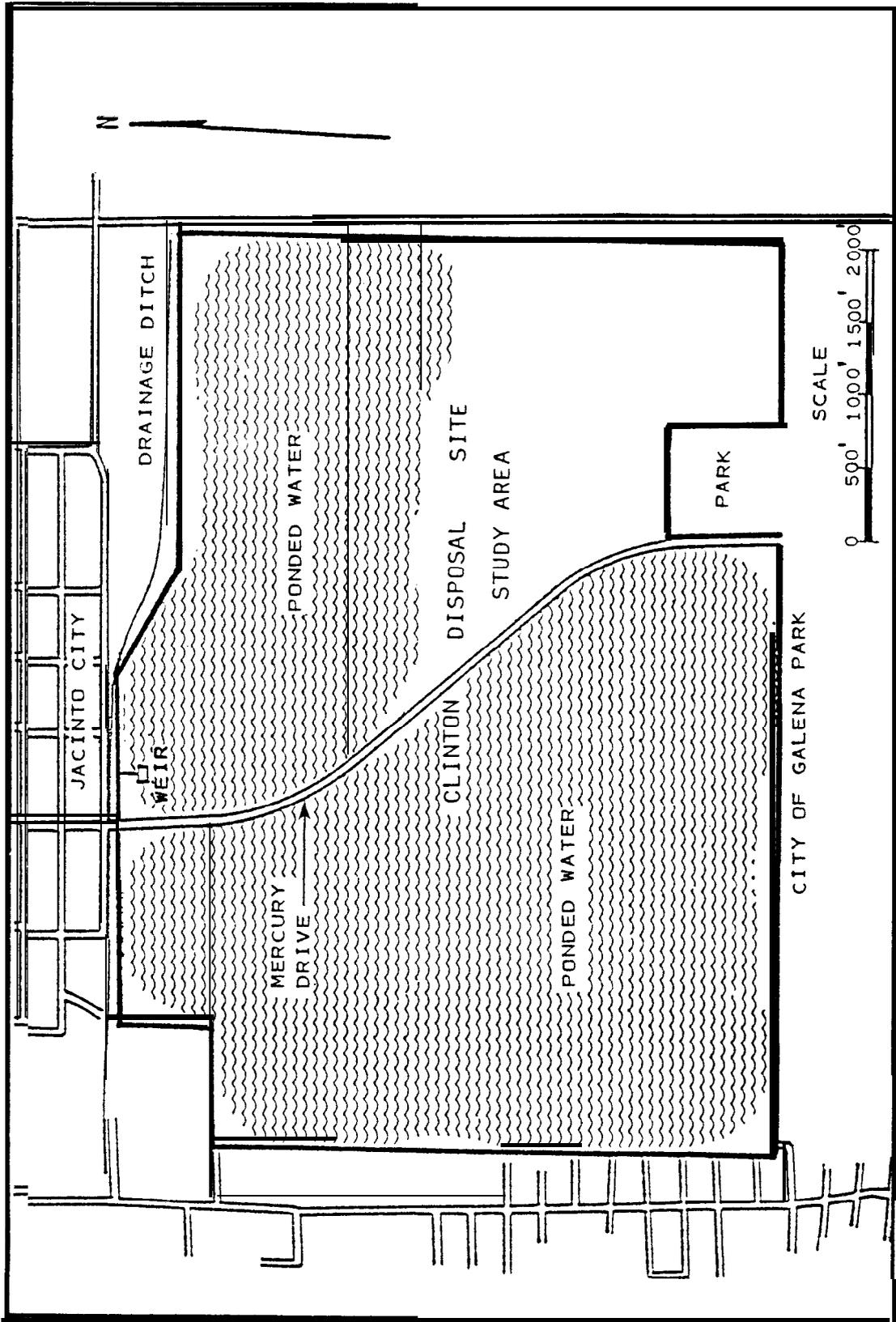


Figure 37. Map of Houston disposal site

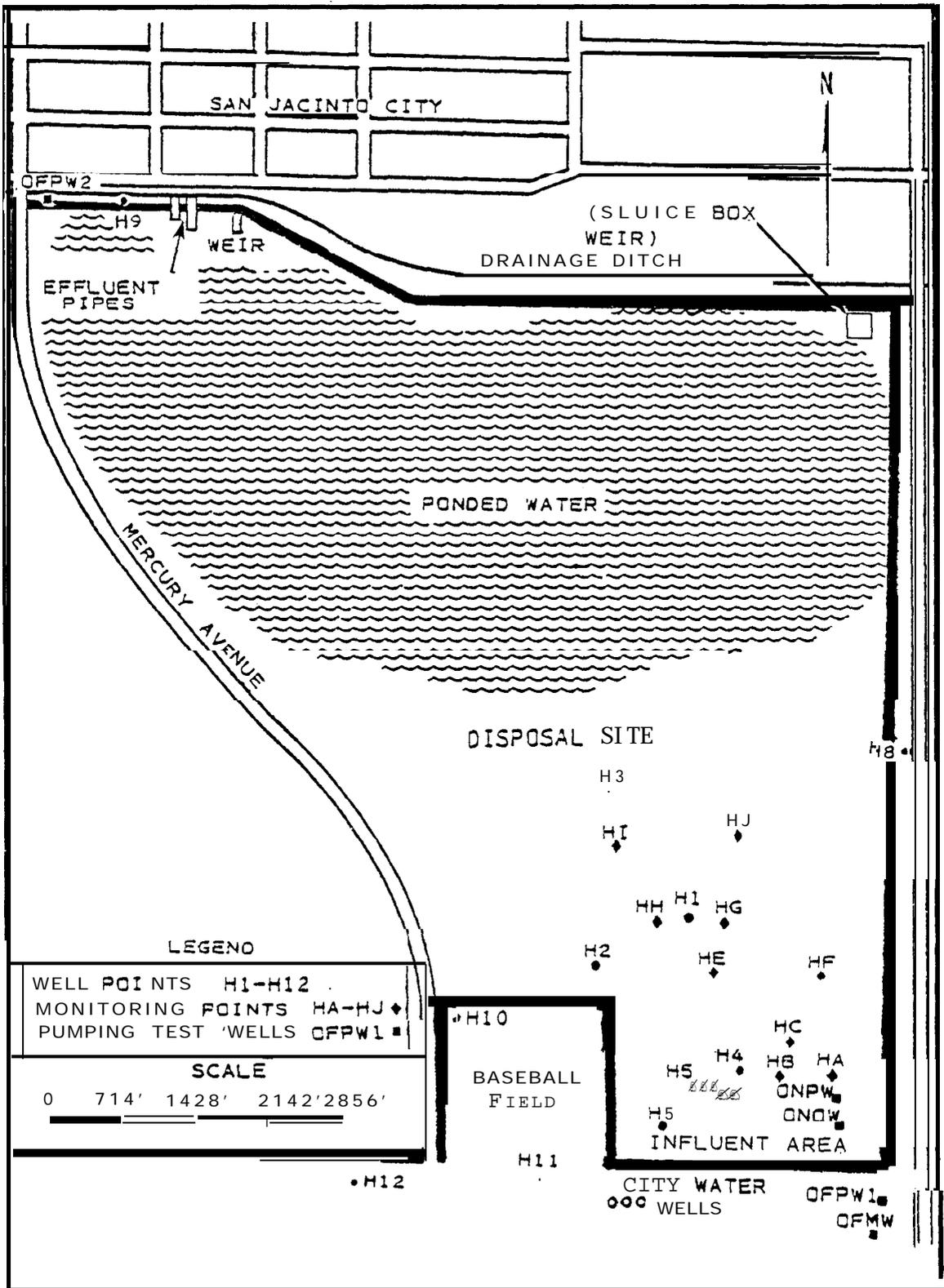


Figure 38. Houston site

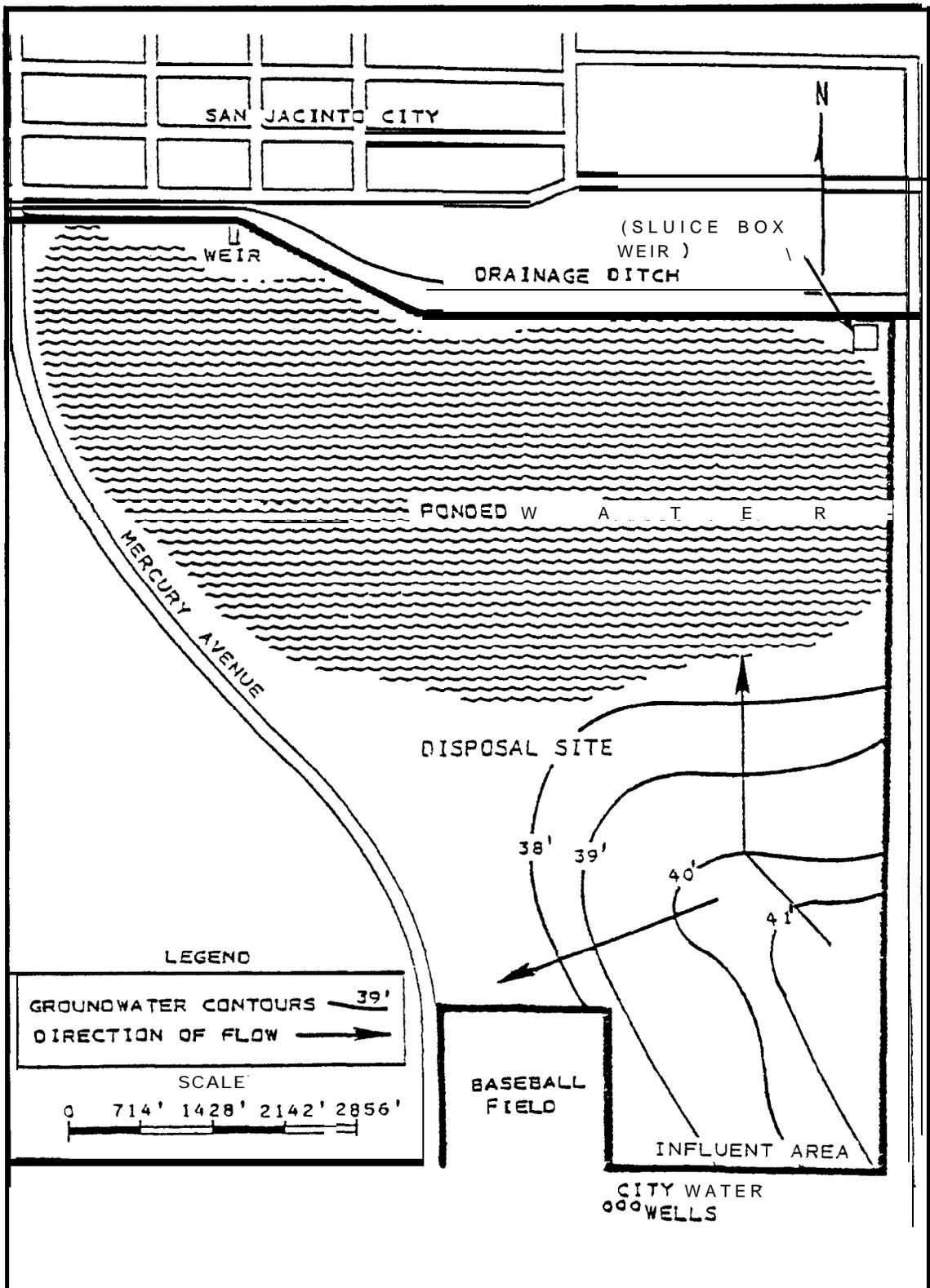


Figure 39 . Water level contours on November 6, 1976, Houston, Texas

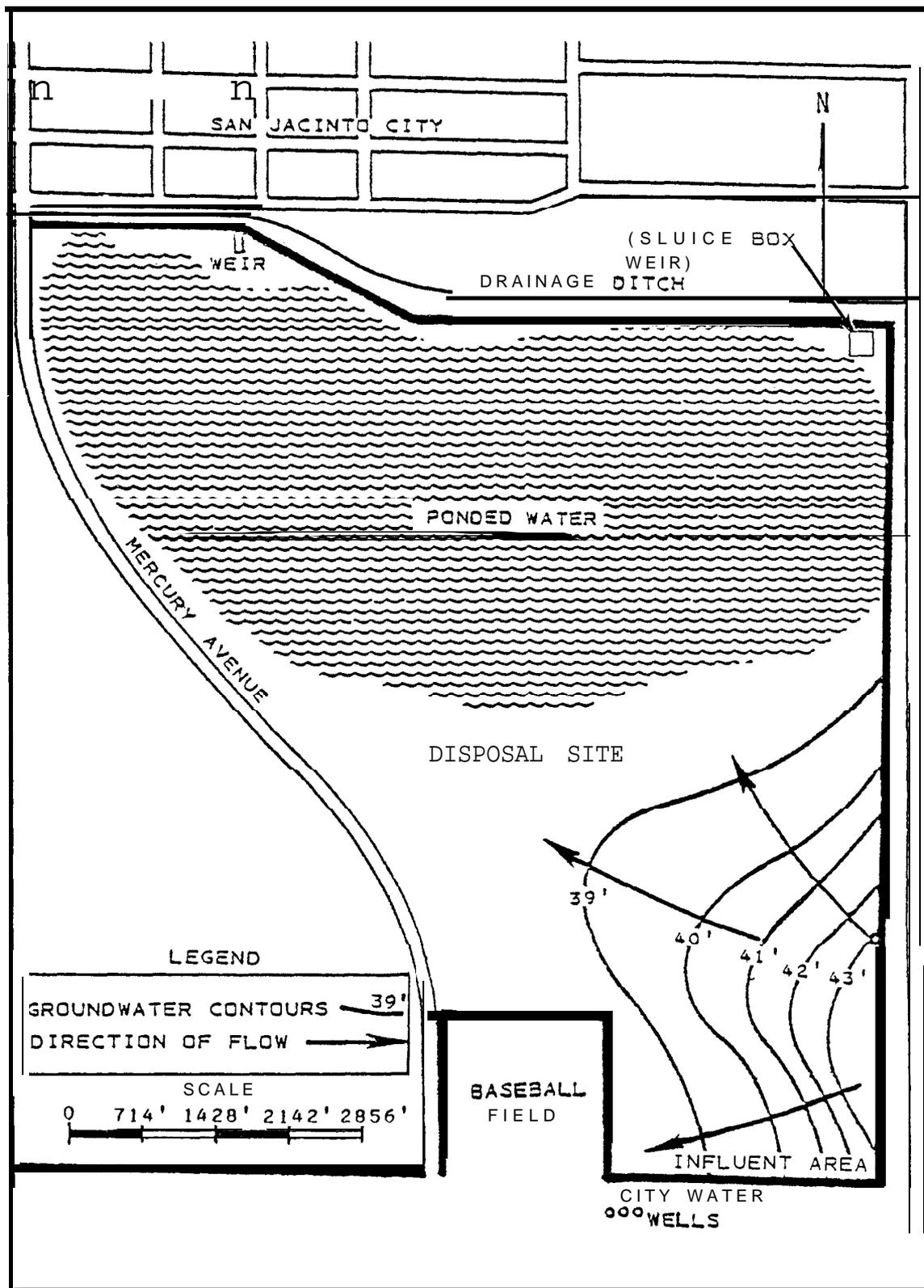


Figure 40 Water level contours on December 10, 1976, Houston site

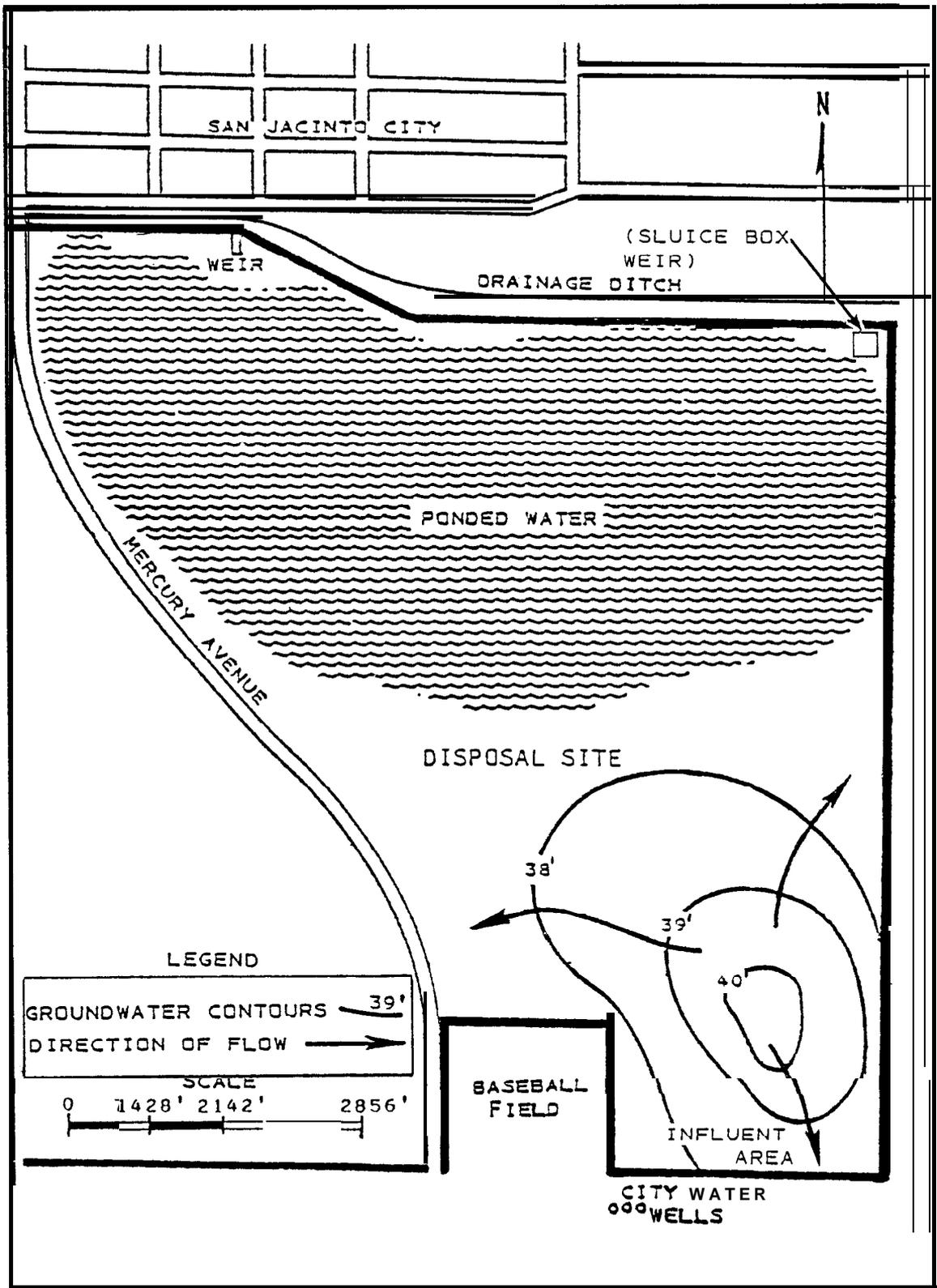


Figure 41. Water level contours on March 25, 1977, Houston site

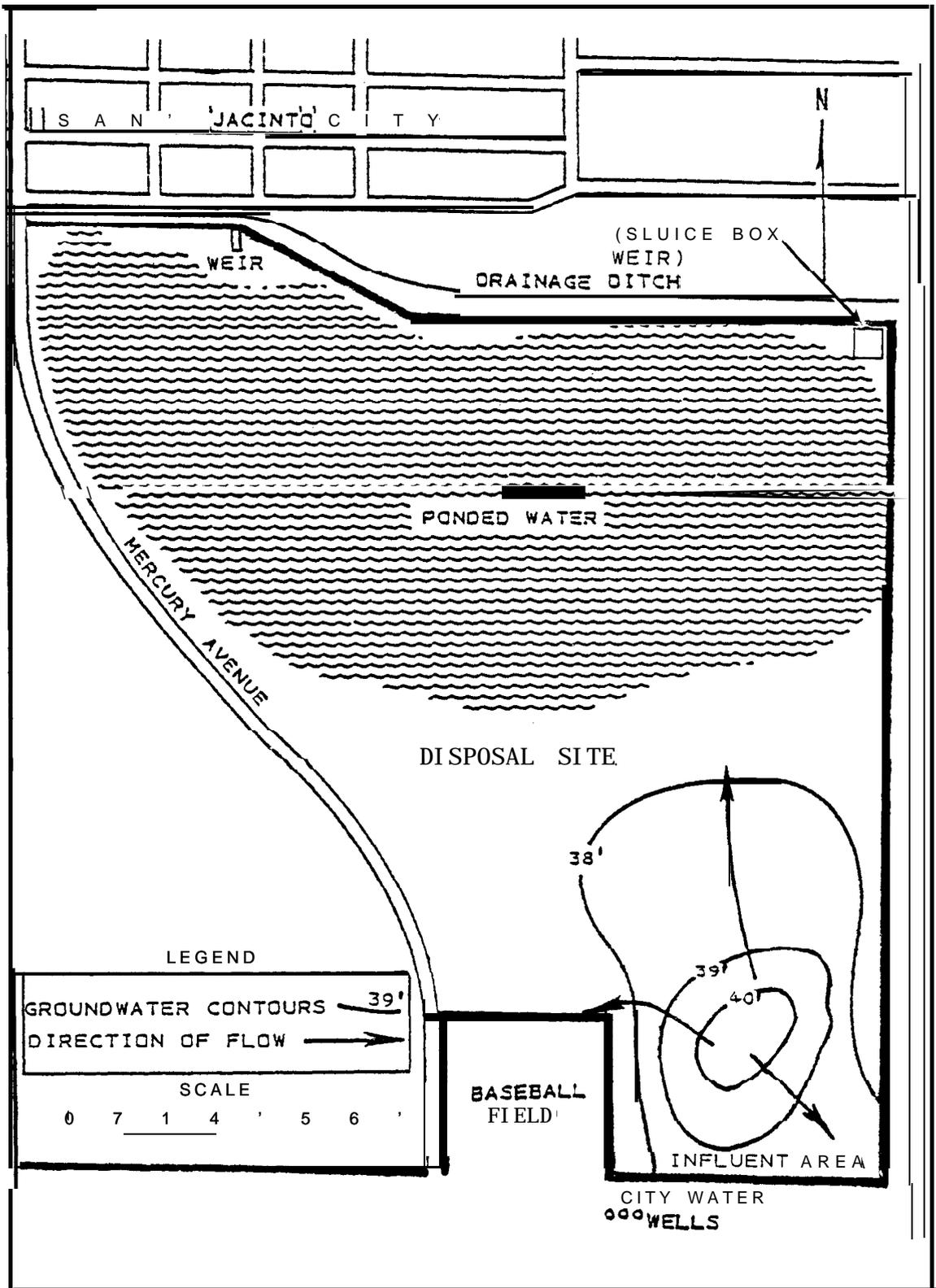


Figure 42. Water level contours on June 12, 1977, Houston site

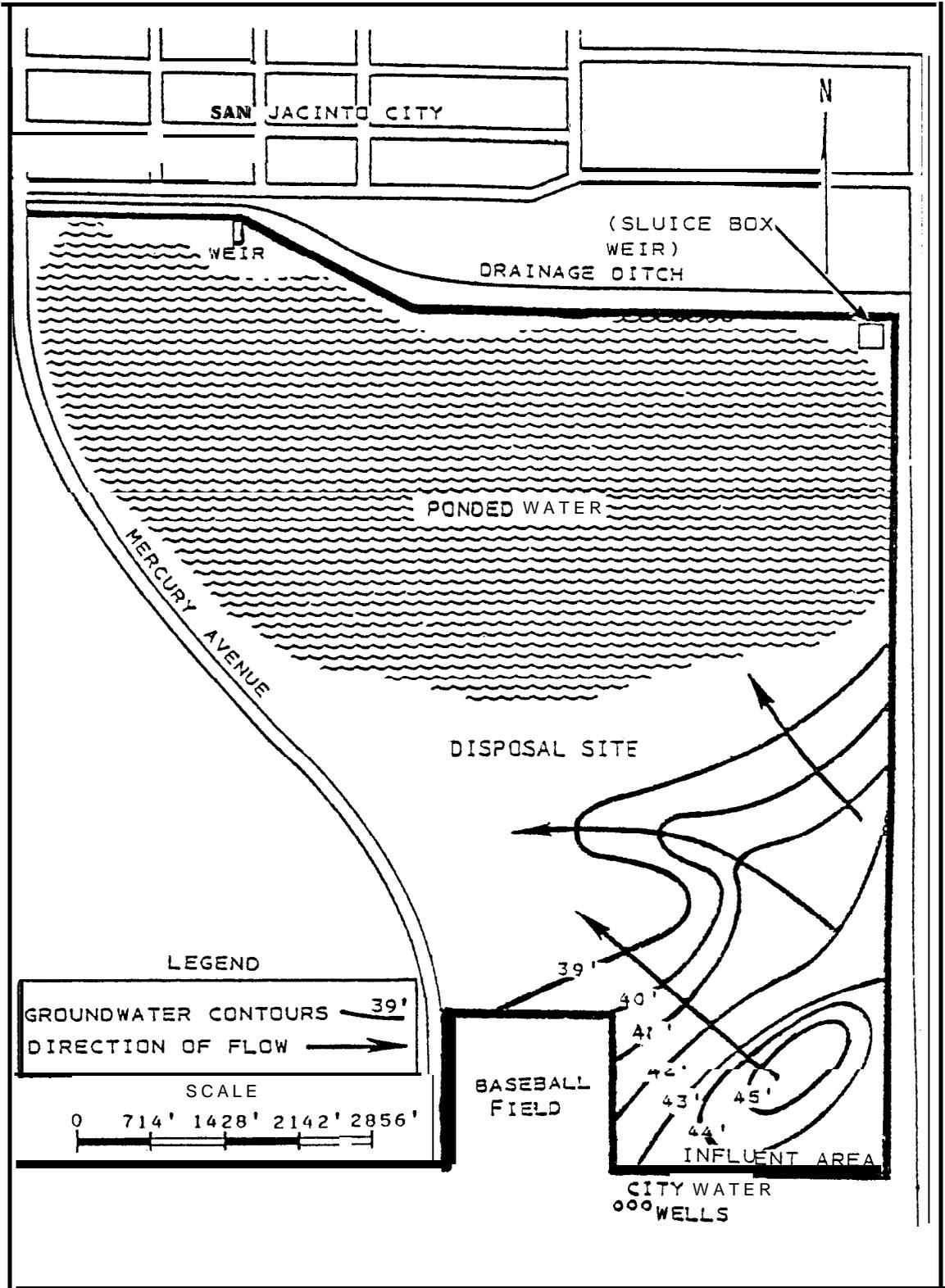


Figure 43.. Water level contours on July 30, 1977, Houston site

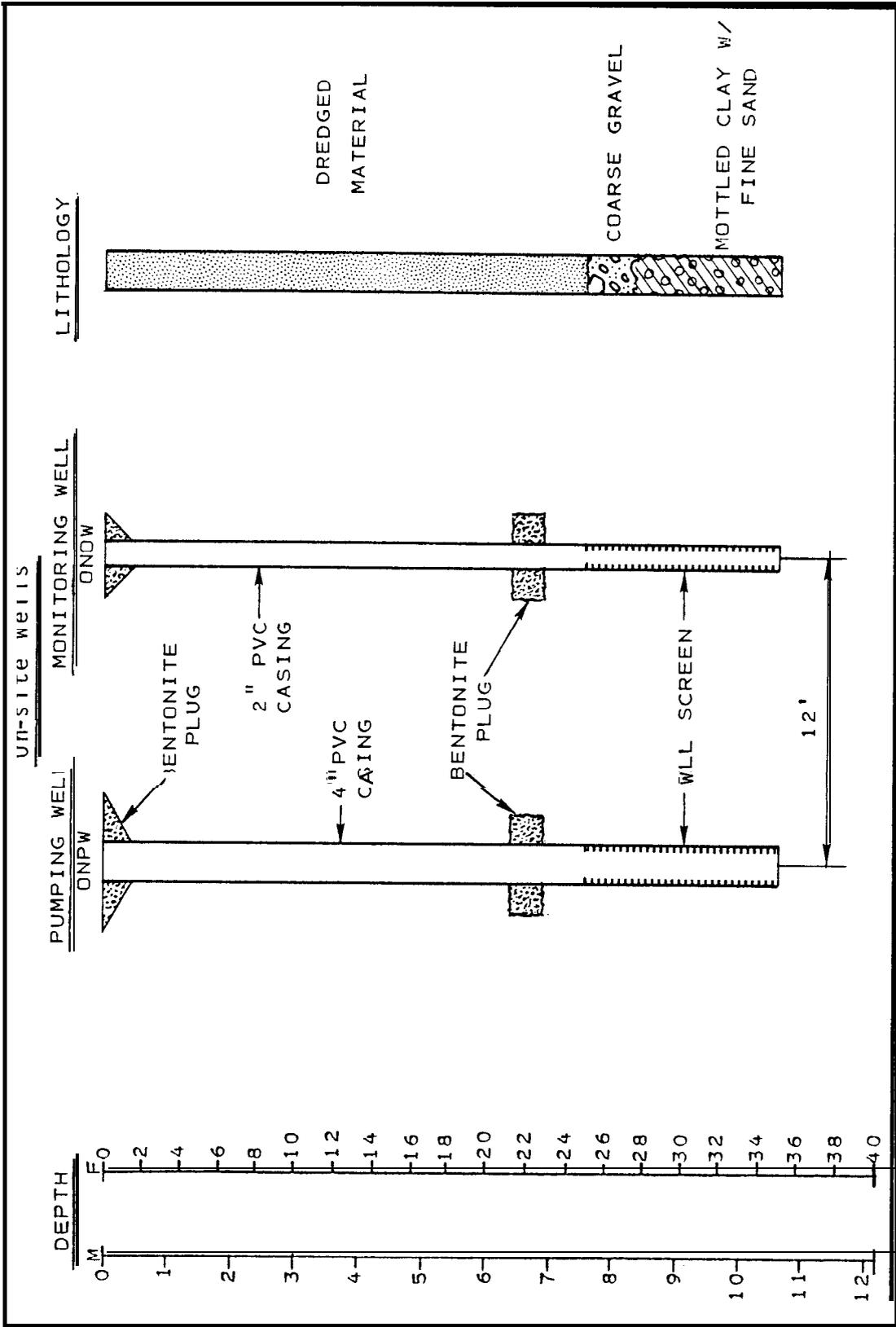


Figure 44: On-site pumping and monitoring wells at Houston site

Off-site Wells

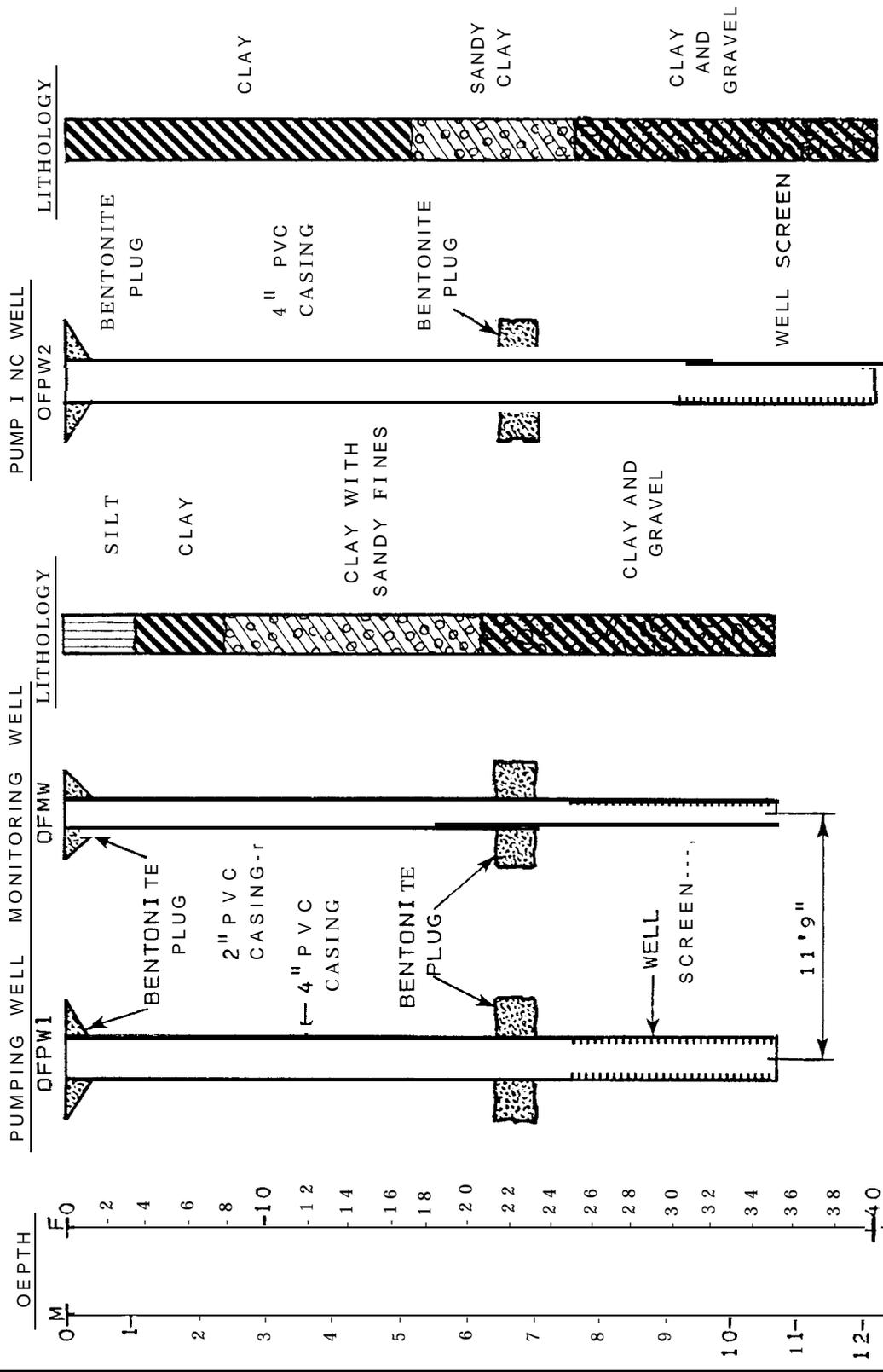


Figure 45. Off-site pumping and monitoring wells at Houston site

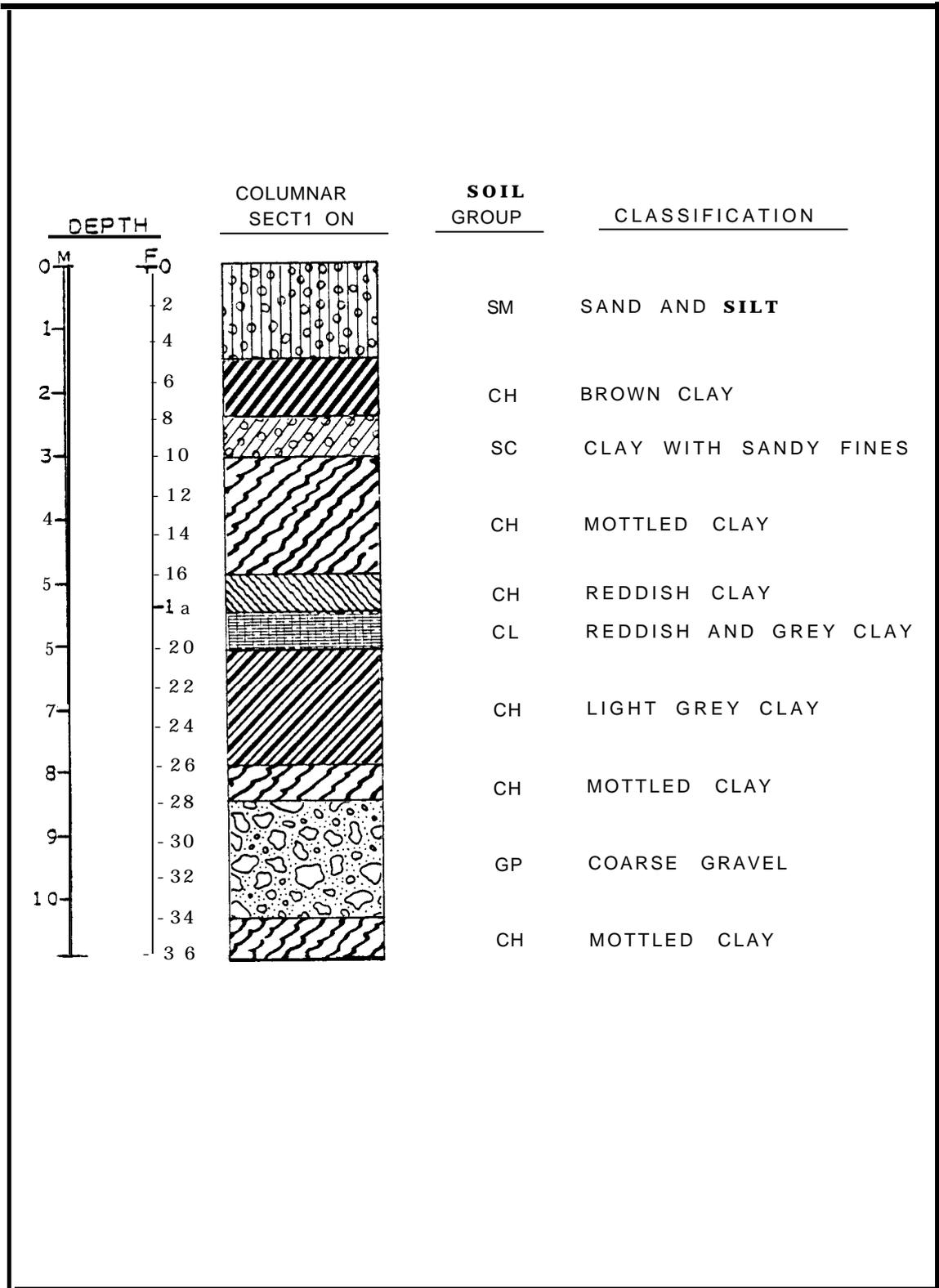


Figure 47. Generalized soil profile for Houston

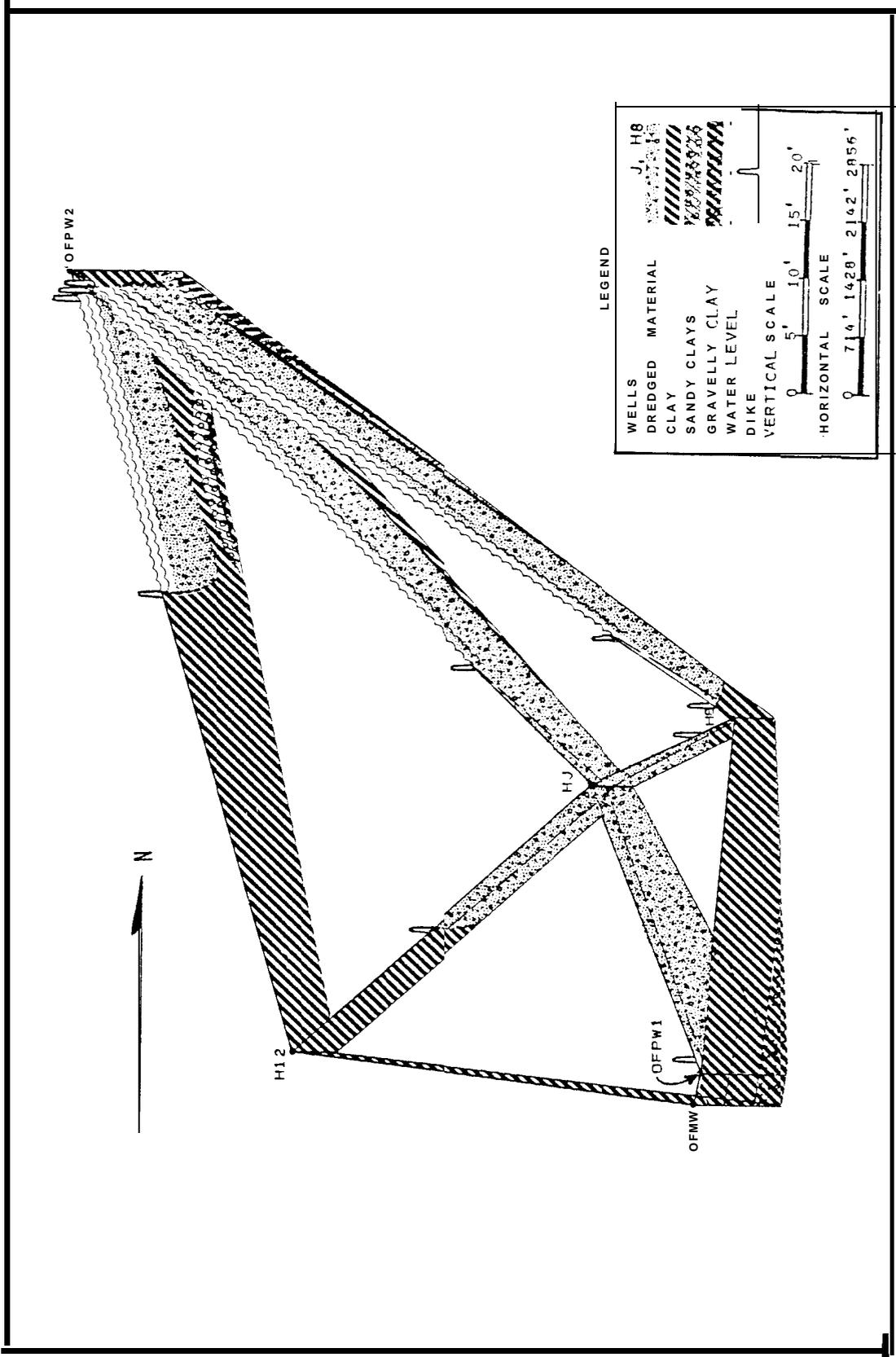


Figure 48. Fence diagram for Houston site

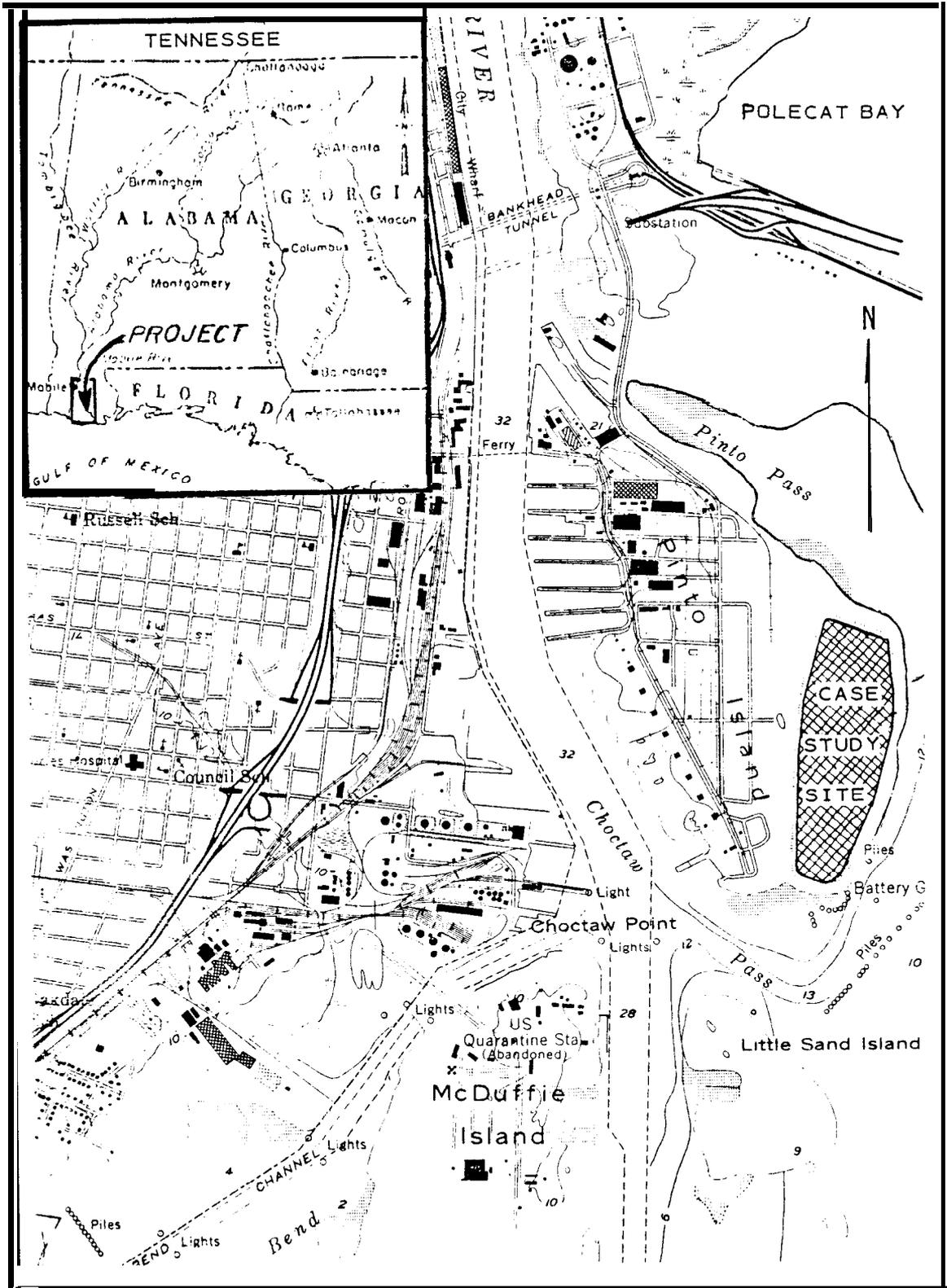


Figure 49. Regional map for Pinto Island site

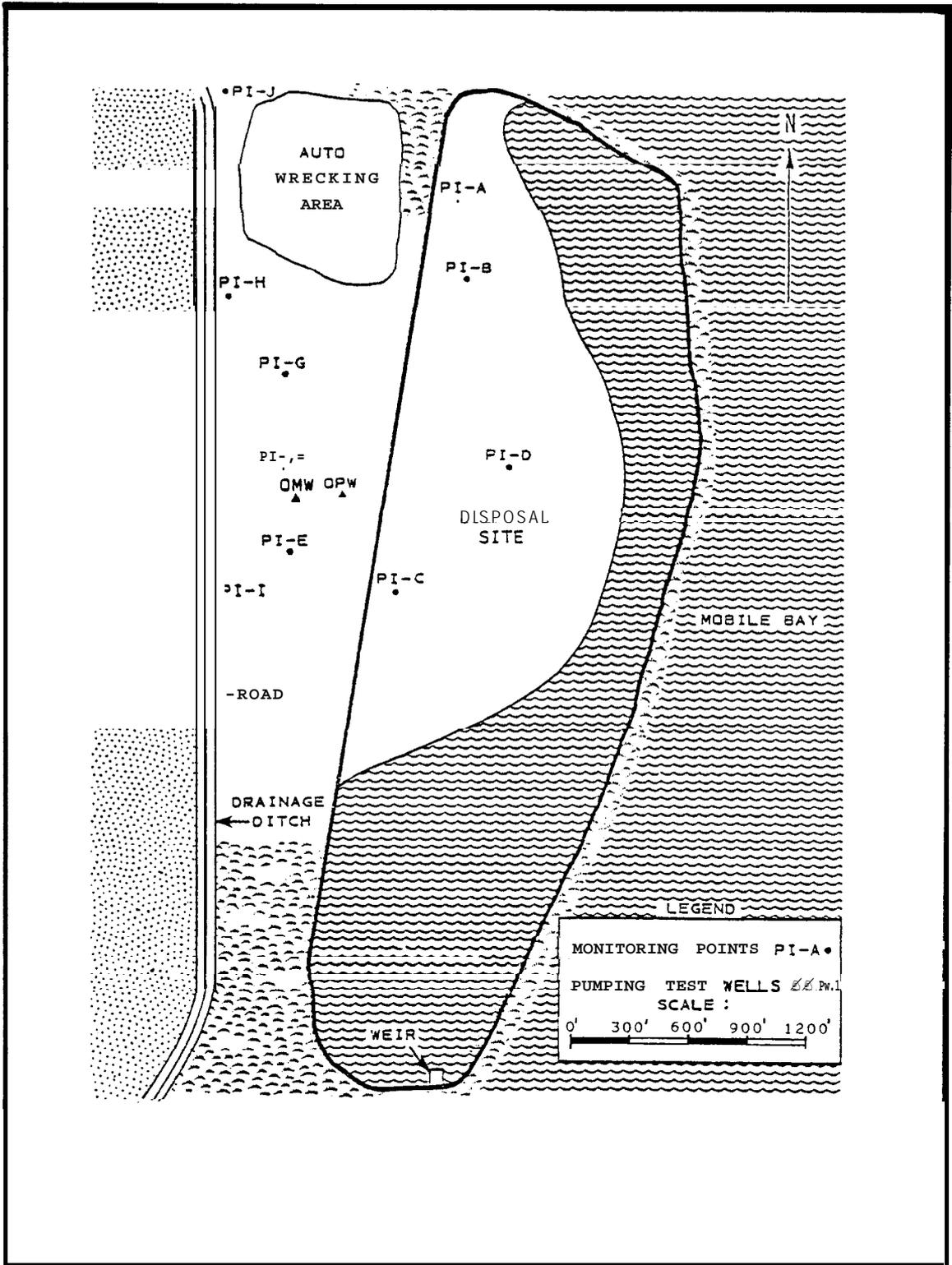


Figure 50. Pinto Island site

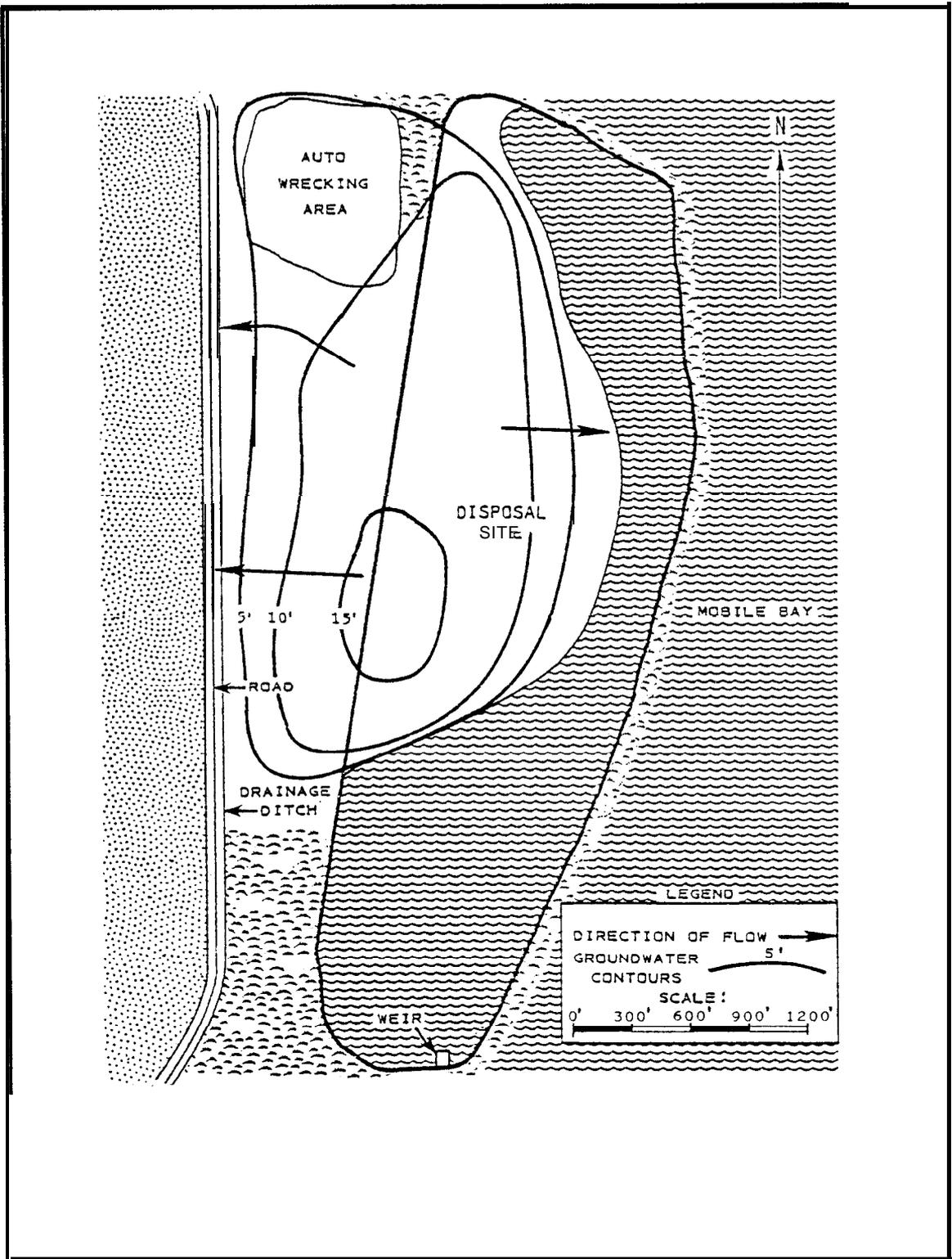


Figure 51. Water level contours on January 17, 1977, Pinto Island site

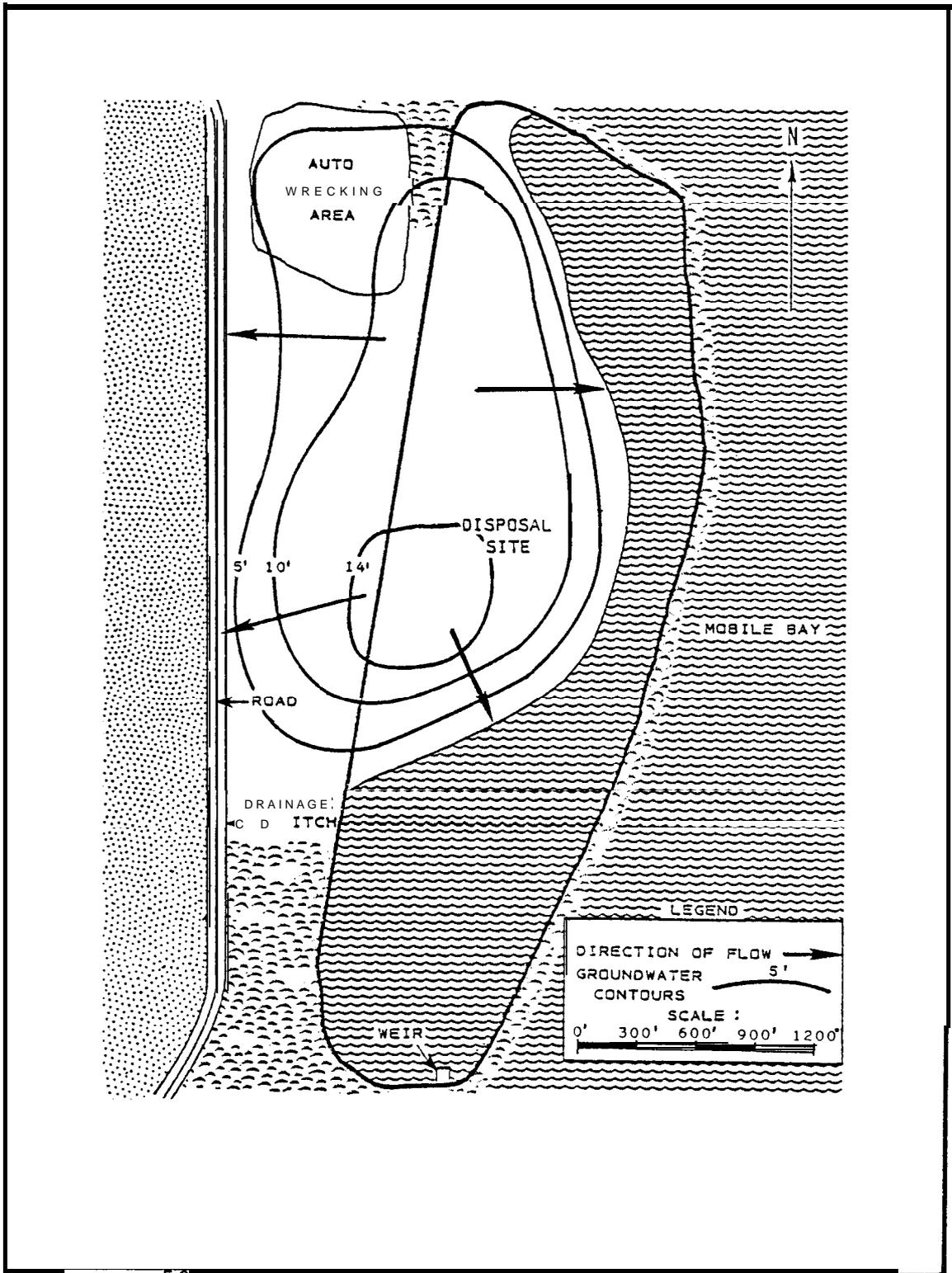


Figure 52. Water level contours on March 26, 1977, Pinto Island site

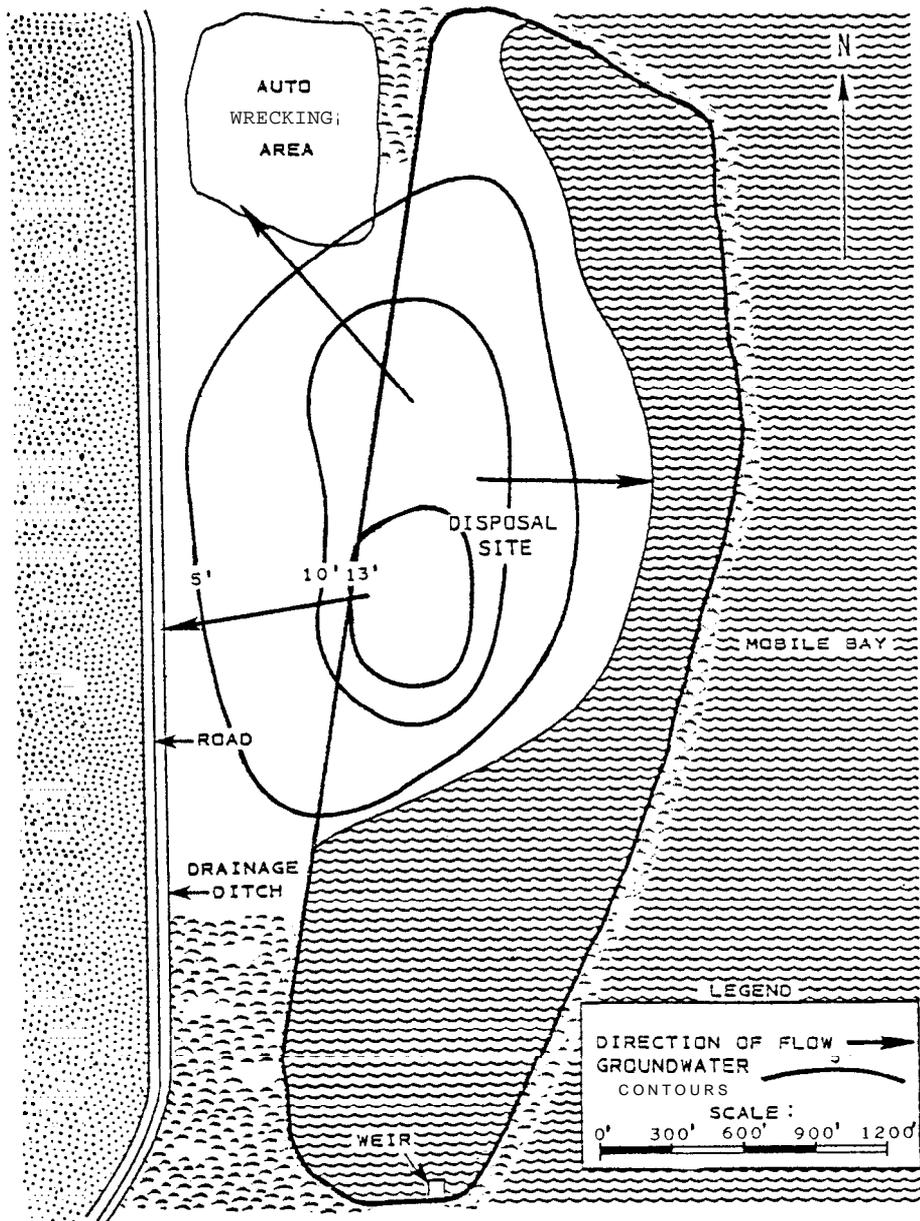


Figure 53. Water level contours on June 7, 1977, Pinto Island site

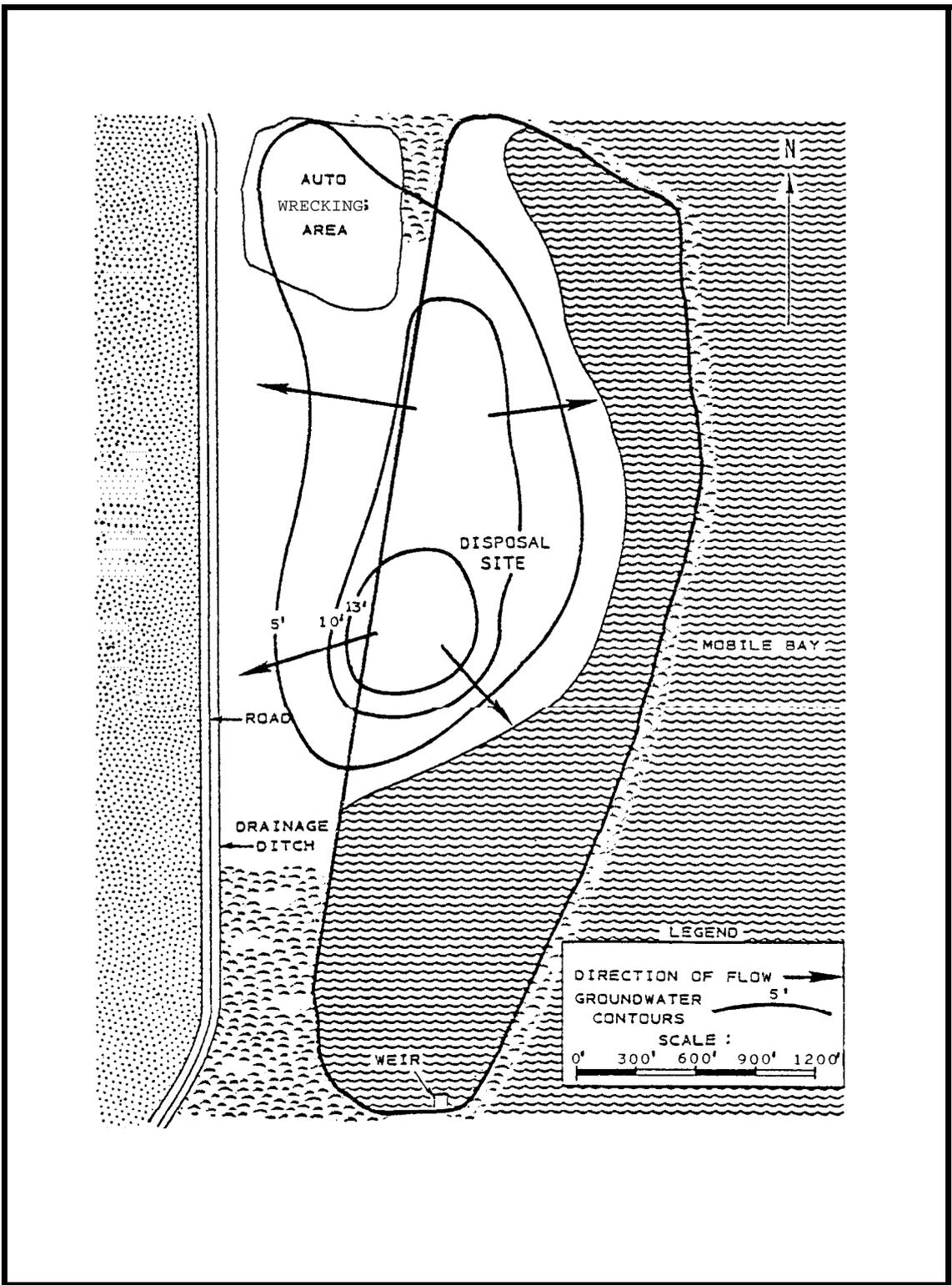


Figure 8.4. Water level contours on August 1, 1977, Pinto Island site

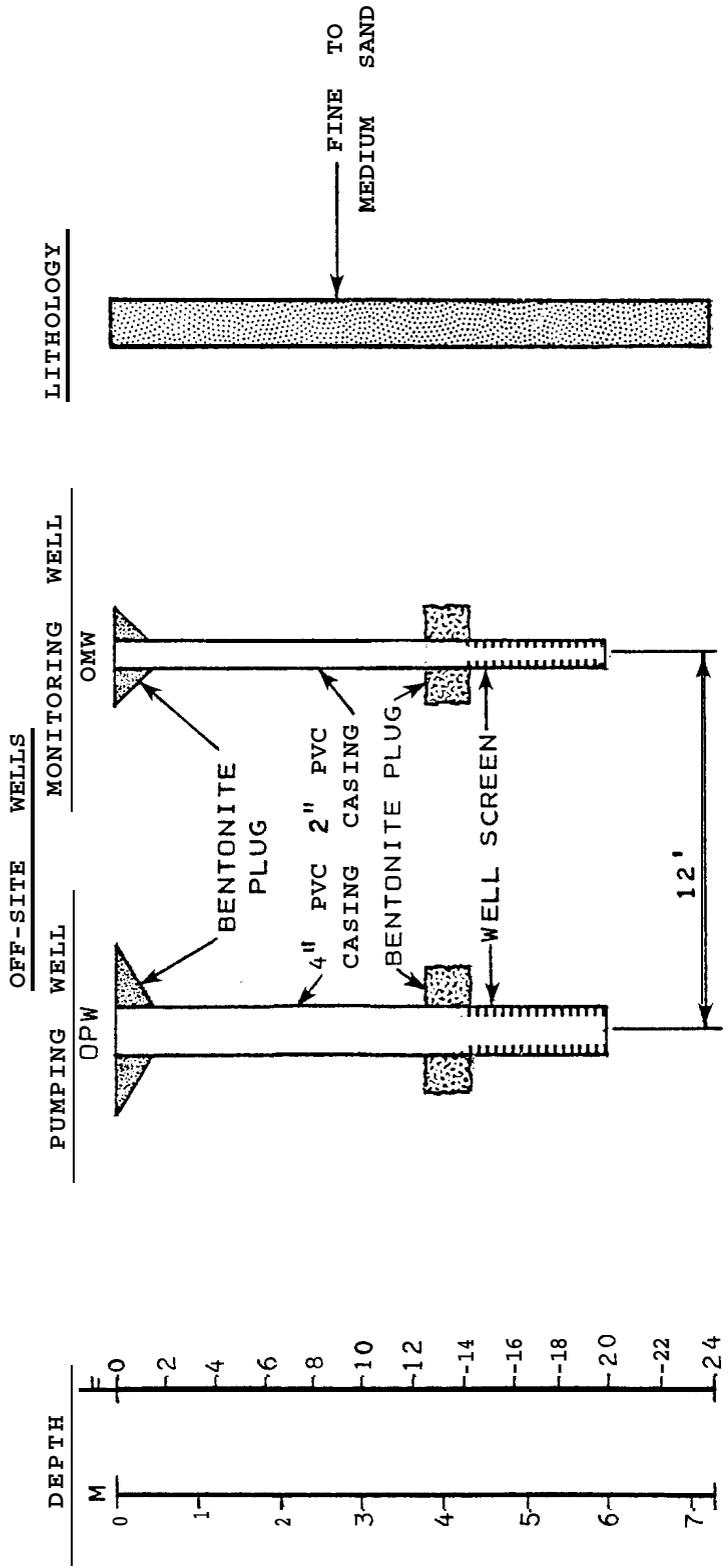
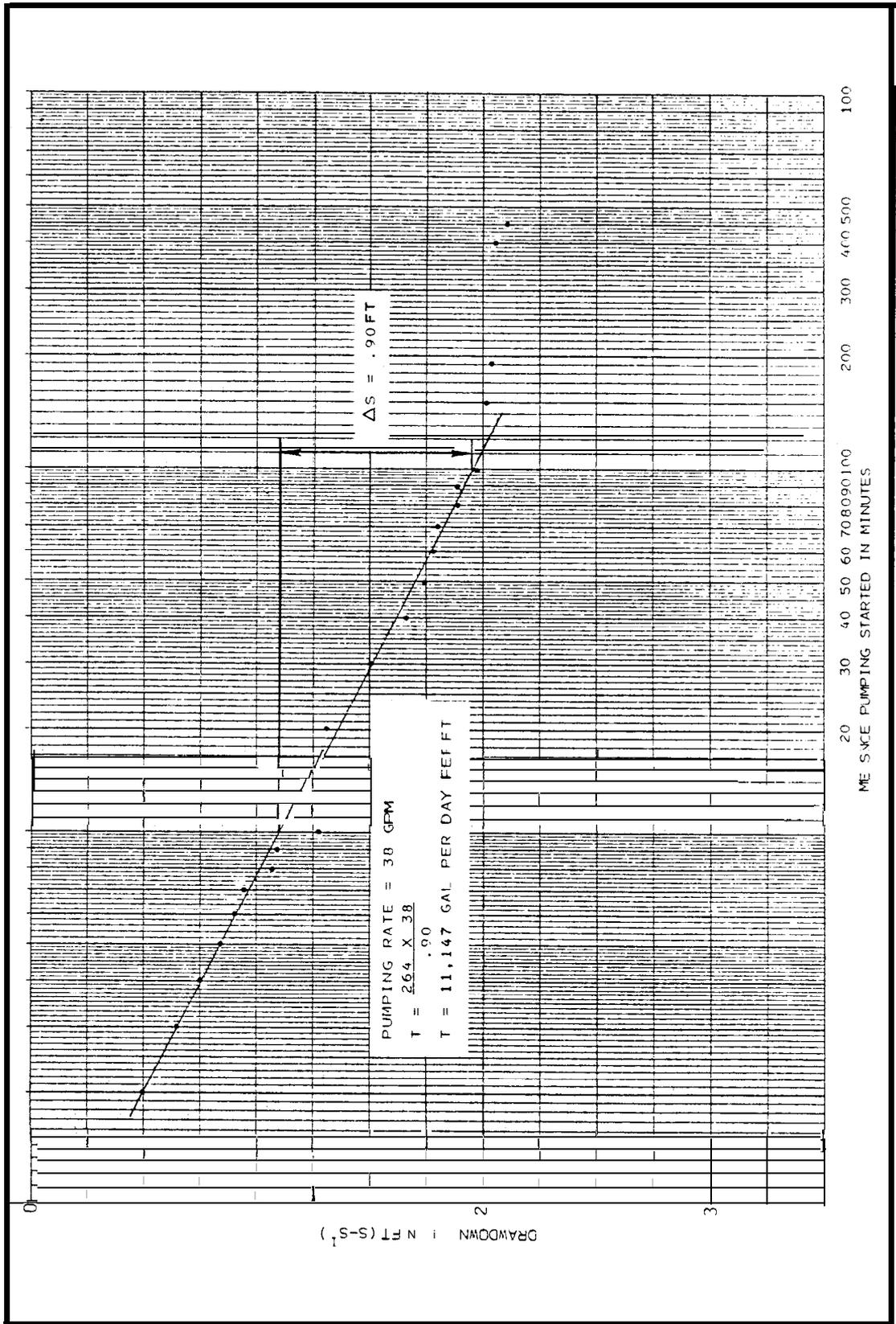
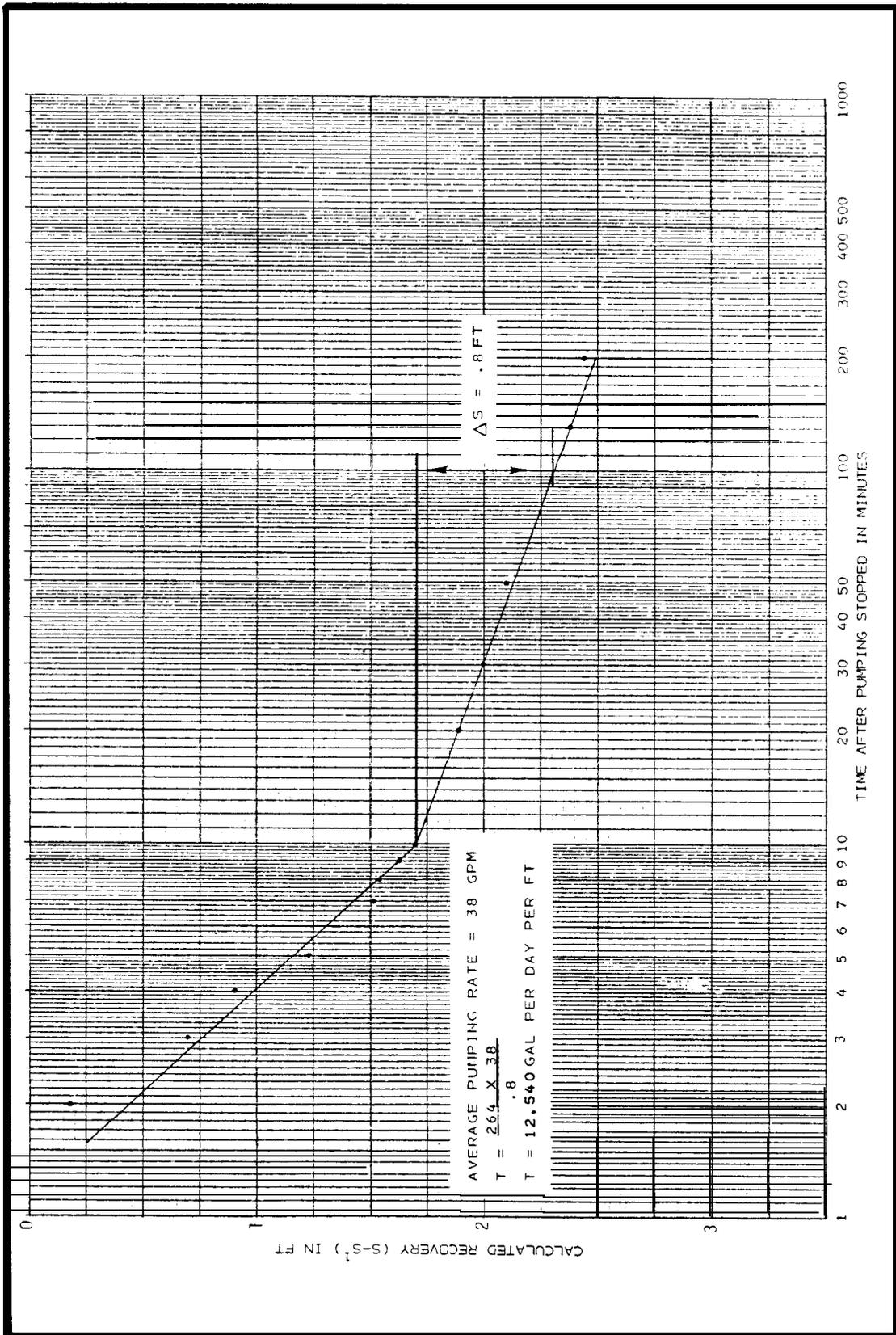


Figure 55. Off-site pumping and monitoring wells at Pinto Island site



Drawdown curve for well OPW



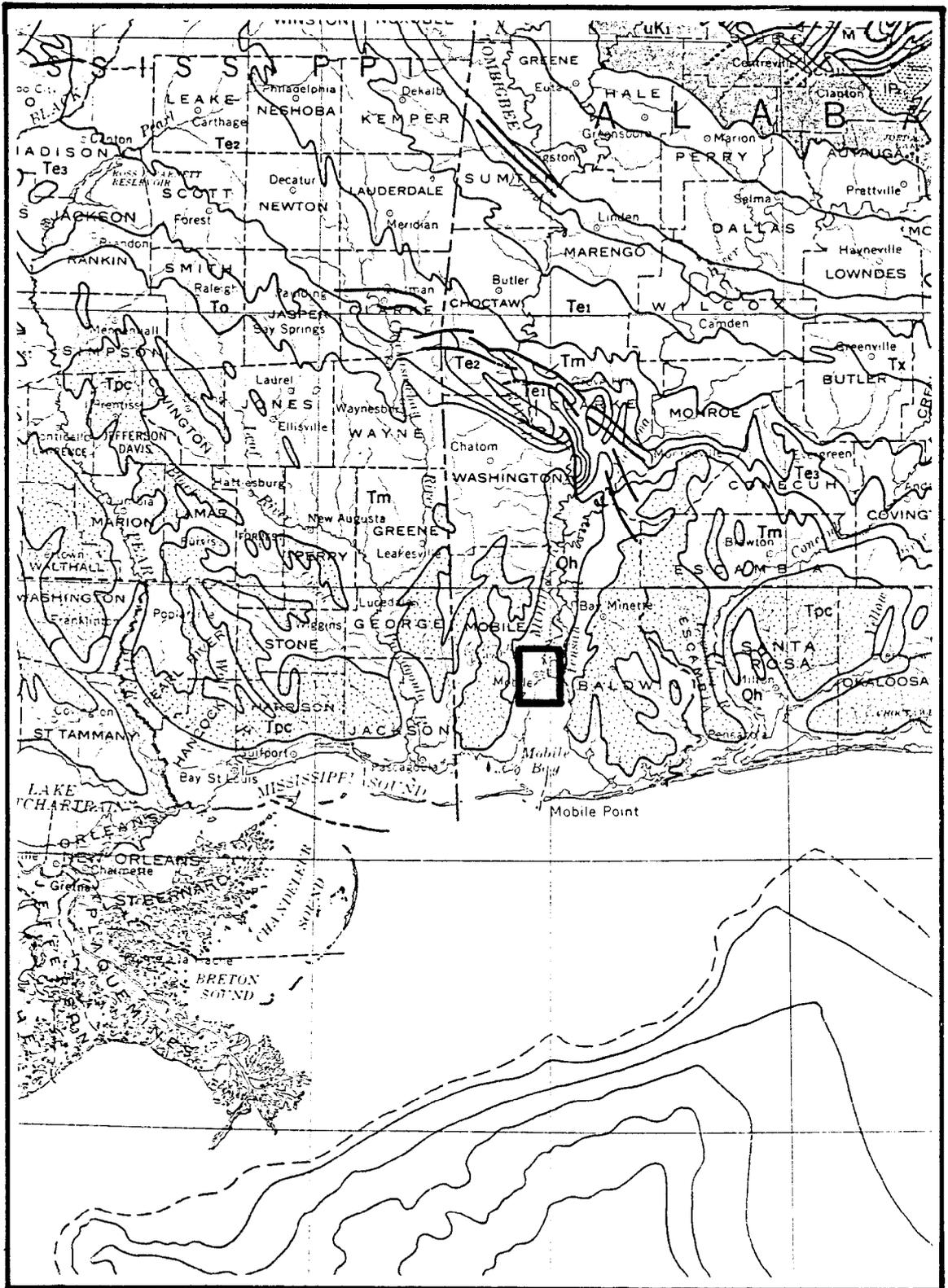


Figure 58. Geologic map of Mobile area

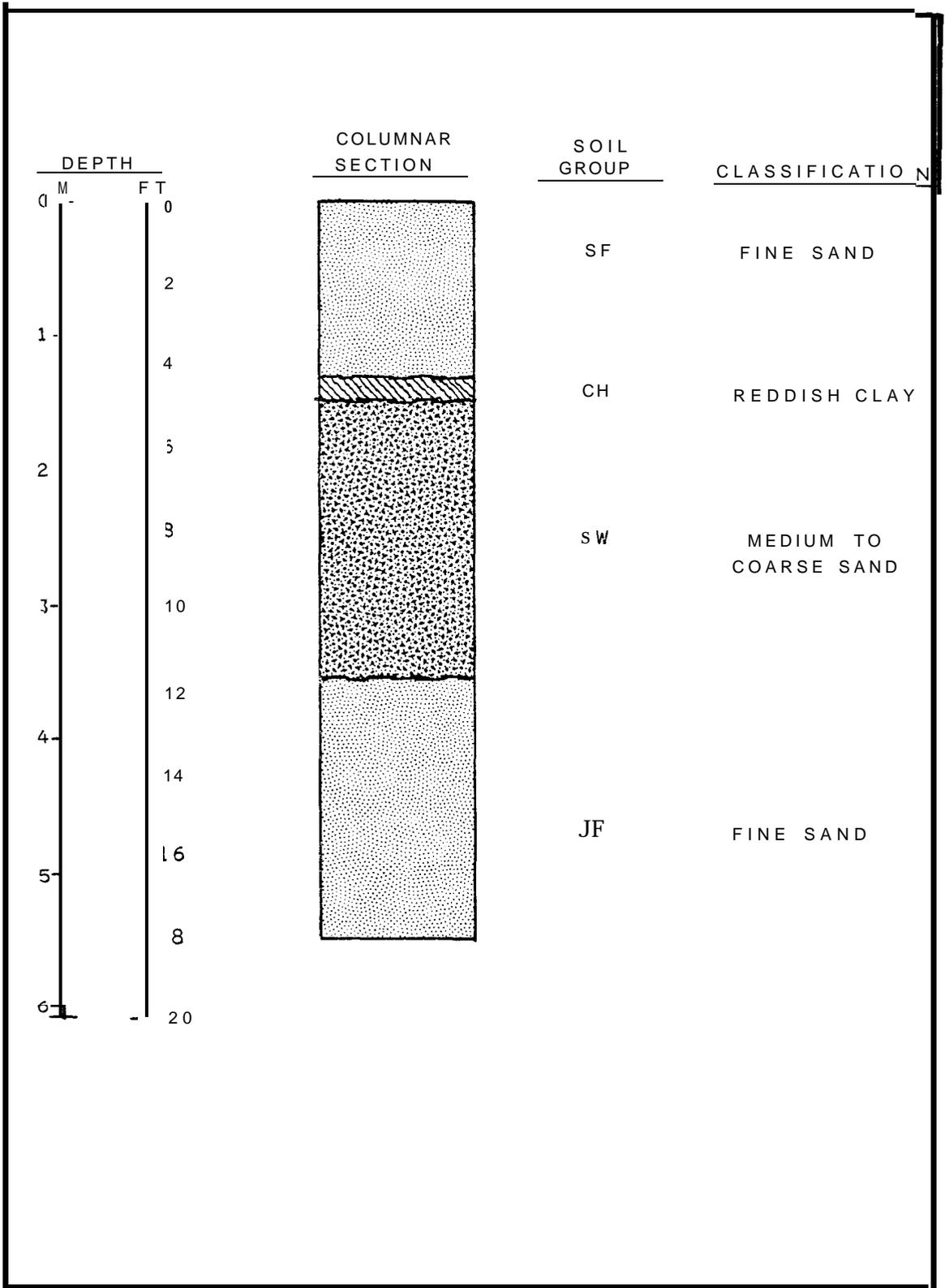


Figure 59. Generalized soil profile, Pinto Island site

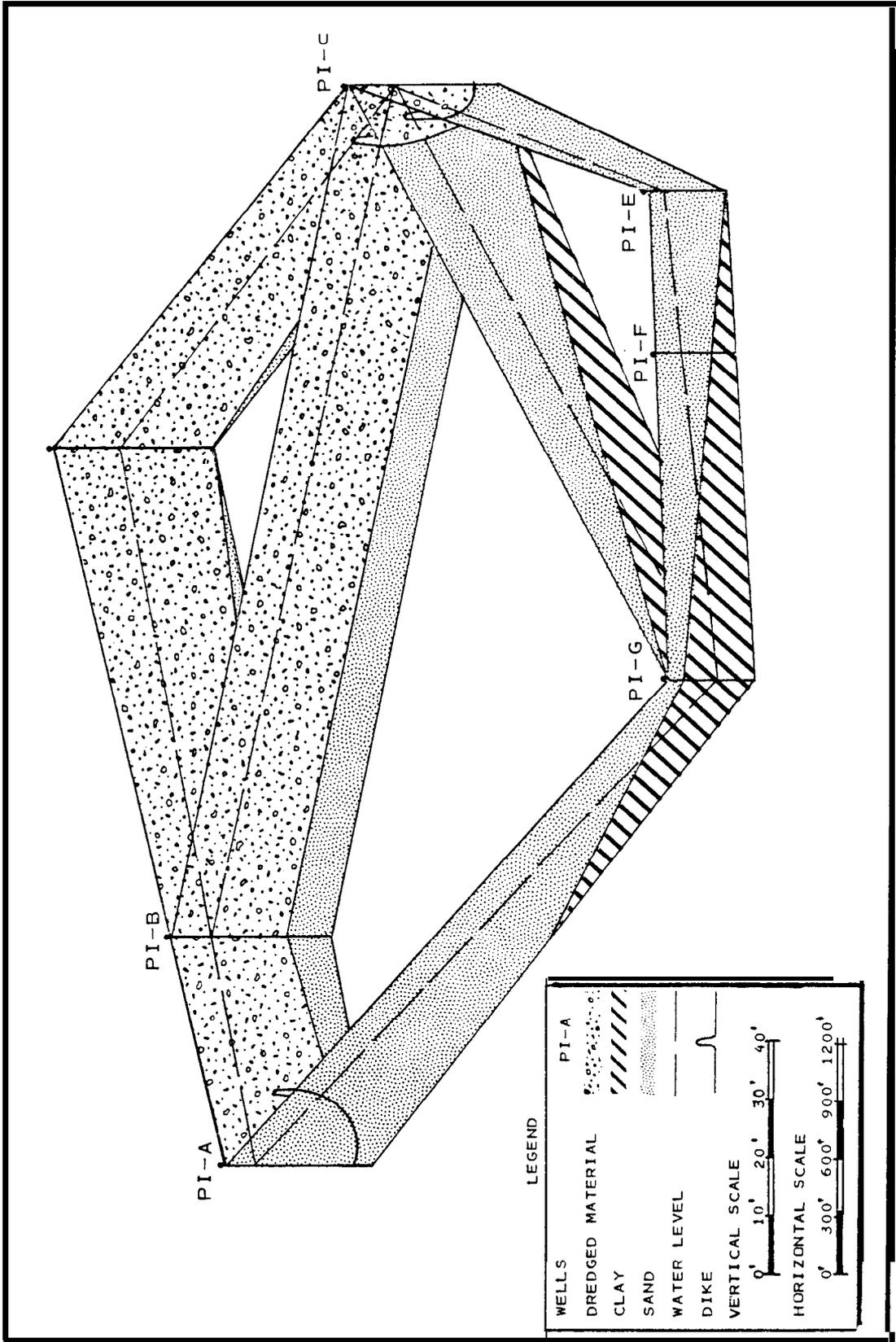


Figure 60. Fence diagram for Pinto Island site

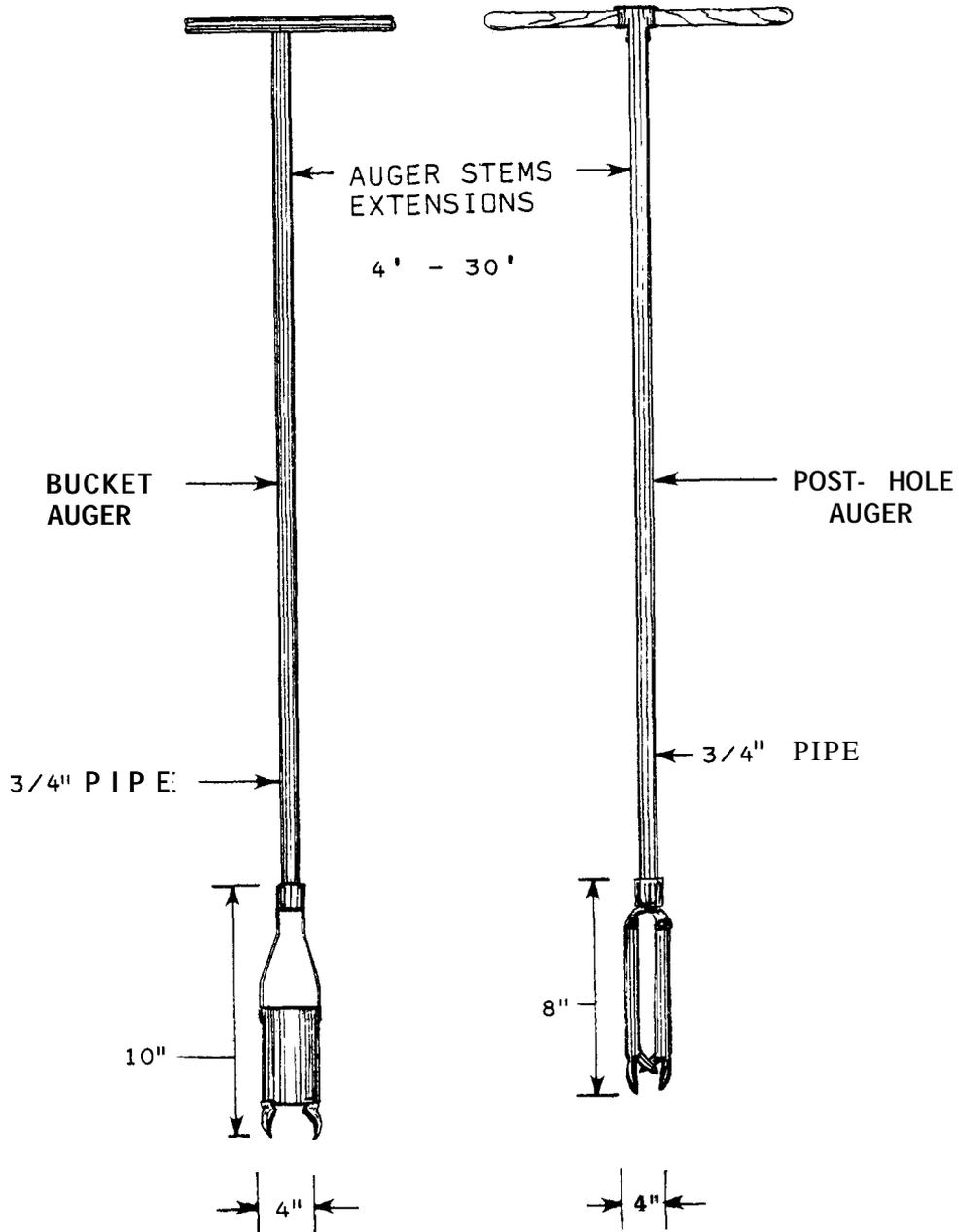


Figure 61. Bucket auger and post-hole auger

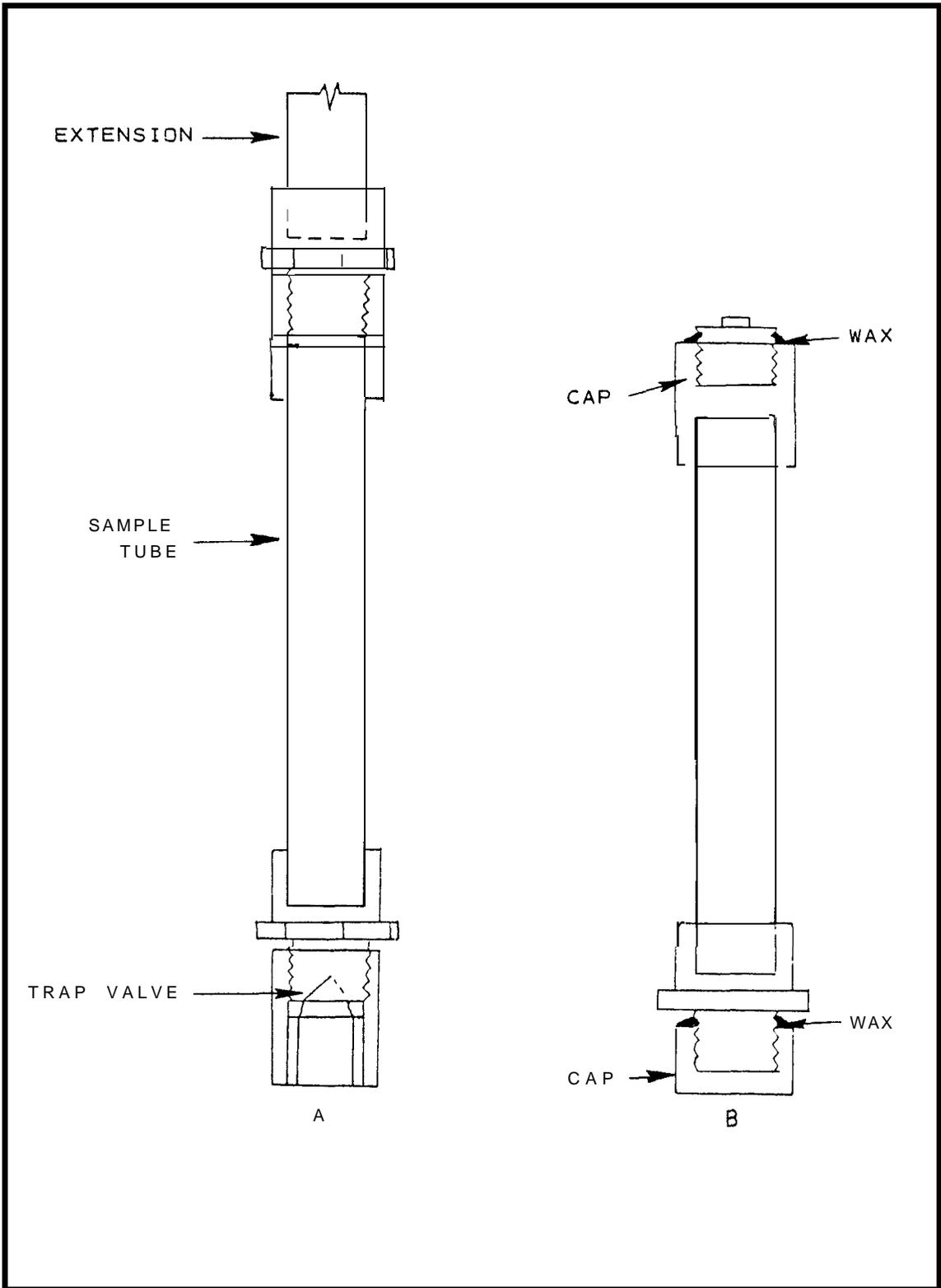


Figure62 . Sampler and sample tube

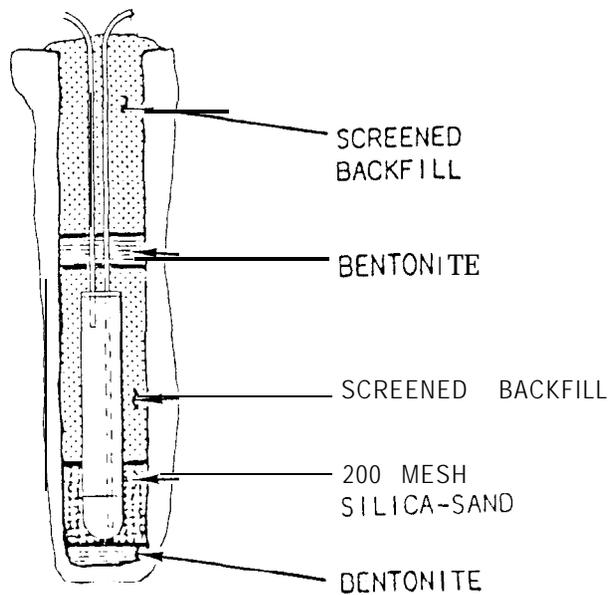
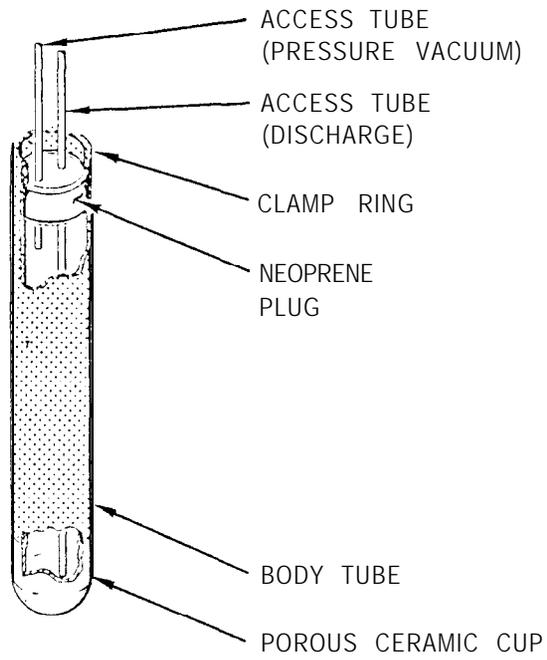


Figure 63. Pressure-vacuum soil lysimeter

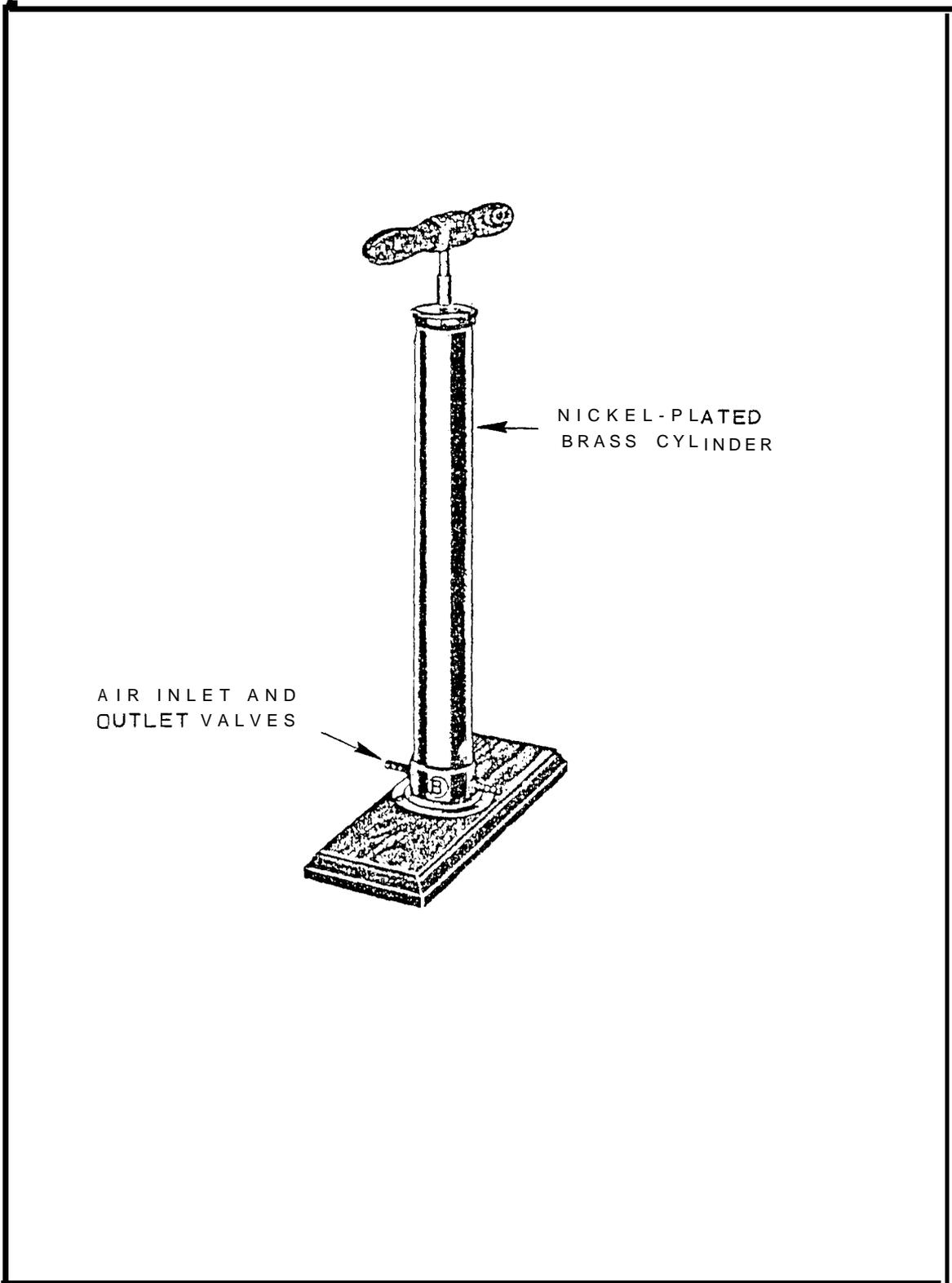


Figure64 . Two-way hand pump

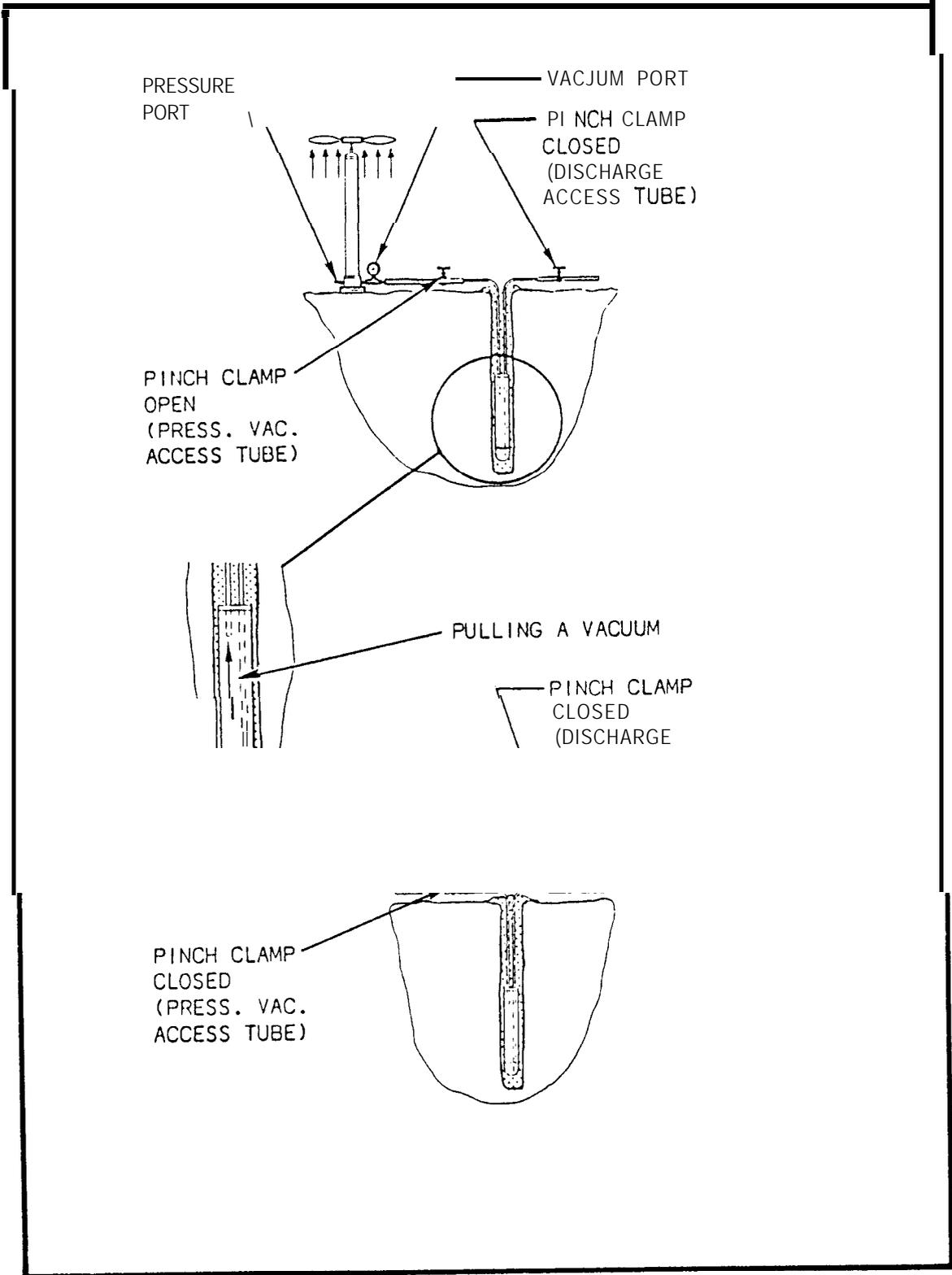


Figure65 . Application of vacuum within pressure-vacuum lysimeter

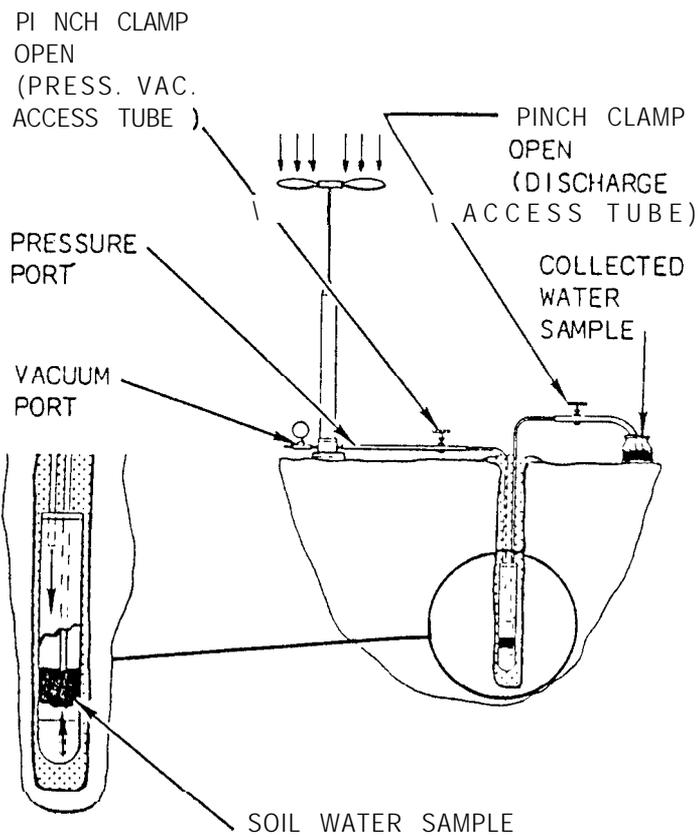


Figure 66. Collection of interstitial water from pressure-vacuum lysimeter

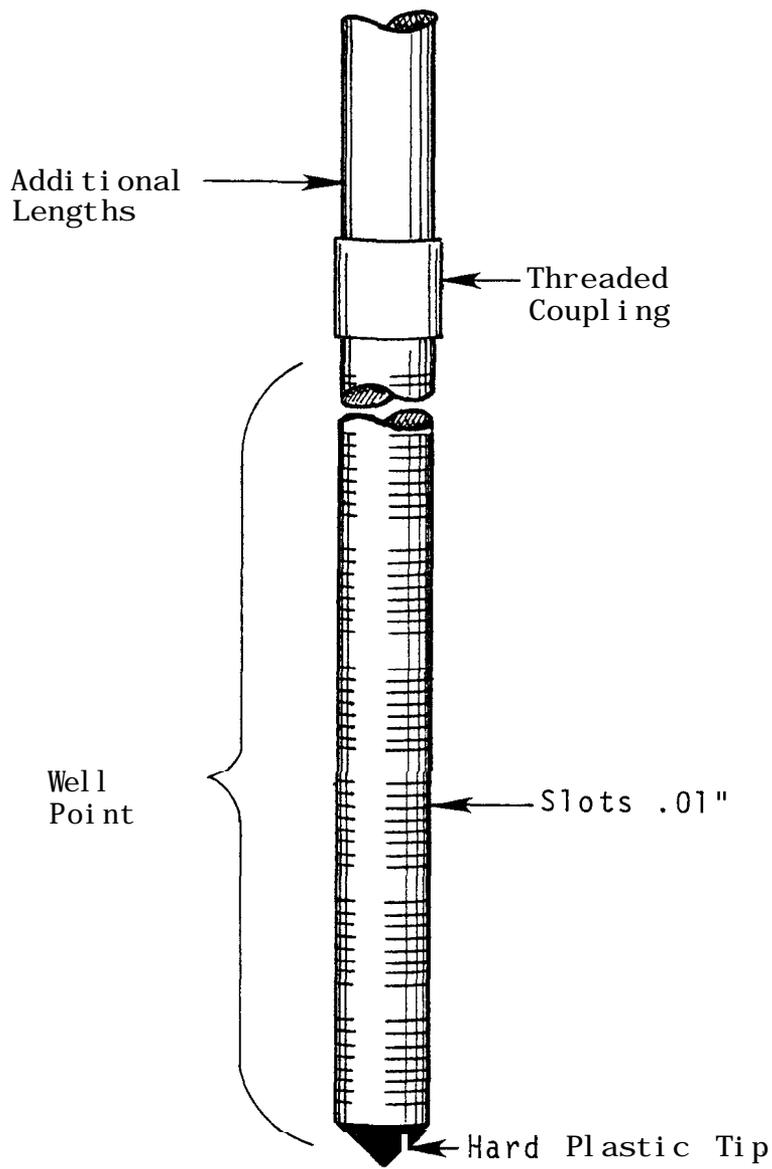


Figure 67. Plastic well point

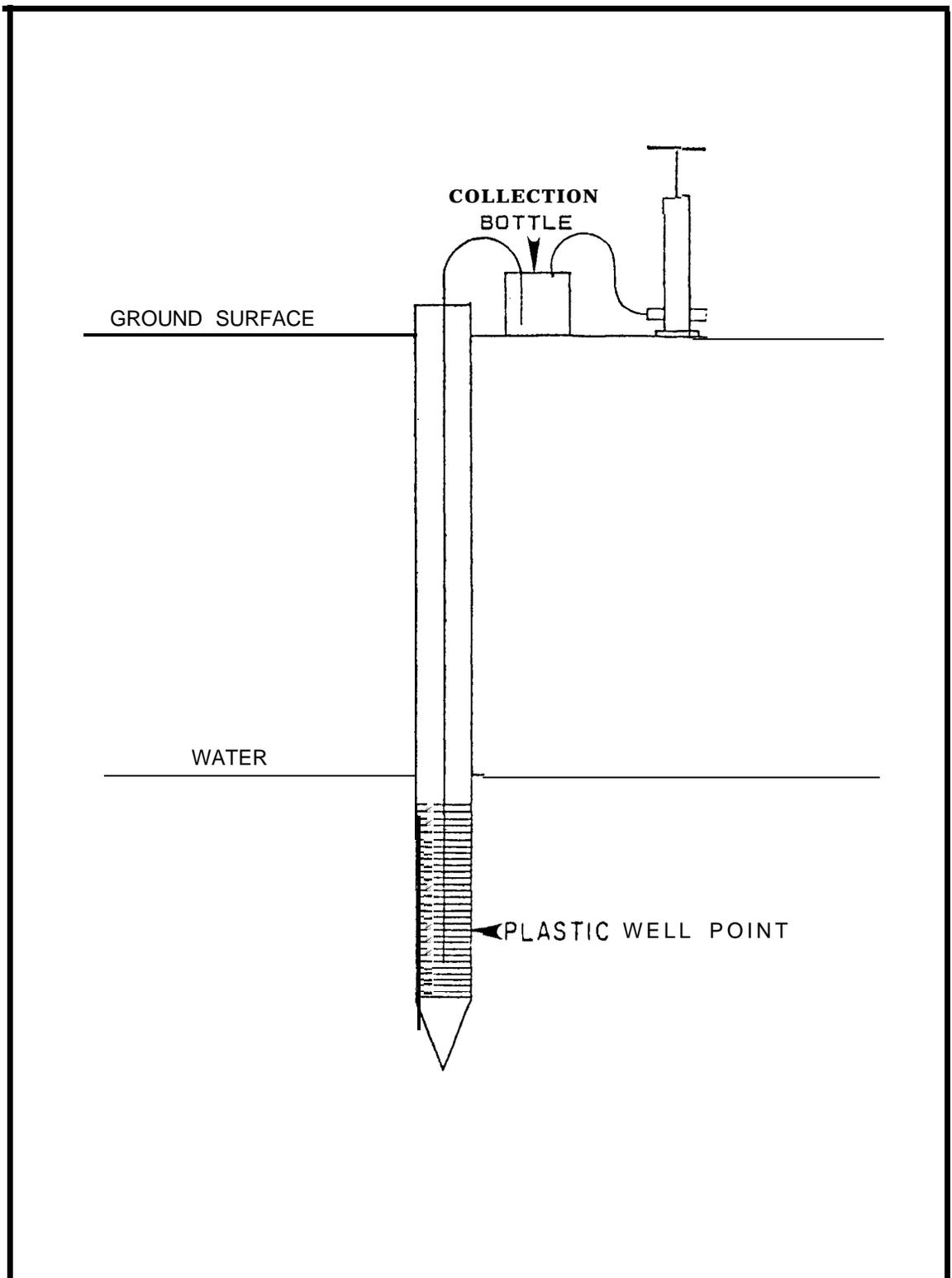
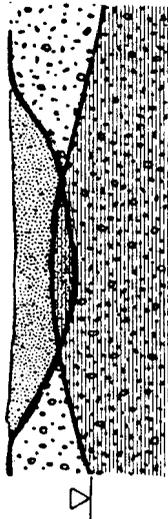
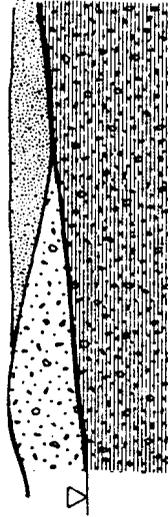


Figure 68. Procedure for collecting water from groundwater wells



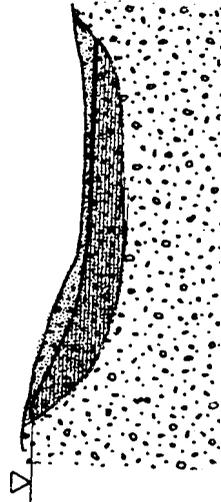
SAYREVILLE SITE

GROUNDWATER IS MOUNDED UNDER THE SITE; ESSENTIALLY A RADIAL FLOW FROM THE SITE



GRAND HAVEN SITE

GROUNDWATER INUNDATES PART OF THE FILL; LEVEL IS SEASONALLY DEPENDENT; FLOW IS ACROSS SITE, TOWARD RIVER AND LOW MARSH AREAS TO NW.



HOUSTON SITE

LOCAL GROUNDWATER SYSTEM ENCAPSULATED WITHIN THE FILL AND ISOLATED BY IMPERVIOUS CLAY SUBSTRATUM.



PINTO ISLAND SITE

GROUNDWATER FLOWS THROUGH FILL, STRONGLY INFLUENCED BY TIDAL CYCLES; SALINE WATER INTRUSION PROMOTES SHALLOW WATER TABLE FOR FRESH WATER.

LEGEND

- DREDGED MATERIAL 
- INDIGENOUS SOILS 
- GROUNDWATER LEVEL 
- ZONE OF SATURATION 

Figure 69. Hydrologic models for four case study sites

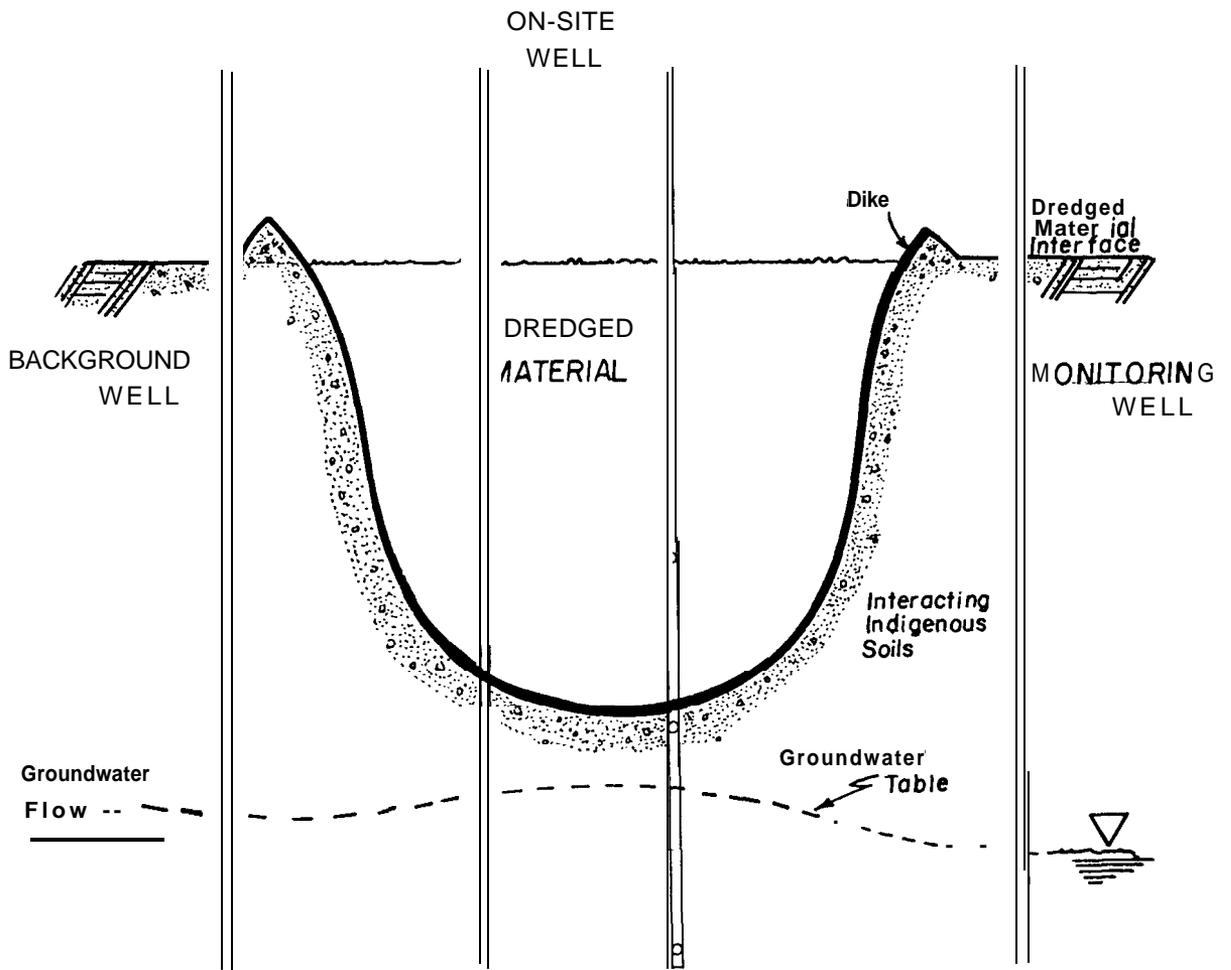


Figure 70. General position of Samplers

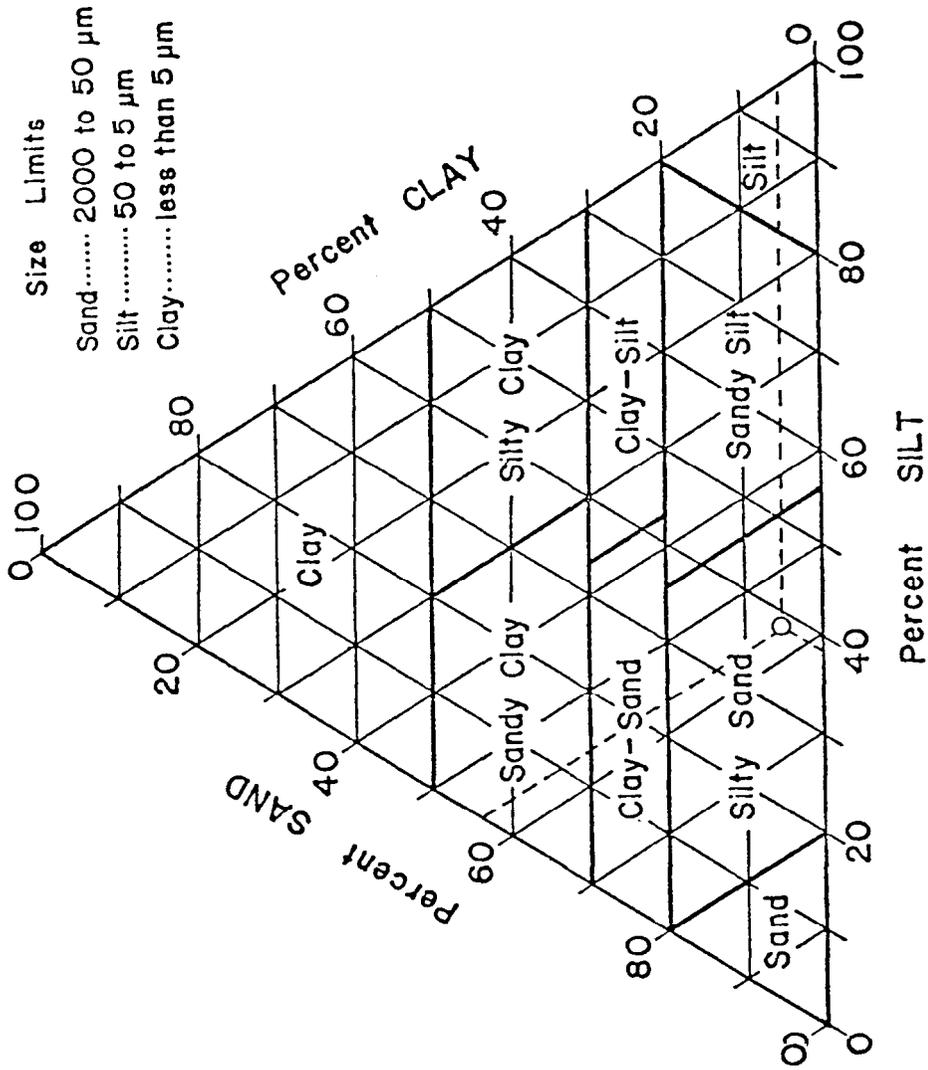


Figure 7I • Triangular classification chart (Lower Mississippi Valley Division, Corps of Engineers, U.S. Army)

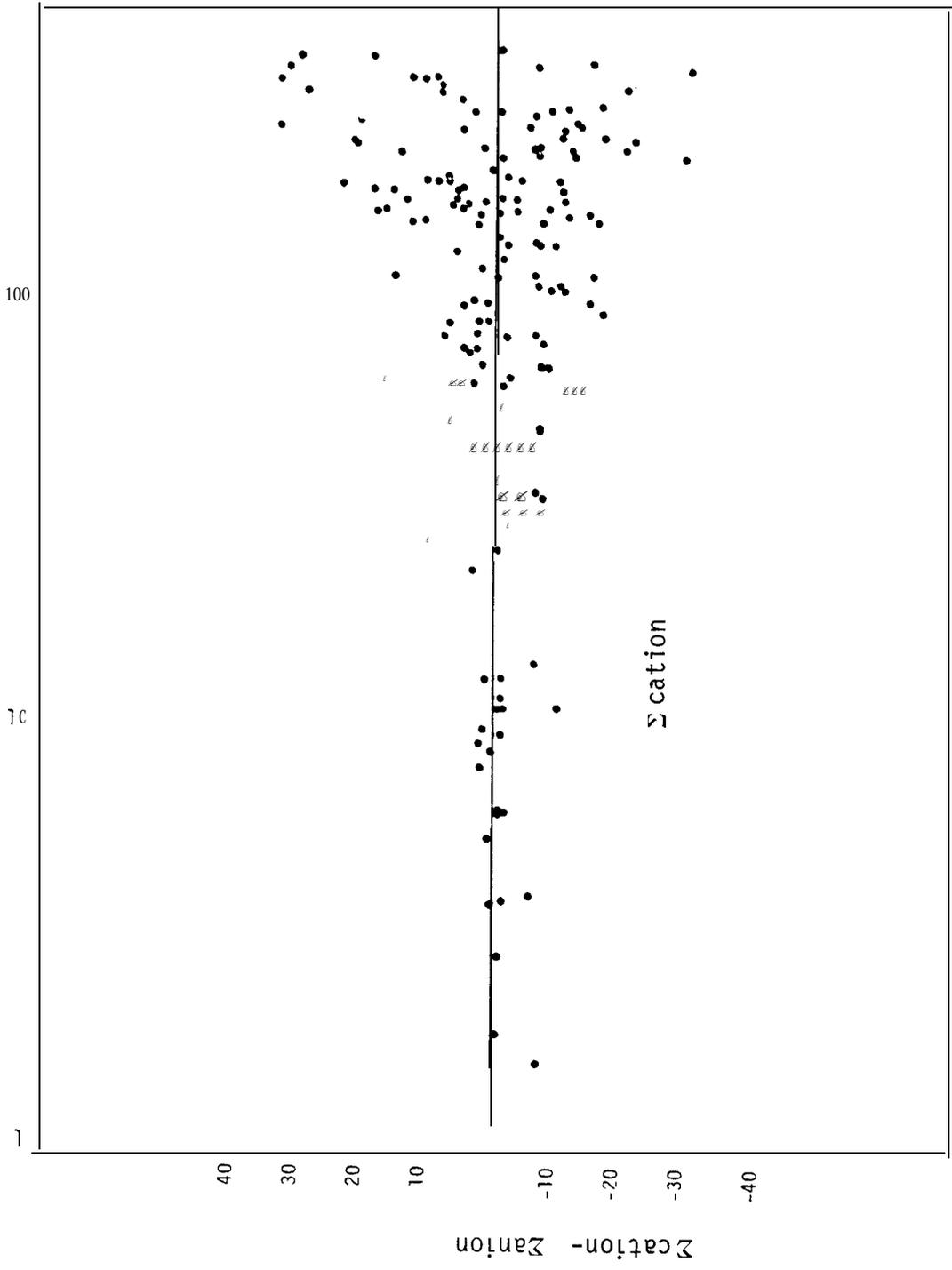


Figure 72. Ionic Balance

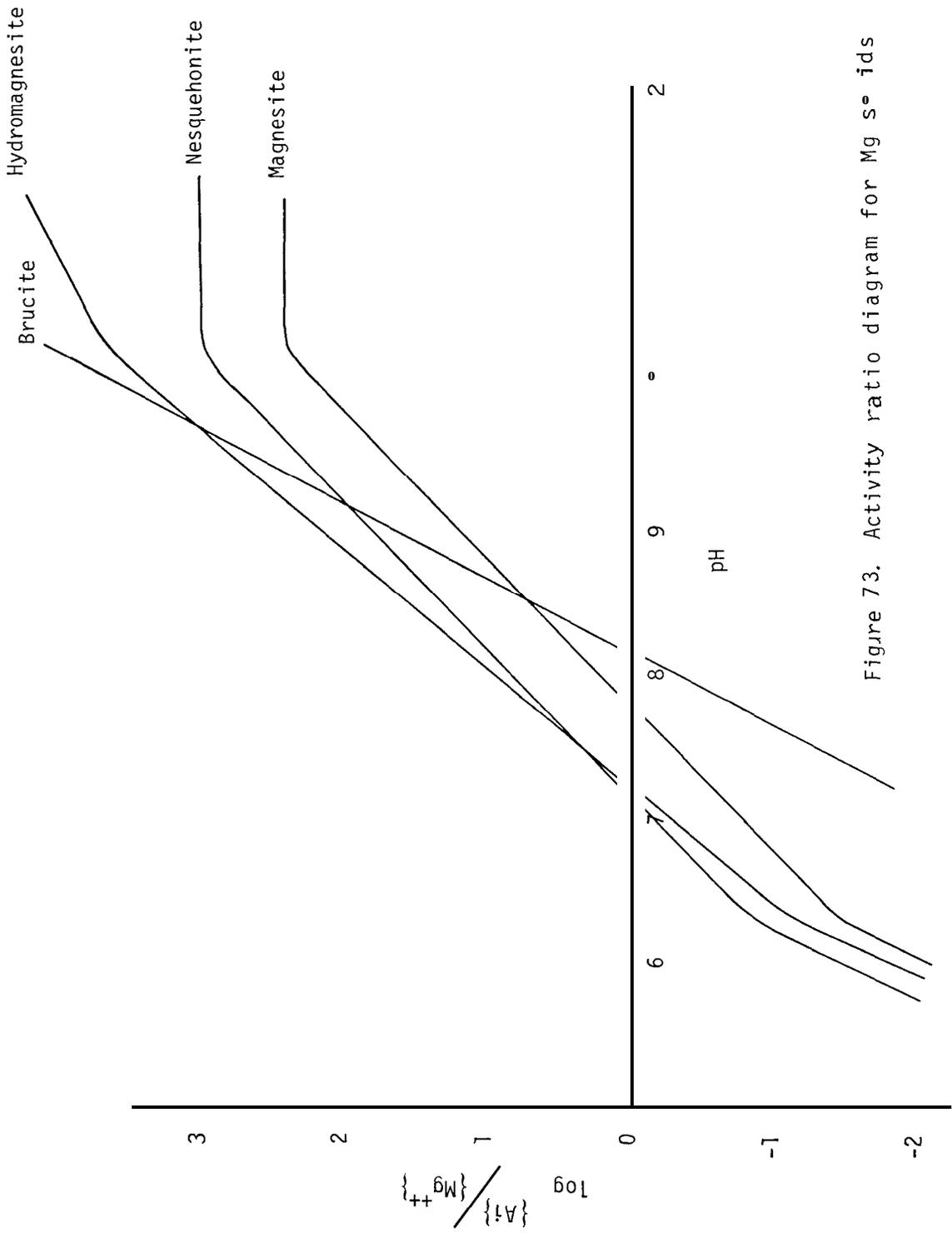


Figure 73. Activity ratio diagram for Mg species

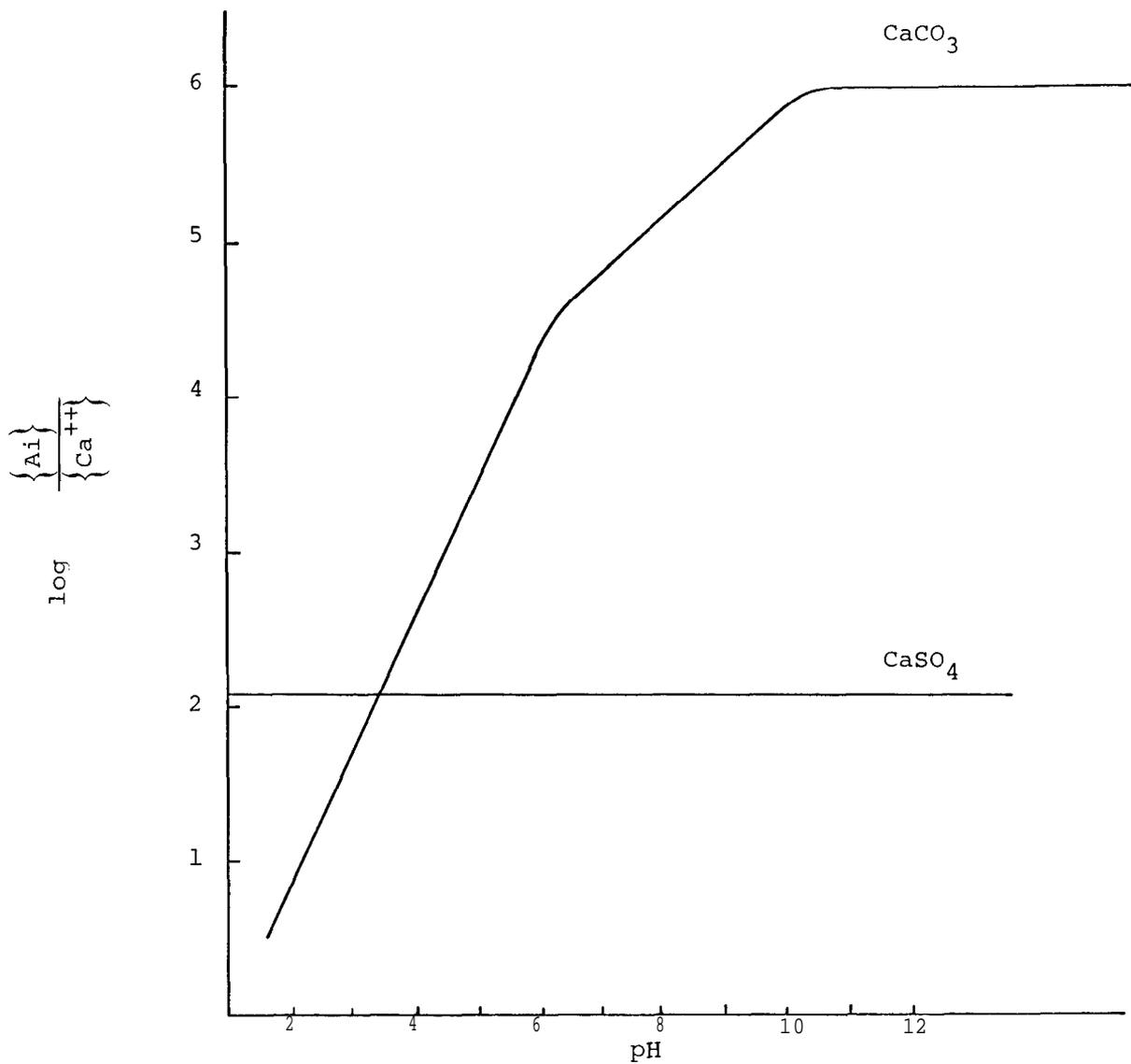


Figure 74. Activity Ratio diagram for calcium solids

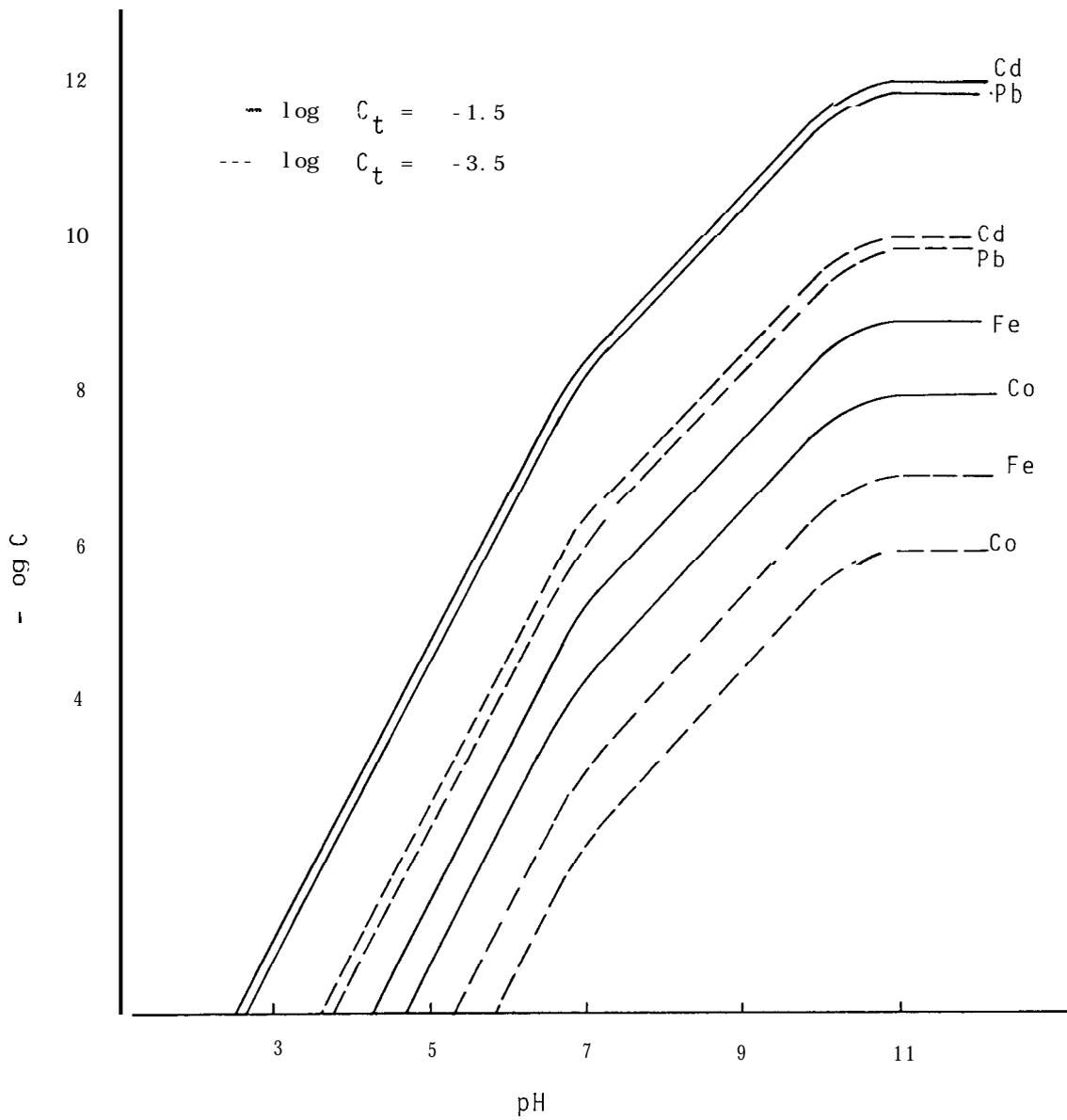


Figure 75. Solubility of Cd, Cu, Fe, Pb carbonates

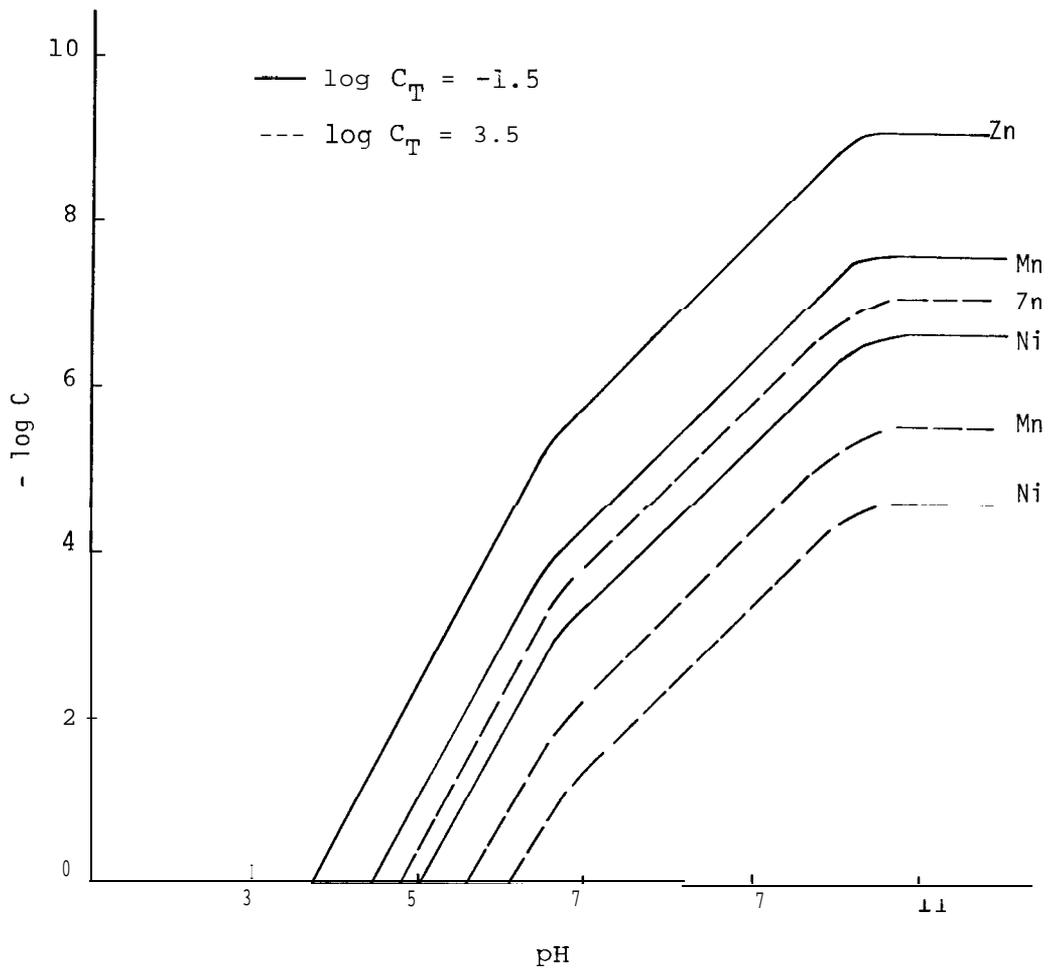


Figure 76. Solubility of Mn, Ni, and Zn carbonates

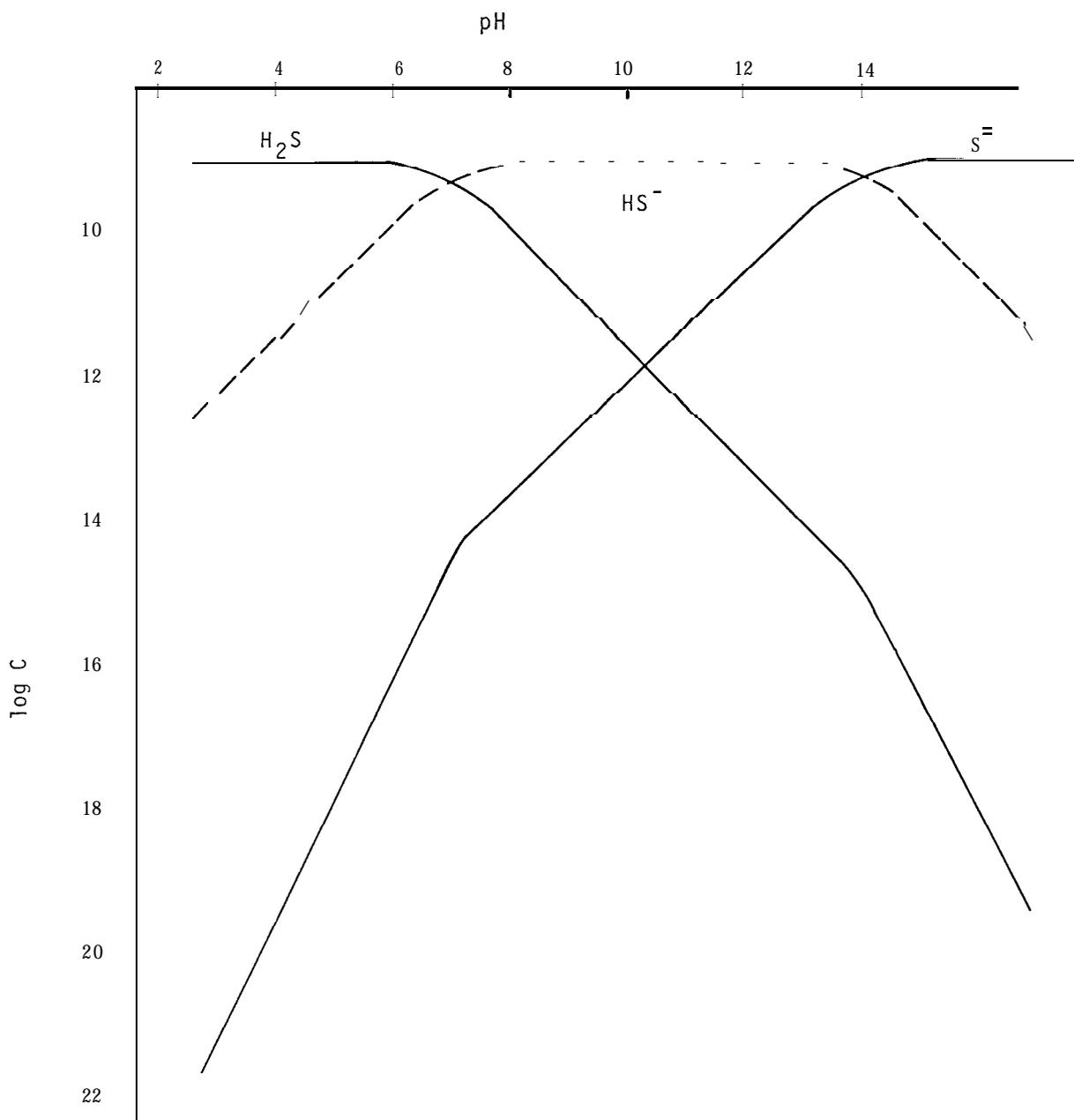


Figure 77. Distribution of sulfide species

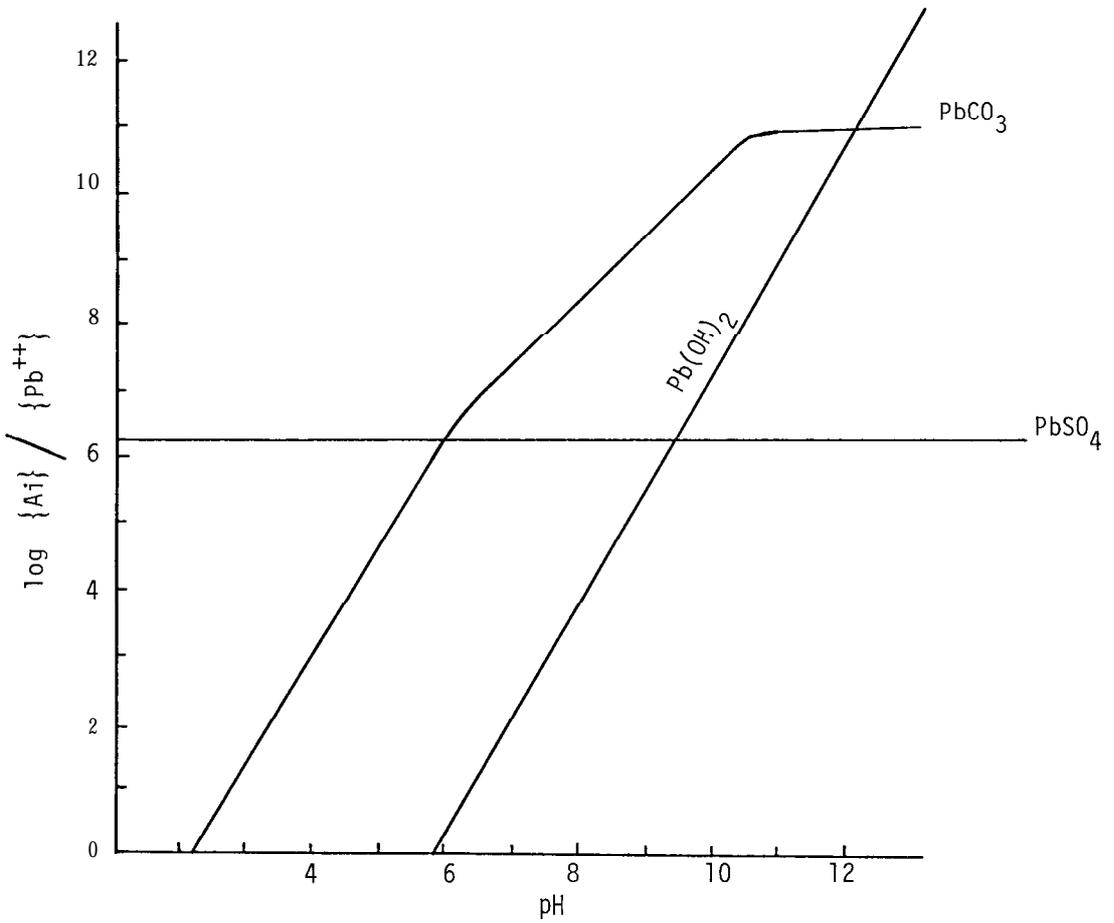


Figure 78. Activity ratio diagram for lead

APPENDIX A: CLIMATOLOGICAL DATA, GRAND HAVEN,
MICHIGAN, CASE STUDY SITE

MUSKEGON COUNTY AIRPORT CLIMATOLOGICAL DATA

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	
Sept. 1976																															
Temp.																															
Max.	68	69	77	72	71	74	78	82	73	67	75	77	78	75	62	66	75	73	74	62	60	55	56	63	66	57	65	58	64	68	
Min.	48	41	54	59	51	44	61	62	51	47	58	55	54	59	51	53	57	49	48	44	43	31	34	30	35	46	43	30	54	42	
Prec.	.18								.57								.06			.08				.19							
Oct. 1976																															
Temp.																															
Max.	73	78	80	77	66	51	55	52	55	59	64	68	61	61	61	47	45	45	40	45	43	43	49	45	48	47	40	47	51	56	
Min.	40	47	48	54	45	44	39	36	40	38	36	53	45	31	46	36	30	23	33	33	36	37	29	38	31	26	22	35	42	40	
Prec.					.24	.41									.07			.02				.03	.03	.03						.42	
Nov. 1976																															
Temp.																															
Max.	49	53	47	37	42	47	38	33	45	40	29	35	38	37	40	45	44	48	47	40	36	31	30	35	51	63	36	22	16	20	
Min.	22	41	33	30	34	37	23	21	29	27	26	26	33	30	18	26	37	36	29	28	27	26	27	26	28	36	22	13	10	11	
Prec.			.09	.05			.01			.12	.18	.13				.04					.04	.02		.07		.22	.32	.05	.12	.05	
Dec. 1976																															
Temp.																															
Max.	22	19	13	26	29	32	26	18	36	39	31	30	28	37	36	33	36	37	41	34	21	29	26	36	36	31	23	22	8	7	
Min.	15	-2	-3	12	20	23	11	10	16	15	13	16	11	28	22	23	29	17	34	15	11	21	12	12	25	14	13	8	3	-11	
Prec.	.12	.12	.04	.10		.30	.01	.07	.03			.02	.02				.02	.06	.03	.01	.10		.02	.07	.10	.15	.13	.16			
Jan. 1977																															
Temp.																															
Max.	24	24	25	26	24	25	18	20	8	15	14	10	24	24	19	8	11	23	23	24	25	22	26	29	29	27	13	15	7	11	
Min.	15	17	17	4	1	8	11	7	-8	7	8	6	5	15	1	-1	5	10	14	10	19	15	16	25	20	3	0	2	4	5	
Prec.	.07	.12	.14			.02	.23	.04	.14	.07	.09	.16	.01	.07	.13	.08						.06			.30	.21	.44	.24	.23		

A2

MUSKEGON COUNTY AIRPORT CLIMATOLOGICAL DATA (Continued)

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	
July 1977																																
Temp.																																
Max.	72	77	78	84	85	84	79	80	81	84	82	82	80	92	88	84	84	77	89	87	84	83	81	74	77	75	77	53	75	81		
Min.	54	53	63	67	72	71	68	62	62	59	64	69	57	56	73	70	69	69	72	76	66	56	61	62	60	50	46	67	65	62		
Prec.			.43	.05		.12	.01								.09	.16	.89				.17			.10						.38		
Aug. 1977																																
Temp.																																
Max.	75	75	78	82	82	75	77	77	77	78	70	74	79	72	78	77	71	58	71	73	68	74	70	70	74	80	88	86	75	76	84	
Min.	62	60	58	64	67	67	68	68	66	65	62	48	59	55	49	63	49	47	46	44	55	46	53	46	43	55	74	66	56	53	61	
Prec.		.06		.27	.30			.11	.45			.36			.08					.08		.11			.01		.33	.31				

A4

APPENDIX B: WELL LOGS, GRAND HAVEN,
MICHIGAN, CASE STUDY SITE



Job: DREDGED MATERIAL STUDY/GRAND HAVEN, MICH.

Investigator: R. Morrison/K. Yu
 Date: 12/4/76
 Rig: 4" Land bucket auger
 Existing Elevation: 585.2
 Well No: MA (onsite)

Depth	Sample Location	Material	Description	Remarks
1		Dredged material	Fine sands	Aerobic
2		"	" "	"
3		" "	" "	Anaerobic
4		" "	Water encountered	"
5		" "	Dredged material/ soil interface	"
6		" "	Sand	"
7		" "	"	"
8		" "	"	"
9		" "	Bottom of hole	"
10				
11				
12				
13				
14				
15				
16				
17				



JOB: DREDGED MATERIAL STUDY/GRAND HAVEN, MICH.

Investigator: R. Morrison/K. Yu
 Date: 12/1/76
 Rig: 4" Hand bucket auger
 Existing Elevation: 585.0
 Well No: MB (onsite)

Depth	Sample Location	Material	Description	Remarks
1		Dredged material	Sand and silts	Aerobic
2		" "	" "	"
3		" "	" "	Anaerobic
4		" "	" "	
5		" "	Water encountered	
6		" "	Dredged material/ soil interface	
7		" "	Sand	
8		" "	Bottom of hole	
9				
10				
11				
12				
13				
14				
15				
16				
17				



Job: DREDGED MATERIAL STUDY/GRAND HAVEN, MICH.

Investigator: R. Morrison/K. Yu
 Date: 12/4/76
 Rig: 4" Hand bucket auger
 Existing Elevation: 584.0
 Well No: MC

Depth	Sample Location	Material	Description	Remarks
1		Sand	Fine sands	Brochipod shells present
2		"	" "	" "
3		"	" "	" "
4		"	Water encountered	" "
5		"		" "
6		"		" "
7		"	Bottom of hole	" "
8				
9				
10				
11				
12				
13				
14				
15				
16				
17				



JOB: DREDGED MATERIAL STUDY/GRAND HAVEN, MICH.

Investigator: R. Morrison/K. Yu
 Date: 12/4/76
 Rig: 4" Hand bucket auger
 Existing Elevation: 585.3
 Well No: M0 (offsite)

Depth	Sample Location	Material	Description	Remarks
1		Sand	Sand	
2			"	
3			Water encountered	
4			Sand clay	
5			" "	
6			Bottom of hole	
7				
8				
9				
10				
11				
12				
13				
14				
15				
16				
17				



Job: DREDGED MATERIAL STUDY/GRAND HAVEN, MICH.

Investigator: R. Morrison/K. Yu
 Date: 12/5/76
 Rig: 4" Hand bucket auger
 Existing Elevation: 586.2
 Well No: ME (offsite)

Depth	Sample Location	Material	Description	Remarks
1		Sands	Fine to medium sands	
2		"	" " "	Gastropod shells
3		"	Water encountered	
4		"	" "	
5		"	" "	
6		"	" "	
7		"	Bottom of hole	
8				
9				
10				
11				
12				
13				
14				
15				
16				
17				



Job: DREDGED DISPOSAL STUDY/GRAND HAVEN, MICH.

Investigator: R. MORRISON/K. YU

Date: 12/5/76

Rig: 4" Hand bucket auger

Existing Elevation: 589.0

Well No: MF (offsite)

Depth	Sample Location	Material	Description	Remarks
1		Sand	Fine sands	
2		"	" "	Shell fragments
3		"	" "	
4		"	Water encountered	
5		"	" "	
6		"	" "	
7		"	Bottom of hole	
8				
9				
10				
11				
12				
13				
14				
15				
16				
17				



Job: DREDGED MATERIAL STUDY/GRAND HAVEN, MICH

Investigator: R. Morrison/K. Yu

Date: 12/5/76

Rig: 4" hand bucket auger

Existing Elevation: 589.7

Well No: MG (onsite)

Depth	Sample Location	Material	Description	Remarks
1		Dredged material	Well sorted sand	Aerobic
2		" "	" " "	"
3		" "	Clayey sand	Anaerobic
4		" "	" "	"
5		" "	Dredged material/soil interface	"
6		∇ Sand	Water encountered	"
7		" "	" "	"
8	—		Bottom of hole	"
9				
10				
11				
12				
13				
14				
15				
16				
17				



Job: DREDGED MATERIAL STUDY/HAVEN, MICH.
 Investigator: R. Morrison/K. Yu
 Date: 12/5/76
 Rig: 4" Hand bucket auger
 Existing Elevation: 589.7
 Well No: MH (onsite)

Depth	Sample Location	Material	Description	Remarks
1		Dredged material	Sandy clay	Aerobic
2		"	"	"
3		"	"	Anaerobic
4		"	Water encountered	"
5		Sand	Interface dredged material and soil	"
6		"	Sand	"
7		"	Sand	"
8		"	Bottom of fill	"
9				
10				
11				
12				
13				
14				
15				
16				
17				



Job: DREDGED MATERIAL STUDY/GRAND HAVEN, MICH.

Investigator: R. Morrison/K. Yu
 Date: 12/5/76
 Rig: 4" Hand bucket auger
 Existing Elevation: 585.5
 Well No: MI (Offsite - background well)

Depth	Sample Location	Material	Description	Remarks
1		Sand	Fine to medium sand	
2		"	Fine to medium sand	
3		"	Fine to medium sand	
4		"	Water encountered	
5		"	Some gravels present	
6		"	Some gravels present	
7		"	Some gravels present	
8		"	Bottom of hole	
9				
10				
11				
12				
13				
14				
15				
16				
17				



Job: DREDGED MATERIAL STUDY/GRAND HAVEN, MICH.

Investigator: R. Morrison/K. Yu

Date: 12/5/76

Rig: 4" Hand bucket auger

Existing Elevation: ---

Well No: MJ (offsite - background well)

Depth	Sample Location	Material	Description	Remarks
1		Sand	Fine sands	
2		"	Water encountered	
3		"	Fine sands	
4		"	Fine sands	
5		"	Bottom of hole	
6				
7				
8				
9				
10				
11				
12				
13				
14				
15				
16				
17				



Job: DREDGED MATERIAL STUDY/GRAND HAVEN, MICH.

Investigator: R. Morrison/K. Yu

Date: 12/9/76

Rig: 6" Truck mounted auger

Existing Elevation: _____

Well No: MP (offsite pumping well)

Depth	Sample Location	Material	Description	Remarks
1		Sand	Light brown, fine sands	Easy Drilling
2		"		
3		"		
4		"		
5	<u>▽</u>	"	Water encountered	
6		"		
7		"		
8		"		
9		"		
10		"		
11		"		
12		"		
13		"	Fine to medium grained	Well screen installed 15'-20'
14		Sand	Coarse sands	
15		"	" "	
16		"	" "	
17		"	Coarse + medium grained sands	



JOB: DREDGED MATERIAL STUDY/GRAND HAVEN, MICH.

Investigator: R. Morrison/K. Yu
 Date: 12/4/76
 Rig: 6" Truck-mounted auger
 Existing Elevation:
 Well No: MP (offsite pumping well)

Depth	Sample Location	Material	Description	Remarks
18		Sand	Coarse	More resistance in drilling
19		Clay	Light grey/tight	
20		"	" "	
21		"	" "	
22		"	" "	
23		"	" "	
24		"	" "	
25		"	" "	
26		"	" "	
27		"	" "	
28		"	" "	
29		"	" "	
30		"	" "	
31		"	" "	
32		"	" "	
33		"	" "	
41	—	"	Bottom of hole	



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Job: DREDGED MATERIAL STUDY/GRAND HAVEN, MICH.

Investigator: R. Morrison/K. Yu

Date: 12/4/76

Rig: 6" Truck-mounted auger

Existing Elevation: _____

Well No: M0 (offsite monitoring well)

Depth	Sample Location	Material	Description	Remarks
1		Sand	Light brown, fine sands	Easy drilling
2		"		
3		"		
4		"		
5	<u>∇</u>	"	Water encountered	
6		"		
7		"		
8		"		
9		"		
10		"		
11		"		
12		"		
13		"	Fine to medium grained	Well screen installed 15'-20'
14		Sand	Coarse sands	
15		"	" "	
16		"	" "	
17		"	Coarse + medium grained sands	



Job: DREDGED MATERIAL STUDY/GRAND HAVEN, MICH.

Investigator: R. Morrison/K. Yu

Date: 12/4/76

Rig: 6" Truck-mounted auger

Existing Elevation:

Well No: M0 (offsite monitoring well)

Depth	Sample Location	Material	Description	Remarks
18		Sand	Coarse	More resistance in drilling
19		Clay	Light grey/tight	
20		"	" "	
21		"	" "	
22		"	" "	
23		"	" "	
24		"	" "	
25		"	" "	
26		"	" "	
27		"	" "	
28		"	" "	
29		"	" "	
30		"	" "	
31		"	" "	
32		"	" "	
33		"	" "	
41		"	Bottom of hole	

APPENDIX C: CLIMATOLOGICAL DATA,
SAYREVILLE, NEW JERSEY, CASE STUDY SITE

NEWARK AIRPORT CLIMATOLOGICAL DATA

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31		
Sept. 1976																																	
Temp.																																	
Max.	83	71	72	76	83	74	81	88	77	75	74	82	89	89	77	74	78	80	82	82	69	67	76	68	67	69	75	69	68	63			
Min.	56	60	54	54	60	53	52	63	64	56	50	54	62	63	66	69	70	66	64	61	56	49	44	55	48	55	66	49	43	51			
Prec.		.18									.48				1.10	.15				.05						.21	.11			.22			
Oct. 1976																																	
Temp.																																	
Max.	60	63	66	73	62	69	73	75	76	60	58	62	71	60	73	63	50	51	51	64	64	51	54	53	57	54	42	45	59	57	60		
Min.	55	56	58	54	52	60	63	49	45	40	38	44	47	41	46	44	36	30	48	44	38	36	44	51	33	29	29	33	38	46	49		
Prec.		.18	.02	.26	.02	.01		.04	.95											2.11				.18	.22	.22					.07		
Nov. 1976																																	
Temp.																																	
Max.	46	51	54	58	48	51	53	40	58	48	44	42	43	48	46	47	48	53	58	46	44	40	40	39	39	61	61	57	47	27			
Min.	34	29	41	44	35	35	37	27	23	36	33	31	27	29	28	30	28	38	37	37	31	32	31	28	27	30	50	46	24	16			
Prec.					.24					.02																					.25		
Dec. 1976																																	
Temp.																																	
Max.	30	41	22	33	39	43	56	34	31	47	45	42	41	32	47	45	40	41	46	47	39	30	39	32	36	36	24	26	31	20	21		
Min.	15	17	9	19	23	24	34	15	15	29	34	35	11	11	29	32	32	29	24	35	17	17	24	22	21	20	16	18	18	8	14		
Prec.		.01				1.13						.14				.05					.26				.11	.29	.01	.15	.02				
Jan. 1977																																	
Temp.																																	
Max.	27	36	30	38	32	32	33	28	29	41	23	19	22	26	33	25	7	11	26	35	27	21	29	31	37	33	30	45	13	19	21		
Min.	13	22	18	25	20	20	21	18	18	20	14	12	7	18	17	-5	-2	-1	3	14	17	13	13	17	24	20	19	12	0	9	8		
Prec.							.21		.06	.66			.41	.01		.09								.06	.03		.02						

3

NEWARK AIRPORT CLIMATOLOGICAL DATA (Continued)

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31		
Feb. 1977																																	
Temp.																																	
Max.	27	31	35	36	35	20	29	35	37	43	53	49	49	44	39	29	26	24	41	35	32	47	55	51	58	55	55	49					
Min.	17	19	20	31	13	7	12	14	14	29	30	36	37	37	26	16	14	16	29	31	21	18	36	35	42	37	37	33					
Prec.			.10	.02	.24							.03								.16				2.02	.02		.17						
March 1977																																	
Temp.																																	
Max.	45	45	55	57	63	54	45	52	67	69	71	60	57	58	59	61	51	39	47	42	54	48	40	38	44	55	62	47	80	84	70		
Min.	28	26	30	40	43	38	36	34	38	45	45	43	47	49	47	42	37	32	30	33	35	38	36	25	24	32	35	42	41	58	47		
Prec.			1.29	.02								1.04	.01				.51		.12		2.60						.08						
April 1977																																	
Temp.																																	
Max.	59	49	68	49	51	52	48	46	46	60	53	90	86	73	70	70	69	75	74	61	76	85	78	50	58	51	60	70	60	69			
Min.	40	42	48	39	39	36	31	30	26	33	45	48	58	51	45	45	48	45	50	49	50	59	50	44	44	46	46	43	38	45			
Prec.			.97	.01	.62	.73	.02																	.11	1.07	.01	.50					.04	
May 1977																																	
Temp.																																	
Max.	73	71	73	61	66	87	75	68	46	61	70	78	79	73	74	81	90	90	71	81	82	80	80	86	84	84	85	91	76	68	74		
Min.	46	54	54	50	51	53	40	37	44	47	49	55	51	49	50	59	68	56	55	63	62	62	66	69	65	58	65	54	54	53			
Prec.		.02		.21	.52		.02	.08	.05								.32																.13
June 1977																																	
Temp.																																	
Max.	73	86	72	82	83	68	68	69	61	66	75	80	79	76	82	77	82	88	85	85	77	80	78	77	80	84	81	84	90	87			
Min.	61	63	57	54	65	54	53	50	56	53	59	62	66	63	65	65	63	68	73	63	61	59	61	61	65	68	68	67	71	68			
Prec.	.19	.01			.28	.06	2.11	.16																									

3

NEWARK AIRPORT CLIMATOLOGICAL DATA (Continued)

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31		
July 1977																																	
Temp.																																	
Max.	85	84	82	90	90	85	78	90	86	81	78	78	92	91	93	97	99	98	100	90	102	88	85	90	78	79	78	76	78	82	90		
Min.	72	68	62	66	74	71	68	70	72	70	69	70	73	73	71	72	77	75	78	75	78	68	61	67	69	62	57	62	68	67	67		
Prec.						.03		.03				.62				.02				.59					.59						.10		
Aug. 1977																																	
Temp.																																	
Max.	84	84	74	87	92	92	89	89	89	86	90	85	79	76	82	81	83	76	76	77	74	83	80	80	76	77	83	91	90	90	78		
Min.	69	66	68	70	72	74	74	75	71	71	72	74	67	71	68	68	69	61	58	62	56	65	64	63	55	58	62	68	71	72	70		
Prec.	.51		.35		.21	.05	1.0	.13	.01	.06			.8	.16			.11					.6		.2									

CA

APPENDIX D: WELL LOGS, SAYREVILLE,
NEW JERSEY, CASE STUDY SITE



Job: Dredged Material Study/Sayreville, N.J.

Investigator: R. Morrison/D. Bauer

Date: November 29, 1976

Rig: 4" Hand Bucket Auger

Existing Elevation: 107.93

Well No: NJA (onsite)

Depth	Sample Location	Material	Description	Remarks
1		Dredged Material	Brownish silts	Aerobic
2		"		
3		"	Some clays lenses	
4		"	"	Anaerobic
5		"	"	
6		"	"	
7		"	"	
8		"	"	
9		"	"	
10		▽	Water encountered	
11		"	"	
12		"	Dark grey silts/some fine sands	
13		"	"	
14		"	"	
15		"	"	
16		"	"	
17			Bottom of fill	



Job: Dredged Material Study/Sayreville, N.J.

Investigator: R. Morrison/D. Bauer

Date: November 29, 1976

Rig: 4" Hand Bucket Auger

Existing Elevation: 107.93

Well No: NJA (onsite)

Depth	Sample Location	Material	Description	Remarks
18		Gravels	Unsorted coarse gravels	Extremely permeable water flowing into well
19	├	"		
20	—	"	Bottom of hole	
21				
22				
23				
24				
25				
26				
27				
28				
29				
30				
31				
32				
33				
34				
35				



Job: Dredged Macerals Study/Sayreville, N.J.

Investigator: R. Morrison/D. Bauer

Date: November 29, 1976

Rig: 4" Hard Bucket Auger

Existing Elevation: 106.0

Well No: NJB (onsite)

Depth	Sample Location	Material	Description	Remarks
1		Dredged Material	Silts and mottled clays	Aerobic
2		"	Greyish silts	"
3		"	"	Anaerobic
4		"	"	"
5		"	"	"
6		"	"	"
7		"	"	"
8		"	"	"
9		"	"	"
10		"	Water encountered	"
11		"	Clays with fine sands	"
12		"	"	"
13		"	Bottom of fill	"
14		Gravels	Coarse, unsorted gravels	Fragments of New Brunswick shale
15		"	"	"
16		"	Bottom of hole	"
17				



Job: Dredged Materials Study/Sayreville, N.J.

Investigator: R. Morrison/D. Bauer

Date: November 28, 1976

Rig: 4" Hand Bucket Auger

Existing Elevation: 105.3 (relative)

Well No: NJC (onsite well)

Depth	Sample Location	Material	Description	Remarks
1		Dredged Material	Greyish silts with some fine sand	Aerobic
2		"	"	"
3		"	"	"
4		"	More clays	Anaerobic
5		"	"	"
6		"	"	"
7		"	"	"
8		"	"	
9		"	"	
10		"	"	
11		"	"	
12		"	"	
13		"	"	
14	▽	"	Water encountered	
15		"		
16		"	Bottom of fill	
17			Sand with gravels	Coarse gravels and unconsolidated sands



Site: Dredged Materials Study/Sayreville, N.J.

Investigator: R. Morrison/D. Bauer

Date: November 28, 1976

Rig: 4" Hand Bucket Auger

Existing Elevation: 105.3 (relative)

Well No: NJC (onsite well)

Depth	Sample Location	Material	Description	Remarks
18		Coarse gravels	Well-rounded gravels	
19				
20			Bottom of hole	
21				
22				
23				
24				
25				
26				
27				
28				
29				
30				
31				
32				
33				
34				
35				



Job: Dredged Material Study/Sayreville, N.J.

Investigator: R. Morrison/D. Bauer
 Date: November 28, 1976
 Rig: 4" Hand Bucket Auger
 Existing Elevation: 112.4 (relative)
 Well No: NJD (onsite)

Depth	Sample Location	Material	Description	Remarks
1		Dredged Materials	Greyish silts; clays >20%	Aerobic
2		"	Increasing % of clay	"
3		"		Anaerobic
4		"	Lenses of fine sand encountered	"
5		"		"
6		"		"
7		"		"
8		"		"
9		"		"
10		"		"
11		"	Bottom of fill	"
12		"	Water encountered	
13		Sands w/ gravels	Coarse gravels and fine to medium sands	Fragments of New Brunswick shale observed.
14		"	"	"
15		"	"	"
16			Bottom of hole	
17				



Job: Dredged Materials Study/Sayreville, N.J.

Investigator: R. Morrison/D. Bauer
 Date: November 29, 1976
 Rig: 4" Hand Bucket Auger
 Existing Elevation: 108 (relative)
 Well No: NJE (offsite well)

Depth	Sample Location	Material	Description	Remarks
1		Bog	Plant roots or decomposed vegetation	
2		Silts with sands	Mottled grey silt/ fine sand	
3		Clay	Dark grey clay	Tight; hard crilling
4		Clay	Water encountered	
5		"	Reddish/grey clay	
6		"	"	
7		"	Bottom of hole	
8				
9				
10				
11				
12				
13				
14				
15				
16				
17				



Job: Dredged Material Study/Sayreville, N.J.

Investigator: D. Bauer/W. Hutchinson

Date: November 29, 1976

Rig: 4" Hand Bucket Auger

Existing Elevation: 101.0 (relative)

Well No: NJF (offsite)

Depth	Sample Location	Material	Description	Remarks
1		Bog	Decomposed roots and vegetation; greyish silt	
2		Sand	Fine reddish sands	
3		"	Coarse sands	
4		"		
5		Sand/gravels	Coarse sands/gravels	Resistance in drilling
6		▽ "	Water encountered	
7		"	Well rounded gravels with fine sands	
8		"	"	
9		"	"	
10	—	"	Bottom of hole	
11				
12				
13				
14				
15				
16				
17				



Job: Dredged Material Study/Sayreville, N.J.

Investigator: R. Morrison/R. Gilbert

Date: November 29, 1976

Rig: 4" Hand Bucket Auger

Existing Elevation: 102.1

Well No: NJH (offsite)

Depth	Sample Location	Material	Description	Remarks
1		Bog	Roots, decomposed vegetation, fine sands	
2		Sands	Fine grained yellowish sand	
3		"	"	
4		"	"	
5		"	"	
6			Water encountered	
7		Gravels/sand	Pea-size gravels with fine grained sand	
8			Bottom of hole	
9				
10				
11				
12				
13				
14				
15				
16				
17				



Job: Dredged Material Study/Sayreville, N.J.

Investigator: W. Hutchinson/R. Gilbert

Date: NOVEMBER 29, 1976

Rig: 4" Hand Bucket Auger

Existing Elevation: _____

Well No: NJI (background well)

Depth	Sample Location	Material	Description	Remarks
1		Bog	Roots, decomposed vegetation/fine sands	
2		Sand	Fine grained yellowish sand	Walls sloughing in
3		"		
4		▽	Water encountered	
5		"		
6		Sand/gravels	Some gravels present	
7		"	Bottom of hole	
8				
9				
10				
11				
12				
13				
14				
15				
16				
17				



Job: Dredged Material Study/Sayreville, N.J.

Investigator: W. Hutchinson/R. Gilbert

Date: November 29, 1976

Rig: 4" Hand Bucket Auger

Existing Elevation: _____

Well No: NJJ (background well)

Depth	Sample Location	Material	Description	Remarks	
1		Bog	Roots, decomposed vegetation/fine sands		
2		Sand	Fine grained yellowish sands		
3		"	"		
4			Water encountered		
5					
6		Sands/gravels	Pea gravels present in small amounts		
7			Bottom of hole		
8					
9					
10					
11					
12					
13					
14					
15					
16					
17					



Job: Dredged Materials Study/Sayreville, N.J.

Investigator: R. Morrison/K. Yu

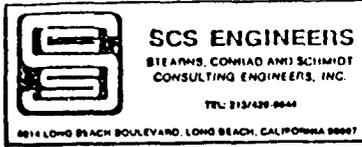
Date: November 29, 1976

Rig: 10" Water Rotary

Existing Elevation: _____

Well No: OFMW (offsite pumping Well)

Depth	Sample Location	Material	Description	Remarks
1		Bog	Roots and decomposed vegetation	Easy drilling
2	I	Gravels	Unsorted coarse gravels	"
3		"	"	"
4	I	"	"	
5		▽ "	Water encountered	
6	I	"	"	
7		"	"	
8	I	"	"	
9		Sand	Yellowish fine sand	
10	I	Clay	Light colored clay	
11		"	"	
12	I	"	"	
13		"	"	
14	I	"	Dark clay; very tight	
15		"	"	
16	I	"	"	
17		"	"	



Job: Dredged Materials Study/Sayreville, N.J

Investigator: R. Morrison/K. Yu

Date: November 29, 1976

Rig: 10" Water Rotary

Existing Elevation: _____

Well No: OFMW (offsite pumping well)

Depth	Sample Location	Material	Description	Remarks
18	I	Clay	Dark clay	
19		"		
20	I	Sand	Fine grained sand	
21		"	Coarse sand	
22	I	Gravels/sand	Coarse gravels with sand	
23				
24	I	Gravels	Gravels; well rounded; pebble size	More resistance during drilling
25		"		
26	I	"		
27		"	Coarse gravels	"
28	I	"	"	Screen installed from 25' to 35'
29		"	"	
30	I	"	"	Pebbles of glauconite
31		"	"	
32	I	"	"	Fragments of New Brunswick shale
33		"	"	
34		"	"	
35	I	"	Bottom of hole	



Job: Dredged Materials Study/Sayreville, N.J.

Investigator: R. Morrison/K. Yu

Date: November 29, 1976

Rig: 10" Water Rotary

Existing Elevation: 104.8 (relative)

Well No: NJP3 (offsite observation well)

Depth	Sample Location	Material	Description	Remarks
1		Bog	Decomposed roots and vegetation	
2	I	Gravels	Coarse gravels with medium to coarse sands	
3		"	"	
4		"	"	
5		▽	Water encountered	
6	I	"	"	
7		"	"	
8	I	Sands	Medium grained; light yellow sand	
9		"		
10	I	Clay	Light grey clay	
11		"		
12	I	"		
13		"		
14	I	"		
15		"	Dark grey	Very tight
16	I	"	"	
17				



Job: Dredged Materials Study/Sayreville, N.J.

Investigator: R. Morrison/K. Yu

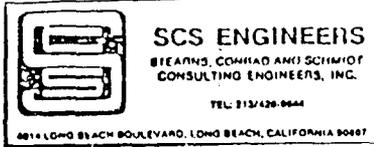
Date: November 29, 1976

Rig: 10" Water Rotary

Existing Elevation: 104.8 (relative)

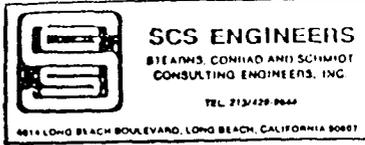
Well No: NJP3 (offsite observation well)

Depth	Sample Location	Material	Description	Remarks
18	I	Clay	Dark grey	
19		"	"	
20	I	Sand	Fine sands; yellowed	
21		"		
22	I	"	Medium grained	
23		"		
24		"		
25	I	"	Coarse grained	
26		"		
27		"		4" screen
28	I	"		
29		"		4" well screen installed from 25-35'
30		Gravel/sands	Very coarse gravels with fine sands	
31		Gravels	Coarse gravels; pebbles size	Glauconate viable
32	I			
33				Fragments of New Brunswick shale
34				
35	I		Bottom of hole	



Job: Dredged Material Study/Sayreville, N.J.
 Investigator: R. Morrison/K. Yu
 Date: November 29, 1976
 Rig: 10" Water Rotary Rig
 Existing Elevation: 104. (relative)
 Well No: NJP4 (offsite observation well)

Depth	Sample Location	Material	Description	Remarks
1		Bog	Decomposed roots and vegetation	
2	I	Gravels	Coarse gravels with medium to coarse sands	
3		"	"	
4		"	"	
5		▽ "	Water encountered	
6	I	"	"	
7		"	"	
8	I	Sands	Medium grained; light yellow sand	
9		"		
10	I	Clay	Light grey clay	
11		"		
12	I	"		
13		"		
14	I	"		
15		"	Dark grey	Very tight
16	I	"	"	
17				



Job: Dredged Material Study/Sayreville, N.J.

Investigator: R. Morrison/K. Yu

Date: November 29, 1976

Rig: 10" Water Rotary Rig

Existing Elevation: 104. (relative)

Well No: HJP4 (offsite pumping well)

Depth	Sample Location	Material	Description	Remarks
18	I	Clay	Dark grey	
19		"	"	
20	I	Sand	Fine sands; yellowed	
21		"		
22	I	"	Medium grained	
23		"		
24		"		
25	I	"	Coarse grained	
26		"		
27		"		4" screen
28	I	"		
29		"		4" well screen installed from 25-35'
30		Gravel/sands	Very coarse gravels with fine sands	
31		Gravels	Coarse gravels; pebbles size	Glauconate viable
32	I	"		
33				Fragments of New Brunswick shale
34				
35	I		Bottom of hole	

APPENDIX E: CLIMATOLOGICAL DATA,
HOUSTON, TEXAS, CASE STUDY SITE

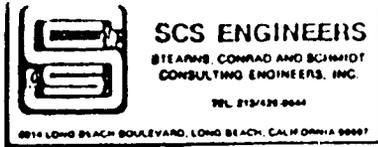
HOUSTON INTERCONTINENTAL AIRPORT CLIMATOLOGICAL DATA

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	
<u>Sept. 1976</u>																																
Temp.																																
Max.	95	88	92	93	93	92	92	91	93	86	82	84	91	88	89	90	88	88	85	77	82	82	84	86	88	89	85	80	78	82		
Min.	69	68	68	71	70	68	70	71	69	67	58	60	65	69	67	68	68	66	68	62	55	55	56	62	64	62	68	64	60	54		
Prec.	1.77	.06	.05	.05				.01					.42						.50	7.6						.52	.13	.18				
<u>Oct. 1976</u>																																
Temp.																																
Max.	85	84	85	86	78	74	73	58	72	81	82	81	80	81	76	69	68	72	71	61	67	70	81	69	62	67	58	53	58	67	68	
Min.	53	55	56	66	60	52	47	44	40	44	49	50	54	51	53	55	45	41	42	36	33	44	63	61	55	49	48	45	46	41	41	
Prec.					.17		.06	.15							1.87	.13			.40				1.96				.20	.89				
<u>Nov. 1976</u>																																
Temp.																																
Max.	67	70	75	73	67	77	78	65	77	78	80	50	42	41	52	46	63	52	55	73	67	60	58	67	68	80	68	39	43	53		
Min.	41	38	38	44	37	39	42	42	42	55	47	42	34	36	36	39	41	44	49	54	44	33	34	50	52	63	39	26	22	19		
Prec.									.29	.10	.04	.42						.33	.88	.08					.22	.04	.65					
<u>Dec. 1976</u>																																
Temp.																																
Max.	53	56	63	67	65	66	49	64	66	68	62	50	63	51	53	68	66	68	65	68	47	47	60	64	61	61	65	70	68	72	40	
Min.	28	32	29	31	51	44	29	27	31	56	41	41	49	43	45	40	40	45	58	34	25	39	35	30	45	31	35	41	30	40	25	
Prec.	.11				.47	1.03				.16	.95	.66	.54	.15					1.25	.24	.02	.04	.01	.59								
<u>Jan. 1977</u>																																
Temp.																																
Max.	43	39	44	54	58	53	56	55	56	44	45	52	57	51	59	43	44	40	47	61	65	51	54	59	61	62	77	73	50	43	53	
Min.	32	31	34	41	46	40	31	42	20	18	20	39	43	34	33	27	22	24	18	22	27	33	46	34	29	37	43	35	28	35	31	
Prec.	.01	.81			.29		.09	.12			.10	.18									.17	.10									.78	.02

HOUSTON INTERCONTINENTAL AIRPORT CLIMATOLOGICAL DATA (Continued)

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31		
July 1977																																	
Temp.																																	
Max.	94	93	95	97	93	92	92	93	94	92	90	97	98	94	98	93	91	93	92	87	95	94	96	96	95	95	91	92	94	95	98		
Min.	73	72	66	69	70	70	69	70	69	71	71	72	67	71	69	69	71	71	70	73	71	71	74	73	71	73	74	74	72	71	72		
Prec.					.05								.1	.2	.3	.01		.1	.5						.03	.6		.6					
Aug. 1977																																	
Temp.																																	
Max.	96	99	100	98	89	91	97	97	96	98	92	92	93	89	92	95	95	82	90	94	93	93	93	96	92	91	90	87	91	91			
Min.	72	73	70	71	71	69	74	73	72	72	72	73	75	75	73	73	72	76	75	73	74	75	76	74	74	73	75	72	75	73			
Prec.				.01	.13							.3	.2	.1	.2		.1	.09	1.6						.01	.4	.4	.5					

APPENDIX F: WELL LOGS, HOUSTON, TEXAS
CASF STUDY SITE



Job: Dredged Material Study/Houston, Texas

Investigator: R. Morrison/D. Myers

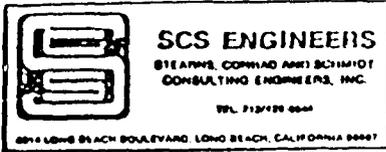
Date: 12/3/76

Rig: 4" Hand Bucket Auger

Existing Elevation: 44.8

Well No: HA

Depth	Sample Location	Material	Description	Remarks
1		Dredged Material	Clay	Aerobic
2		"		
3		"	Blackish	Anaerobic
4		"		
5		"	Water Encountered	
6		"	Light brown clay	
7		"		
8		"		
9		"	Clay	
10		"	"	
11		"	"	
12		"	"	
13		"	"	
14		"	"	
15		"	Fine sand	
16		"	Clay	
17		"		



Job: Dredged Material Study/Houston, Texas

Investigator: R. Morrison/D. Myers

Date: 12/3/76

Rig: 4" Hand Bucket Auger

Existing Elevation: 44.8

Well No: HA

Depth	Sample Location	Material	Description	Remarks
18	├		Bottom of hole	
19	├			
20				
21				
22				
23				
24				
25				
26				
27				
28				
29				
30				
31				
32				
33				
34				
35				



Job: Dredged Material Study/Houston, Texas

Investigator: R. Morrison/D. Myers

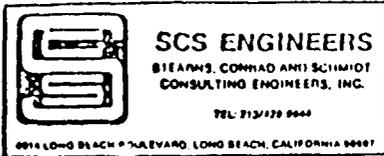
Date: 12/3/76

Rig: 4" Hand Bucket Auger

Existing Elevation: 48.8

Well No: HB

Depth	Sample Location	Material	Description	Remarks
1		Dredged Material	Clay	Aerobic
2		"		
3		"		Anaerobic
4		"	Water encountered	
5		"	Black clay	
6		"		
7		"		
8		"		
9		"	Sand clay	
10				
11		"		Very difficult
12		"		coving through
13		"		material
14		"	Clay	
15		"		
16		"		
17		"		



Job: Dredged Material Study/Houston, Texas

Investigator: R. Morrison/D. Myers

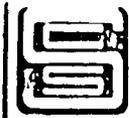
Date: 12/3/76

Rig: 4" Hand Bucket Auger

Existing Elevation: 48.8

Well No: HB

Depth	Sample Location	Material	Description	Remarks
18		"	Clays	
19		"	"	
20		"	"	
21	—		Bottom of hole	
22				
23				
24				
25				
26				
27				
28				
29				
30				
31				
32				
33				
34				
35				



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CONSULTING ENGINEERS, INC.

TEL: 714/426-0644

8014 LONG BEACH BOULEVARD, LONG BEACH, CALIFORNIA 90807

Job: Dredged Material Study/Houston, Texas

Investigator: R. Morrison/D. Myers

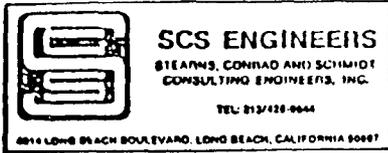
Date: 12/3/76

Rig: 4" Hand Bucket Auger

Existing Elevation: 48.8

Well No: HC

Depth	Sample Location	Material	Description	Remarks	
1		Dredged Material	Clay	aerobic	
2		"	"		
3		"		anaerobic	
4		∇	"	Water encountered	sulfide odor
5		"			present
6		"	Sandy clay		
7		"			
8		"			
9		"			
10		"			
11		"		Drilling	
12		"	Clay	extremely	
13				difficult	
14					
15					
16					
17					



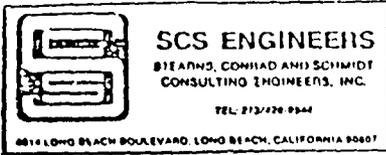
Job: Dredged Material Study/Houston, Texas
 Investigator: B. Morrison/D. Myers
 Date: 12/3/76
 Rig: 4" Hand Bucket Auger
 Existing Elevation: 48.8
 Well No: HC

Depth	Sample Location	Material	Description	Remarks
18	 	Dredged Material	Clay	
19				
20				
21				Bottom of hole
22				
23				
24				
25				
26				
27				
28				
29				
30				
31				
32				
33				
34				
35				



Job: Dredged Material Study/Houston, Texas
 Investigator: R. Morrison/D. Myers
 Date: 12/3/76
 Rig: 4" Hand Bucket Auger
 Existing Elevation: 44.9
 Well No: HD

Depth	Sample Location	Material	Description	Remarks
1		Dredged Material	Fine sands	aerobic
2		"	"	
3		"	"	
4		"	Water encountered	
5		"	"	anaerobic
6			"	
7			Sand clay	
8		"	"	
9		"	"	
10			"	
11			Clay	
12			"	
13			"	
14			Sand clay	
15		"	"	
16		"	Clay	
17		"		



Job: Dredged Material Study/Houston, Texas

Investigator: R. Morrison/D. Myers

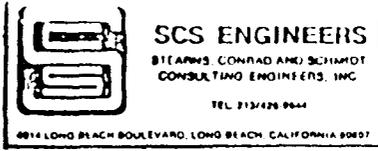
Date: 12/3/76

Rig: 4" Hand Bucket Auger

Existing Elevation: 44.9

Well No: HD

Depth	Sample Location	Material	Description	Remarks
18		Dredged Material	Clay	
19		"	"	
20		"	"	
21			Bottom of hole	
22				
23				
24				
25				
26				
27				
28				
29				
30				
31				
32				
33				
34				
35				



Job: Dredged Material Study/Houston, Texas
 Investigator: R. Morrison/D. Myers
 Date: 12/3/76
 Rig: 4" Hand Bucket Auger
 Existing Elevation: _____
 Well No: HE

Depth	Sample Location	Material	Description	Remarks
1		Dredged Material	Sand	Aerobic
2				
3			Water encountered	
4		"		
5		"		Anaerobic
6		"	Black clay	
7				
8		"		
9		"	Fine sand	
10			Bottom of hole	
11				
12				
13				
14				
15				
16				
17				



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6814 LONG BEACH BOULEVARD, LONG BEACH, CALIFORNIA 94807

Job: Dredged Disposal Study/Houston, Texas

Investigator: R. Morrison/D. Myers

Date: 12/3/76

Rig: 4" Hand Bucket Auger

Existing Elevation: _____

well no: HG

Depth	Sample Location	Material	Description	Remarks	
1		Dredged Material	Sand	Aerobic	
2			"		
3			Sand	Anaerobic	
4				"	
5				"	
6				Water encountered	
7				"	
8				"	
9				Bottom of hole	
10					
11					
12					
13					
14					
15					
16					
17					



Job: Dredged Material Study/Houston, Texas

Investigator: E. Morrison/D. Myers

Date: 12/3/76

Rig: 4" Hand Bucket Auger

Existing Elevation: _____

Well No: HH

Depth	Sample Location	Material	Description	Remarks	
1		Dredged Material	Sand	Aerobic	
2					
3			Sand blackish	Anaerobic	
4				Water encountered	
5				Sand	Hole sloughing
6					in
7					
8					
9'				Bottom of hole	
10					
11					
12					
13					
14					
15					
16					
17					



Job: Dredged Material Study/Houston, Texas

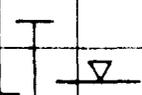
Investigator: R. Morrison/D. Myers

Date: 12/3/76

Rig: 4" Hand Bucket Auger

Existing Elevation: 46.7

Well No: H1

Depth	Sample Location	Material	Description	Remarks
1		Dredged Material	Sand	Aerobic
2		"	"	
3		"	"	Anaerobic
4		"	Blackish	"
5		"	"	"
6		"	Water encountered	
7		"	sand	
8		"		
9		"		
10		"	Bottom of hole	
11				
12				
13				
14				
15				
16				
17				



Job: Dredged Material Study/Houston, Texas

Investigator: R. Morrison/D. Myers

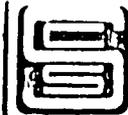
Date: 12/3/76

Rig: 4" Hard Bucket Auger

Existing Elevation: _____

Well No: HJ

Depth	Sample Location	Material	Description	Remarks
1		Dredged Material	Sand	aerobic
2		"	"	
3		"	"	
4		"	"	anaerobic
5		"	"	
6		"	Water encountered	
7		"	"	
8		"	"	
9		"	"	
10		"	Bottom of hole	
11				
12				
13				
14				
15				
16				
17				

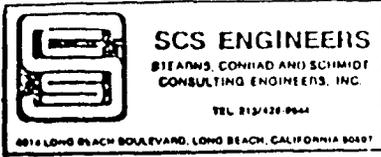


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4014 LONG BEACH BOULEVARD, LONG BEACH, CALIFORNIA 90807

Job: Dredged Material Study/Houston, Texas
 Investigator: R. Morrison/D. Myers
 Date: 12/4/76
 Rig: 12" Bucket Auger
 Existing Elevation: 49.3'
 Well No: ONPW (onsite)

Depth	Sample Location	Material	Description	Remarks
1		Dredged Material	Very fine	Aerobic
2			Light brown clay	Anaerobic
3			Blackish clays	Sulfide smell
4		"	"	Present
5		"	"	
6		"	"	
7		Dredged Material	Water encountered	
8		"	Blackish	Material
9		"	"	sloughing into
10		"	"	hole
11		Dredged Material	"	
12			Sands	
13		Dredged Material		
14		"	Light grey clay	
15		"		
16		"		
17				



Job: Dredge Material Study/Houston, Texas

Investigator: R. Morrison/D. Myers

Date: 12/4/76

Rig: 12' Bucket Auger

Existing Elevation: 49.3'

Well No: ONPW (onsite)

Depth	Sample Location	Material	Description	Remarks
18				
19		Clay	Blackish	
20		"		
21		"		
22		"		
23		"		
24		"	Spoil/soil interface	
25		Clay with gravels		Well
26		Sand/clay	Mottled clays	screened from
27		" "	"	25' to 30' with
28		Sand/clay	"	4" PVC casing with
29		" "	"	.004" screen
30		—	Bottom of hole	
31				
32				
33				
34				
35				



SCS ENGINEERS

BEARNS, CONRAD AND SCHMIDT
CONSULTING ENGINEERS, INC.

TEL: 313/429 9644

4814 LONG BEACH BOULEVARD, LONG BEACH, CALIFORNIA 90807

Job: Dredged Material Study/Houston, Texas

Investigator: R. Morrison/D. Myers

Date: 12/4/76

Rig: 12" Bucket Auger

Existing Elevation: 49.2

Well No: QNOW (onsite)

Depth	Sample Location	Material	Description	Remarks
1		Topsoil		Aerobic
2		Dredged Material	Light brown clay	
3		"	Blackish clays	Sulfide
4		"		small present
5		"	Clays	Anaerobic
6		"		
7		"	Water encountered	
8		Dredged Material	Light grey clay	
9		"	"	
10		"	"	
11		"	"	
12		"	"	
13		"	"	
14		"	"	
15		"	"	
16		"	"	
17		"	"	



Job: Dredged Material Study/Houston, Texas

Investigator: R. Morrison/D. Myers

Date: 12/4/76

Rig: 12" Bucket Auger

Existing Elevation: 49.2

Well No: ONOW (onsite)

Depth	Sample Location	Material	Description	Remarks
18		"	"	
19		"	"	
20		"	"	
21		"	"	
22		"	"	
23		"	"	
24		Clays with/gravels	Spoil/soil interface	Well screened
25		Clay with/sands	Coarse gravels grey clays	from 25' to 30'
26		"	Mottled clays with/fine sands	w/ 2" casing
27		"		with .004"
28		"		screen
29				
30			Bottom of hole	
31				
32				
33				
34				
35				

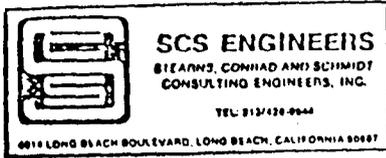
**SCS ENGINEERS**STEARNS, CONRAD AND SCHMIDT
CONSULTING ENGINEERS, INC.

TEL. 813/438-8644

8816 LONG BEACH BOULEVARD, LONG BEACH, CALIFORNIA 90807

Job: Dredged Material Study/Houston, TexasInvestigator: R. Morrison/D. MyersDate: 12/4/76Rig: 12" Bucket AugerExisting Elevation: 33.4'Well No: 0-FPW-J (offsite)

Depth	Sample Location	Material	Description	Remarks
1		Silts	Light grey	
2				
3				
4				
5		Clay	Dark brown	Very tight
6				
7				
8		Clay with/sand	Mottled clays	
9			With fine sands	
10				
11		Clay	Red, pink, white, grey, clays	Very tight
12				
13				
14				
15				
16		Clay with/sand	Mottled clay with	
17			fine sands	



Job: Dredged Material Study/Houston, Texas
 Investigator: R. Morrison/D. Myers
 Date: 12/4/76
 Rig: 12" Bucket Auger
 Existing Elevation: 33.4
 Well No: 0-FPW-1 (offsite)

Depth	Sample Location	Material	Description	Remarks
18				
19		Clay	Reddish clays with grey streaks	
20		"	Light grey clays	
21		"	" "	
22		"	" "	
23		"	" "	
24		"	" "	
25		"	" "	
26			Mottled clays with	
27		Clay with/gravel	Coarse gravels	
28	▽		Water encountered	
29			" "	
30			" "	Well screened
31		Clay with/gravel	" "	from 30 to 35'
32			" "	with 4" PVC
33			" "	casing with
34			" "	.009" slotting
35		Clay	Bottom of hole	



Job: Dredged Material Study/Houston, Texas

Investigator: R. Morrison/D. Myers

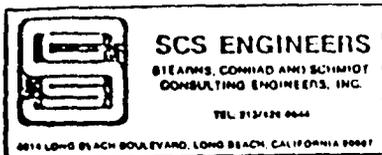
Date: 12/4/76

Rig: 12" Bucket Auger

Existing Elevation: _____

Well No: 0-FPW-2 (offsite)

Depth	Sample Location	Material	Description	Remarks
1		Topsoil		
2				
3				
4		Clay	Reddish	
5		"	Dark brown	
6		"	Dark brown	
7		"	"	
8		"	"	
9		"	"	
10		"	"	
11		"	Light brown	
12		"	"	
13		"	"	
14		"	Mottled	
15		"	"	
16		"	"	
17		Sand clay	Fine sands and clay	



Job: Dredge Material Study/Houston, Texas

Investigator: R. Morrison/D. Myers

Date: 12/4/76

Rig: 12" Bucket Auger

Existing Elevation: _____

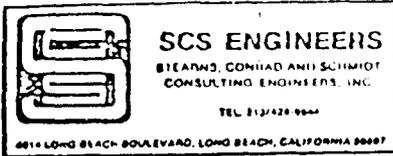
Well No: 0-FPW-2 (offsite)

Depth	Sample Location	Material	Description	Remarks
18		Sandy clay	Clay with/fine sands	
19			"	
20		"	"	
21		"	"	
22		Clay with gravels	White clay with/coarse gravel	
23		"	"	
24		"	"	
25		"	"	
26		Clay	White	
27		"	"	
28		"	"	
29		"	"	
30		Clay	White	
31		"	"	
32		"	"	
33		"	"	
34		"	Red, pink, white	
35		"		



Title: Dredged Material Study/Houston, Texas
 Investigator: R. Morrison/D. Mayers
 Date: 12/4/76
 Rig: 12" Bucket Auger
 Existing Elevation: _____
 Well No: 0-FPW-2 (offsite)

Depth	Sample Location	Material	Description	Remarks
36		Clay	Red, pink, white	Artesian
37	▽		Water encountered	
38		Sand clay	Coarse gravel with clay	
39				
40	—		Bottom of hole	
41				
42				
43				
44				
45				
46				
47				
48				
49				
50				
51				
52				
53				



Job: Dredged Material Study/Houston Texas
 Investigator: R. Morrison/D. Myers
 Date: 12/4/76
 Rig: 12" Bucket Auger
 Existing Elevation: 33.4
 Well NO: OEMW (offsite)

Depth	Sample Location	Material	Description	Remarks
18				
19		Clay	Reddish clays with grey streaks	
20		"	Light grey clays	
21		"	" "	
22		"	" "	
23		"	" "	
24		"	" "	
25		"	" "	
26			Mottled clays with	
27		Clay with/gravel	Coarse gravels	
28	▽	"	Water encountered	
29		"	" "	
30			" "	Well screened
31		Clay with/gravel	" "	from 30 to 35'
32			" "	with 4" PVC
33			" "	casing with
34			" "	.009" slotting
35		Clay	Bottom of hole	



Job: Dredged Material Study/Houston, Texas

Investigator: R. Morrison/D. Myers

Date: 12/4/76

Rig: 12" Bucket Auger

Existing Elevation: 33.4'

Well No: QFMW (offsite)

Depth	Sample Location	Material	Description	Remarks
1		Silts	Light grey	
2				
3				
4				
5		Clay	Dark brown	Very tight
6				
7				
8		Clay with/sand	Mottled clays	
9			With fine sands	
10				
11		Clay	Red, pink, white, grey, clays	Very tight
12				
13				
14				
15				
16		Clay with/sand	Mottled clay with	
17			fine sands	

APPENDIX G: CLIMATOLOGICAL DATA,
PINTO ISLAND, ALABAMA, CASE STUDY SITE

CLIMATOLOGICAL DATA FOR BATES FIELD, MOBILE, ALABAMA

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
Sept. 1976																															
Temp. Max.	85	91	89	83	80	83	78	82	90	81	83	86	88	86	86	88	88	89	90	88	79	81	85	82	81	83	82	82	81	78	
Temp. Min.	71	71	72	69	71	68	71	72	71	65	57	62	67	63	60	61	63	67	67	67	69	58	58	70	70	71	71	70	67	59	
Temp. Prec.		.69	.09	.38	.22	.54	.55	.12													.07			.32	.10	.14	.27	.02			
Oct. 1976																															
Temp. Max.	80	83	87	84	83	75	71	61	68	73	75	75	78	82	79	70	67	70	75	65	64	71	73	78	70	65	58	61	63	73	62
Temp. Min.	55	56	64	61	63	60	58	49	45	46	47	50	49	53	56	56	50	44	51	42	37	40	46	58	57	46	42	48	44	48	45
Temp. Prec.					2.04										1.01									.06							2.56
Nov. 1976																															
Temp. Max.	62	66	69	65	57	66	73	59	67	73	73	61	52	47	49	49	53	66	60	60	64	54	55	64	69	67	72	67	38	46	
Temp. Min.	41	40	38	41	36	33	39	33	31	51	55	39	33	43	43	44	44	38	51	51	43	33	31	33	41	55	66	37	25	24	
Temp. Prec.										.01	.07		.29		.02	.28		.46	.13						.64	.54	2.15	.05			
Dec. 1976																															
Temp. Max.	55	56	59	62	63	55	60	53	53	58	63	69	58	57	50	64	68	70	71	63	42	39	44	56	62	55	64	71	62	68	60
Temp. Min.	27	30	30	32	35	44	39	29	28	41	53	58	42	41	47	42	34	42	47	34	36	25	29	25	45	38	34	48	35	37	26
Temp. Prec.					.28	.25				.33	.85	.41	.09	.28	.02					.04	.46				1.14					.05	.01
Jan. 1977																															
Temp. Max.	41	33	43	50	66	64	49	52	67	46	41	49	54	67	53	45	35	31	34	56	56	54	53	56	53	57	65	70	43	41	43
Temp. Min.	25	31	33	40	44	39	36	35	46	24	20	26	36	48	36	23	15	21	12	24	25	31	39	39	32	32	48	34	22	28	26
Temp. Prec.	1.07	.01	.01	.01	.61				.24				.44	1.58				.04						.37		.71			.08	.37	

62

CLIMATOLOGICAL DATA FOR BATES FIELD, MOBILE, ALABAMA (Continued)

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31		
Feb. 1977																																	
Temp.																																	
Max.	44	58	52	53	56	54	56	58	67	67	71	71	69	73	59	50	65	71	72	60	64	72	71	72	76	79	70	59					
Min.	26	30	41	44	37	28	31	31	38	36	41	57	44	39	38	28	32	53	49	33	32	44	58	53	52	38	43	36					
Prec.			.75									.01							.01				.49										
March 1977																																	
Temp.																																	
Max.	65	65	67	69	56	50	61	66	68	67	69	70	76	79	75	80	74	83	82	77	81	71	70	66	74	75	76	73	80	82	74		
Min.	35	40	55	53	48	47	40	35	37	54	60	52	47	46	59	60	55	70	70	61	64	51	40	48	51	54	66	61	72	71	58		
Prec.			1.03	.54	.12					.21	.02	.99			.01					.13		.15				.07	1.27	.02	.02	1.48			
April 1977																																	
Temp.																																	
Max.	80	80	82	79	63	73	79	84	83	80	81	81	82	81	82	84	84	82	84	78	75	75	81	71	75	72	77	80	81	83			
Min.	58	71	72	58	48	41	45	55	55	53	53	56	55	53	57	61	64	64	64	65	61	66	62	57	54	47	49	57	58	56			
Prec.			.01	.32												.01					.46	1.93											
May 1977																																	
Temp.																																	
Max.	82	71	79	82	83	83	86	89	84	81	82	82	85	84	86	88	86	87	89	91	85	87	88	87	86	84	89	90	89	95	93		
Min.	59	70	67	64	66	67	66	68	66	59	64	64	61	63	64	65	64	63	64	65	65	66	66	67	64	67	67	67	71	74	68		
Prec.	2.71	.24					.18	.08													.42	.10			.12	.43	.20	.10			.72		
June 1977																																	
Temp.																																	
Max.	92	90	96	96	94	94	84	85	90	95	95	94	89	91	93	94	90	91	93	93	96	94	94	97	96	94	95	89	92	95			
Min.	68	67	71	71	71	73	68	60	66	70	75	74	75	74	74	72	75	75	74	74	75	76	77	77	78	78	75	77	75	74			
Prec.	.63											.01			.24	.30	.03	.05															

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APPENDIX H: WELL LOGS, PINTO ISLAND,
ALABAMA, CASE STUDY SITE



Job: Dredged Material Study/Pinto Island
 Investigator: R. Morrison/T. Boston
 Date: 1/17/77
 Rig: 4" hand auger
 Existing Elevation: 24.57
 Well No: PI-A

Depth	Sample Location	Material	Description	Remarks
1		Dredged material	Sand	
2		Dredged material	Sand	
3		Dredged material	Sand	
4		Dredged material	Sand	
5		Dredged material	Water encountered	
6		Dredged material	Sand	
7		Dredged material	Sand	
8		Dredged material	Sand	
9		Dredged material	Sand	
10		Dredged material	Sand	
11		Dredged material	Sand	
12		Dredged material	Sand	
13		Dredged material	Sand	
14		Dredged material	Sand	
15		Dredged material	Sand	
16		Sand	Dredged material/soil interface	
17		Sand	Dredged material/soil interface	



SCS ENGINEERS

BEARNS, CONRAD AND SCHMIDT
CONSULTING ENGINEERS, INC.

TEL: 913/428-8044

2011 LONG BEACH BOULEVARD, LONG BEACH, CALIFORNIA 90807

Job: Dredged Material Study/Pinto Island

Investigator: R. Morrison/T. Boston

Date: 11/17/77

Rig: 4" hand auger

Existing Elevation: 18.52

Well No: PI-B

Depth	Sample Location	Material	Description	Remarks
1		Dredged material	Fine sand	Aerobic
2		Dredged material	Fine sand	
3		Dredged material	Fine sand	
4		Dredged material	Fine sand	
5		Dredged material	Fine sand	
6		Dredged material	Water encountered	
7		Dredged material	Water encountered	
8		Dredged material	Water encountered	
9		Dredged material	Water encountered	
10		Dredged material	Water encountered	
11		Dredged material	Water encountered	
12		Dredged material	Water encountered	
13		Dredged material	Water encountered	
14		Dredged material	Water encountered	
15	Dredged material	Water encountered		
16		Sand	Dredged material/soil interface	
17		Sand	Dredged material/soil interface	



Job: Dredged Material Study/Pinto Island

Investigator: R. Morrison/I. Boston

Date: 1/17/77

Rig: 4" hand auger

Existing Elevation: 18.88'

Well No: PI-C

Depth	Sample Location	Material	Description	Remarks
1		Dredged material	Fine sand	
2		Dredged material	Fine sand	
3		Dredged material	Fine sand	
4		Dredged material	Fine sand	
5		Dredged material	Fine sand	
6		Dredged material	Fine sand	
7		Dredged material	Water encountered	
8		Dredged material	Water encountered	
9		Dredged material	Water encountered	
10		Dredged material	Water encountered	
11		Dredged material	Water encountered	
12		Dredged material	Water encountered	
13		Dredged material	Water encountered	
14		Dredged material	Water encountered	
15		Dredged material	Water encountered	
16			Sand	Dredged material/soil interface
17		Sand	Dredged material/soil interface	



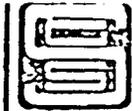
Job: Dredged Material Study/Pinto Island
 Investigator: R. Morrison/T. Boston
 Date: 1/17/77
 Rig: 4" bucket auger
 Existing Elevation: 24.57
 Well No: PI-D

Depth	Sample Location	Material	Description	Remarks
1		Dredged material	Sand	
2		Dredged material	Sand	
3		Dredged material	Sand	
4		Dredged material	Sand	
5		Dredged material	Sand	
6		Dredged material	Sand	
7		Dredged material	Sand	
8		Dredged material	Sand	
9		Dredged material	Water encountered	
10		Dredged material	Water encountered	
11		Dredged material	Water encountered	
12		Dredged material	Water encountered	
13		Dredged material	Water encountered	
14		Dredged material	Water encountered	
15		Dredged material	Water encountered	
16		Dredged material	Dredged material/soil interface	
17		Dredged material	Dredged material/soil interface	



Job: Dredged Material Study/Pinto Island
 Investigator: R. Morrison/T. Boston
 Date: 1/17/77
 Rig: 4" bucket auger
 Existing Elevation: 14.90
 Well No: PI-E

Depth	Sample Location	Material	Description	Remarks
1	—	Sand	Fine to med.	
2	—	Sand ▽	Water encountered	
3	—	Sand	Water encountered	
4	—	Sand	Water encountered	
5	—	Sand	Water encountered	
6	—	Sand	Water encountered	
7	—		Bottom of hole	
8				
9				
10				
11				
12				
13				
14				
15				
16				
17				



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CONSULTING ENGINEERS, INC.

TEL: 312/428-8844

2014 LONG BEACH BOULEVARD, LONG BEACH, CALIFORNIA 90807

Job: Dredged Material Study/Pinto Island

Investigator: R. Morrison/T. Boston

Date: 1/17/77

Rig: 4" hand auger

Existing Elevation: 14-97

Well No: PI-F

Depth	Sample Location	Material	Description	Remarks
1		Sand	Fine to med.	
2		Sand	Fine to med.	
3		Sand	Fine to med.	
4		Sand	Fine to med.	
5		Sand [▽]	Water encountered	
6		Clay	Reddish clay	
7		Clay	Reddish clay	
8		Clay	Reddish clay	
9	—		Bottom of hole	
10				
11				
12				
13				
14				
15				
16				
17				



SCS ENGINEERS

BEARNS, CONRAD AND SCHMIDT
CONSULTING ENGINEERS, INC.

TEL: 913/428-9644

6814 LONG BEACH BOULEVARD, LONG BEACH, CALIFORNIA 90807

Job: Dredged Material Study/Pinto Island

Investigator: R. Morrison/T. Boston

Date: 1/17/77

Rig: 4" bucket auger

Existing Elevation: _____

Well No: PI-G

Depth	Sample Location	Material	Description	Remarks
1		Sand	Fine	
2		Sand	Fine	
3		Sand	Fine	
4		Clay	Reddish	Very tight
5		Clay	Reddish	
6		Sand	Fine	
7		Sand	Fine	
8		Clay	Fine	
9		Clay	Water encountered	
10		Clay	Water encountered	
11		Clay	Water encountered	
12		Clay	Bottom of hole	
13				
14				
15				
16				
17				



Job: Dredged Material Study/Pinto Island

Investigator: R. Morrison/T. Boston

Date: 1/17/77

Rig: 4" bucket auger

Existing Elevation: 12-29

Well No: PI-H

Depth	Sample Location	Material	Description	Remarks
1		Sand	Fine sands	
2		Sand	Fine sands	
3		Sand	Fine sands	
4		Sand	Coarser sands	
5		Sand	Coarser sands	
6		Sand	Coarser sands	
7		Sand	Coarser sands	
8			Sand	Water encountered
9		Sand		
10			Bottom of hole	
11				
12				
13				
14				
15				
16				
17				



Job: Dredged Material Study/Pinto Island
 Investigator: R. Morrison/T. Boston
 Date: 1/17/77
 Rig: 4" bucket auger
 Existing Elevation: 12-29
 Well No: PI-1

Depth	Sample Location	Material	Description	Remarks
1		Sand	Fine sands	
2		Sand	Fine sands	
3		Sand	Medium grained	
4		Sand	Medium grained	
5		Sand	Fine sands	
6		Sand	Fine sands	
7		Sand	Water encountered	
8		Sand	Water encountered	
9		Sand	Water encountered	
10	—		Bottom of hole	
11				
12				
13				
14				
15				
16				
17				



SCS ENGINEERS

STEARNs, CONRAD AND SCHMIDT
CONSULTING ENGINEERS, INC.

TEL: 913/428-0044

6814 LONG BEACH BOULEVARD, LONG BEACH, CALIFORNIA 90807

Job: Dredged Material Study/Pinto Island

Investigator: R. Morrison/T. Boston

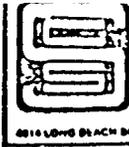
Date: 1/17/77

Rig: 4" bucket auger

Existing Elevation: 10-70

Well No: PI-J

Depth	Sample Location	Material	Description	Remarks
1		Sand	Fine sands	
2		Sand	Fine sands	
3		Sand	Fine sands	
4		Sand	Fine sands	
5		Sand	Fine sands	
6		Sand	Water encountered	
7		Sand		
8		Sand	Bottom of hole	
9				
10				
11				
12				
13				
14				
15				
16				
17				

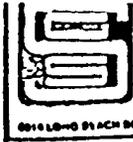
**SCS ENGINEERS**BIEANNS, CONRAD AND SCHMIDT
CONSULTING ENGINEERS, INC.

TEL: 913/428-0044

4814 LONG BEACH BOULEVARD, LONG BEACH, CALIFORNIA 90807

Job: Dredged Material Study/Pinto IslandInvestigator: R. Morrison/T. BostonDate: 8/1/77Rig: 6" cable toolExisting Elevation: 16.7Well No: PI-OPW

Depth	Sample Location	Material	Description	Remarks
1		Sand	Fine grained	
2		Sand	Fine grained	
3		Sand	Fine grained	
4		Sand	Fine grained	
5		Clay	Reddish lense	Tight
6		Clay		
7		Sand		
8		 Sand	Water encountered	
9		Sand		
10		Sand		
11		Sand	Water encountered	
12		Clay	Reddish lense	
13		Clay	Reddish lense	
14		Sand	Fine sands	
15		Sand		Well screen
16		Sand		Placed from
17		Sand		15'-20'



SCS ENGINEERS

STEARNS, COMRAD AND SCHMIDT
CONSULTING ENGINEERS, INC.

TEL: 812/730-0044

8010 LONG BEACH BOULEVARD, LONG BEACH, CALIFORNIA 90807

JOB: Dredged Material Study/Pinto Island

Investigator: R. Morrison/T. Boston

Date: 8/1/77

Rig: 16" cable tool

Existing Elevation: 17.80

Well No: PI-OMW

Depth	Sample Location	Material	Description	Remarks
1		Sand	Fine sands	
2			Fine sands	
3		Clay	Reddish	
4		Sand	Medium grained	
5		Sand	Medium grained	
6		Sand	Medium grained	
7		Sand	Medium grained	
8	▽	Sand	Medium grained	
9	—	Sand	Water encountered	
10		Sand	Water encountered	
11		Clay	Reddish	
12		Sand	Fine grained	
13		Sand	Fine grained	
14		Sand	Fine grained	
15		Sand	Fine grained	Well screen
16		Sand	Fine grained	Placed from
17		Sand	Fine grained	15'-20'

APPENDIX I: SOIL AND DREDGED MATERIAL
PHYSICAL AND CHEMICAL CHARACTERISTICS

TABLE 11

PHYSICAL CHARACTERISTICS OF DREGGED MATERIAL AND SOILS: GRAND HAVEN, MICHIGAN, SITE

	Particle Size Distribution			Texture	Permeability cm/sec	Moisture Equivalent %	Bulk Density gm/c.c.	Moisture Content %
	Sand %	Silt %	Clay %					
MA1	70	10	20	clay sand	1.2×10^{-6}	82	1.6	54
MA2	76	14	10	silty sand	6.7×10^{-6}	60	1.7	53
MA3	74	8	18	silty sand	3.9×10^{-6}	14	2.2	43
MA4	72	8	20	silty sand	1.0×10^{-6}	13	1.8	42
MB1	63	13	26	clay sand	1.8×10^{-6}	13	1.8	42
MB2	65	17	18	silty sand	1.3×10^{-6}	85	1.6	52
MB3	91	4	7	sand	3.6×10^{-6}	27	1.6	35
MB4	94	2	4	sand	1.6×10^{-4}	11	1.8	24
MC1	63	17	20	silty sand	8×10^{-6}	72	1.3	46
MC2	99	<1	<1	sand	5×10^{-3}	3	1.8	12
MD1	67	12	21	clay sand	6.6×10^{-6}	72	1.5	50
MD2	96	2	2	sand	4×10^{-4}	6	2.0	23
ME1	86	7	7	sand	2.4×10^{-3}	28	1.7	28

TABLE 11 (Concluded)

Sample Code	Particle Size Distribution			Texture	Permeability cm/sec	Moisture Equivalent %	Bulk Density gm/c.c.	Moisture Content %
	Sand %	Silt %	Clay %					
ME2	98	1	1	sand	5.2×10^{-3}	2	1.6	10
MF1	90	4	6	sand	3.0×10^{-3}	9	1.6	17
MF2	92	2	6	sand	4×10^{-5}	13	1.8	18
MF3	95	2	3	sand	2.8×10^{-5}	8	1.9	28
MF4	92	1	7	sand	1.1×10^{-4}	10	1.7	26
MG1	84	5	11	sand	7.8×10^{-5}	19	2.0	31
MG2	84	5	11	sand	6.2×10^{-5}	30	1.8	31
MG3	73	15	12	silty sand	2.4×10^{-6}	78	1.6	28
MG4	94	2	4	sand	6.6×10^{-4}	6	1.6	38
MH1	97	1	2	sand	8.9×10^{-4}	3	1.9	16
MH2	99	<1	<1	sand	6.1×10^{-4}	2	1.5	18
MI	99	<1	<1	sand	1.4×10^{-3}	3	1.6	14
MJ	97	1	2	sand	9.1×10^{-4}	7	1.7	10

TABLE 1

PHYSICAL CHARACTERISTICS OF DREDGED MATERIAL AND SOILS: SAYREVILLE, N.J., SITE

Sample Code	Particle Size Distribution			Texture	Permeability cm/sec	Moisture Equivalent %	Bulk Density gm/c.c.	Moisture Content %
	Sand %	Silt %	Clay %					
NJA1	72	10	18	silty sand	1.1×10^{-6}	76	1.2	49
NJA2	69	9	22	silty sand	2.8×10^{-6}	82	1.7	48
NJA3	75	9	16	silty sand	4.4×10^{-6}	56	1.6	38
NJA4	93	3	4	sand	1.1×10^{-5}	11	2.2	13
NJB1	64	10	26	clay sand	9.8×10^{-6}	78	1.9	48
NJB2	73	7	20	clay sand	3.6×10^{-6}	72	1.7	49
NJB3	68	9	23	clay sand	2.5×10^{-7}	83	1.8	52
NJB4	89	3	8	sand	3.2×10^{-6}	31	1.9	31
NJC1	60	11	29	clay sand	6.3×10^{-6}	61	1.7	45
NJC2	60	11	29	clay sand	4.5×10^{-6}	76	1.7	48
NJC3	89	4	7	sand	5.4×10^{-6}	49	1.7	39
NJC4	95	2	3	sand	1.1×10^{-5}	5	1.6	13
NJD1	67	8	25	clay sand	1.3×10^{-6}	83	1.3	48

TABLE 12 (Concluded)

Sample Code	Particle Size Distribution			Texture	Permeability cm/sec.	Moisture Equivalent %	Bulk Density gm/c.c.	Moisture Content %
	Sand %	Silt %	Clay %					
NJD2	77	6	17	silty sand	1.2×10^{-6}	57	1.6	27
NJD3	96	2	2	sand	2.1×10^{-5}	4	1.6	11
NJD4	97	1	2	sand	1.4×10^{-5}	4	2.1	11
NJE1	67	9	24	silty sand	3.1×10^{-6}	77	1.4	45
NJE2	63	11	26	silty sand	1.0×10^{-6}	66	1.8	53
NJF1	57	10	33	sandy clay	1.0×10^{-6}	78	1.3	41
NJF2	64	9	27	clay sand	3.2×10^{-7}	85	1.4	56
NJG1	71	7	22	clay sand	1.2×10^{-6}	85	1.3	37
NJG2	78	6	15	silty sand	2.0×10^{-6}	68	1.6	41
NJH1	62	11	27	clay sand	1.4×10^{-5}	45	1.6	45
NJH2	57	13	30	sandy clay	3.6×10^{-6}	87	1.3	43
NJI	97	1	2	clay sand	7.3×10^{-5}	5	1.7	49
NJJ	62	9	29	clay sand	4.5×10^{-5}	58	1.3	16

TABLE 13

PHYSICAL CHARACTERISTICS OF DREGGED MATERIAL AND SOILS: HOUSTON SITE

Sample Code	Particle Size Distribution			Texture	Permeability cm/sec	Moisture Equivalent %	Bulk Density gm/c.c.	Moisture Content %
	Sand %	Silt %	Clay %					
HA1	78	7	15	silty sand	8.8×10^{-7}	25	1.9	26
HA2	77	11	11	silty sand	9.2×10^{-7}	24	1.9	26
HA3	65	5	10	sand	7.7×10^{-7}	27	1.8	26
HA4	80	5	9	sand	9.3×10^{-8}	35	1.7	25
HB1	78	7	15	silty sand	8.9×10^{-5}	18	1.9	21
HB2	85	10	5	sand	1.5×10^{-6}	16	1.8	20
HB3	78	7	15	silty sand	9.1×10^{-8}	24	2.0	22
HB4	81	11	8	sand	1.2×10^{-7}	20	1.9	21
HC1	81	6	13	sand	5.3×10^{-7}	15	2.1	17
HC2	86	4	10	sand	6.0×10^{-6}	21	1.8	17
HC3	78	12	10	silty sand	5.2×10^{-8}	33	2.2	24
HC4	73	17	10	clay sand	2.1×10^{-8}	38	2.0	33

TABLE 13 (Concluded)

Sample Code	Particle Size Distribution			Texture	Permeability cm/sec	Moisture Equivalent %	Bulk Density gm/c.c.	Moisture Content %
	Sand %	Silt %	Clay %					
HD1	81	6	13	sand	3.5×10^{-5}	14	1.7	26
HD2	83	6	13	sand	2.9×10^{-5}	8	1.8	18
HD3	86	5	9	sand	1.7×10^{-6}	27	2.1	25
HD4	82	6	12	sand	2.7×10^{-5}	6	1.6	19
HE1	82	6	12	sand	2.9×10^{-5}	8	1.8	16
HE2	65	11	24	clay sand	1.3×10^{-6}	20	1.8	17
HF1	82	6	14	sand	2.1×10^{-4}	7	2.0	16
HF2	71	9	20	clay sand	2.9×10^{-6}	18	1.8	17
HG1	70	9	21	clay sand	2.2×10^{-6}	21	1.9	20
HG2	60	13	27	clay sand	4.2×10^{-6}	27	1.9	21
HH1	81	6	13	sand	3.6×10^{-6}	10	1.8	17
HH2	68	11	21	clay	1.5×10^{-6}	14	1.8	22
HI	86	5	9	sand	4.6×10^{-6}	22	2.0	18
HJ	68	10	22	clay sand	5.7×10^{-6}	21	2.0	18

TABLE 14

PHYSICAL CHARACTERISTICS OF DREDGED MATERIAL AND SOILS: PINTO ISLAND SITE

Sample Code	Particle Size Distribution			Texture	Permeability cm/sec	Moisture Equivalent %	Bulk Density gm/c.c.	Moisture Content %
	Sand %	Silt %	Clay %					
PA1	80	6	14	silty sand	2.8×10^{-6}	38	2.0	41
PA2	98	1	1	sand	2.4×10^{-4}	3	1.6	16
PA3	96	1	3	sand	2.1×10^{-6}	15	1.7	21
PA4	95	2	3	sand	8.2×10^{-5}	14	1.9	19
PB1	97	1	2	sand	7.2×10^{-5}	6	1.3	13
PB2	95	2	3	sand	3.2×10^{-6}	13	1.9	19
PB3	99	<1	<1	sand	3.0×10^{-4}	3	2.1	20
PB4	99	<1	<1	sand	1.4×10^{-4}	4	2.0	16
PC1	90	3	7	sand	2.1×10^{-6}	9	2.0	16
PC2	82	9	9	sand	3.4×10^{-6}	37	1.4	29
PC3	94	2	4	sand	8.6×10^{-7}	27	1.8	27
PC4	95	3	2	sand	1.2×10^{-5}	11	2.0	22
PD1	97	1	2	sand	8.1×10^{-5}	3	1.6	12
PD2	96	1	3	sand	7.1×10^{-5}	11	1.9	16
PD3	98	1	1	sand	6.6×10^{-5}	5	2.0	13
PD4	98	1	1	sand	6.5×10^{-5}	8	1.9	19

TABLE 14 (Concluded)

Sample Code	Particle Size Distribution			Texture	Permeability cm/sec	Moisture Equivalent %	Bulk Density gm/c.c.	Moisture Content %
	Sand %	Silt %	Clay %					
PE1	97	1	2	sand	1.8×10^{-5}	8	1.9	19
PE2	38	22	40	sandy clay	5.4×10^{-7}	47	1.6	30
PF1	96	2	2	sand	3.2×10^{-5}	6	1.9	14
PF2	96	1	3	sand	4.0×10^{-5}	3	2.1	16
PG1	97	1	2	sand	1.2×10^{-6}	10	1.8	14
PG2	92	4	4	sand	3.1×10^{-6}	34	1.9	19
PH1	97	1	2	sand	7.0×10^{-5}	4	1.4	16
PH2	96	2	2	sand	9.0×10^{-5}	6	1.6	12
PI	69	11	20	silty sand	8.0×10^{-5}	22	1.8	18
PJ	98	1	1	sand	3.6×10^{-5}	3	1.6	16

TABLE 15

CHEMICAL CHARACTERISTICS OF DREDGED MATERIAL AND SOILS: GRAND HAVEN, MICHIGAN, SITE

Sample Code	pH	EH mV	CEC meg/100gm	TOC %	NH ₃ -N mg/kg	Organic Nitrogen mg/kg	Total Kjeldahl Nitrogen mg/kg	Acid Soluble S ^m mg/kg	Total Phosphorus mg/kg	Oil & Grease mg/kg
MA1	6.4	232	84	6.2	ND	1512	1512	52	1148	3891
MA2	6.5	97	69	4.3	ND	918	918	94	272	2293
MA3	7.0	169	24	0.6	ND	271	271	7	4094	279
MA4	5.1	248	25	2.6	ND	418	418	3	962	240
MB1	7.3	252	71	4.7	ND	5241	5241	36	1029	2352
MB2	5.3	165	74	6.6	296	5185	5481	200	691	2423
MB3	8.0	-249	48	1.2	40	2306	2346	35	5078	4675
MB4	6.8	90	23	1.7	18	582	600	21	876	240
MC1	7.0	177	26	6.5	38	5770	5808	13	2028	2479
MC2	7.4	262	2	0.01	11	493	504	7	507	215
MD1	5.8	192	22	8.5	88	5058	5146	5	1024	122
MD2	6.8	190	25	0.4	ND	877	877	12	315	268
ME1	7.0	175	58	3.4	ND	2012	2012	33	694	1759
ME2	--	--	1	0.11	ND	592	592	18	600	420

TABLE 15 (Concluded)

Sample Code	pH	Eh mV	CEC meg/100gm	TOC %	NH ₃ -N mg/kg	Organic Nitrogen mg/kg	Total Kjeldahl Nitrogen mg/kg	Acid Soluble S ^m mg/kg	Total Phosphorus mg/kg	Oil & Grease mg/kg
MF1	7.4	107	10	1.3	ND	652	652	31	1260	349
MF2	6.9	254	8	0.38	ND	183	183	49	852	670
MF3	7.0	189	29	0.18	9	1537	1546	24	439	914
MF4	--	--	2	1.6	ND	403	403	17	852	353
MG1	4.7	255	13	5.2	ND	1166	1166	25	1396	972
MG2	6.8	290	39	11.3	ND	2147	2147	17	2041	944
MG3	7.0	161	32	3.7	ND	2917	2917	64	2317	1206
MG4	6.6	-100	49	6.4	ND	3821	3821	32	1014	481
MH1	7.2	253	4	0.13	ND	81	81	31	1724	237
MH2	4.6	181	16	1.2	ND	41	41	28	672	630
MI	--	--	2	0.61	16	144	160	19	405	456
MJ	6.8	185	1	0.23	ND	72	72	6	721	481

TABLE 16

CHEMICAL CHARACTERISTICS OF DREDGED MATERIAL AND SOILS: SAYREVILLE, N.J., SITE

Sample Code	pH	Eh mV	CEC meq/100gm	TOC %	NH ₃ -N mg/kg	Organic Nitrogen mg/kg	Total Kjeldahl Nitrogen mg/kg	Acid Soluble S ^m mg/kg	Total Phosphorus mg/kg	Oil & Grease mg/kg
NJA1	--	--	73	1.8	91	4820	4911	99	2917	2200
NJA2	--	256	66	1.6	275	2480	2755	129	2366	2217
NJA3	7.1	221	42	0.58	223	1660	1883	326	395	1617
NJA4	5.8	284	11	0.34	64	508	572	31	1212	415
NJB1	6.7	247	76	1.7	12	4420	4432	276	1778	5460
NJB2	6.4	172	60	2.8	125	3680	3805	77	182	2910
NJB3	7.3	37	84	2.0	125	2660	2785	144	1802	2982
NJB4	8.0	-287	21	0.46	9	--	--	536	64	1909
NJC1	7.6	-90	52	1.7	96	1960	2056	33	1236	355
NJC2	6.9	-207	77	2.7	38	2730	2768	1362	1024	4085
NJC3	7.2	-258	24	0.18	ND	11	11	49	1371	288
NJC4	6.9	-360	--	0.22	ND	253	253	99	314	808
NJD1	6.4	-218	73	1.2	332	3400	3732	445	2144	2999
NJD2	7.3	110	29	0.22	221	2350	2571	109	1030	1553

TABLE 16 (Concluded)

Sample Code	pH	Eh mV	CCr. meq/100gm	TOC %	NH ₃ -N mg/kg	Organic Nitrogen mg/kg	Total Kjeldahl Nitrogen mg/kg	Acid Soluble S ^m mg/kg	Total Phosphorus mg/kg	O11 & Grease mg/kg
NJD3	5.7	-356	7	0.02	9	140	149	177	1675	247
NJD4	6.4	408	--	0.02	21	113	135	23	1235	278
NJE1	6.0	-167	66	1.7	132	2100	2232	2357	413	400
NJE2	7.2	-158	53	1.5	85	1103	1188	1149	202	3180
NJF1	6.1	-250	9	1.7	106	3300	3406	136	1942	2605
NJF2	--	--	43	1.9	291	3000	3291	30	237	4811
NJG1	6.8	166	60	2.2	258	3260	3518	276	2164	5252
NJG2	6.5	-152	61	2.0	164	1380	1444	293	2810	4247
NJH1	7.5	346	30	2.4	--	--	3800	40	2036	2751
NJH2	6.4	-260	35	--	--	--	1140	169	3493	1313
NJI	7.3	350	6	0.48	33	378	411	15	1580	224
NJJ	--	--	61	1.4	67	7800	7867	67	1642	2961

TABLE 17
 CHEMICAL CHARACTERISTICS OF DREDGED MATERIAL AND SOILS: HOUSTON SITE

Sample Code	pH	Eh mV	CEC meq/100gm	TOC %	NH ₃ -N mg/kg	Organic Nitrogen mg/kg	Total Kjeldahl Nitrogen mg/kg	Acid Soluble S ²⁻ mg/kg	Total Phosphorus mg/kg	Oil & Grease mg/kg
HA1	6.7	177	2.4	0.75	36	833	869	18	691	3778
HA2	7.1	183	6.2	0.47	ND	733	733	267	2765	246
HA3	7.3	-120	1.9	0.31	31	345	356	12	534	4505
HA4	6.7	-60	2.2	0.2	53	421	474	44	117	1557
HB1	6.5	-76	2.8	0.2	ND	104	104	18	428	2131
HB2	6.4	-275	4.4	0.1	5	783	788	23	2289	966
HB3	6.9	128	9.5	0.03	14	133	147	90	2223	169
HB4	6.6	93	17	0.01	ND	643	643	60	2976	180
HC1	6.7	-253	43	0.04	ND	280	280	53	3142	2431
HC2	6.1	202	38	0.08	8	245	253	44	1594	451
HC3	6.6	107	20	0.14	12	149	171	155	1170	526
HC4	6.7	53	19	0.1	37	513	550	457	1234	524
HD1	6.6	117	36	0.2	ND	426	426	22	1070	2645
HD2	6.8	200	1.6	0.6	-	545	545	23	1060	652

TABLE 17 (Concluded)

Sample Code	pH	Eh mV	CEC meq/100gm	TOC %	NH ₃ -N mg/kg	Organic Nitrogen mg/kg	Total Kjeldahl Nitrogen mg/kg	Acid Soluble S ²⁻ mg/kg	Total Phosphorus mg/kg	Oil & Grease mg/kg
ND3	6.7	34	22	0.4	-	299	299	40	431	959
ND4	7.1	112	4.8	0.2	ND	80	80	79	379	664
NE1	7.2	89	11	0.3	ND	173	173	21	568	1202
NE2	6.8	109	11	0.78	ND	58	58	37	850	862
NF1	6.7	78	14	0.19	27	151	178	121	2400	948
NF2	6.5	- 55	13	0.29	ND	526	526	48	617	649
NG1	6.7	-171	12	0.13	ND	933	933	73	1908	1165
NG2	6.8	125	16	1.1	ND	117	117	22	817	1065
NH1	6.3	65	8.0	0.11	36	156	192	166	487	407
NH2	6.5	-254	14	0.14	1.7	207	224	41	596	173
NI	6.6	63	21	0.12	ND	268	268	29	1501	245
NJ	6.4	- 68	11	0.1	ND	51	51	34	462	313

TABLE 18
 CHEMICAL CHARACTERISTICS OF DREDGED MATERIAL AND SOIL: PINTO ISLAND SITE

Sample Code	pH	Eh mV	CFC meq/100gm	TOC %	NH ₃ -N mg/kg	Organic Nitrogen mg/kg	Total Kjeldahl Nitrogen mg/kg	Acid Soluble S ^m mg/kg	Total Phosphorus mg/kg	O11 & Grease mg/kg
PA1	6.1	-177	51	0.55	ND	963	963	8	1080	345
PA2	7.2	-232	0.34	0.65	ND	80	80	19	374	520
PA3	6.9	-220	0.75	0.44	17	174	191	19	404	2047
PA4	6.6	-172	11	0.14	ND	259	259	13	706	170
PB1	7.0	251	0.58	0.34	ND	87	87	24	502	71
PB2	5.2	353	0.76	0.87	70	343	413	50	421	281
PB3	6.3	-250	2.1	0.69	ND	59	59	34	744	168
PB4	6.7	-179	0.31	0.66	ND	79	79	23	976	248
PC1	5.1	340	3.7	2.71	ND	106	106	51	498	464
PC2	7.1	-149	45	0.83	52	556	608	78	7200	202
PC3	7.1	-165	22	0.47	20	408	428	44	351	1464
PC4	7.2	- 14	0.82	0.22	ND	221	221	20	4370	496
PD1	5.8	250	2.2	0.44	ND	79	79	5	319	478

TABLE IB (Concluded)

Sample Code	pH	Eh mV	CEC meq/100gm	TOC %	NH ₃ -N mg/kg	Organic Nitrogen mg/kg	Total Kjeldahl Nitrogen mg/kg	Acid Soluble S ²⁻ mg/kg	Total Phosphorus mg/kg	Oil & Grease mg/kg
PD2	6.8	230	0.54	1.79	ND	173	173	7	385	213
PD3	6.9	-258	2.7	0.83	ND	38	38	12	4020	1065
PD4	7.0	-189	1.7	0.46	35	124	159	10	1127	585
PE1	7.2	120	29	0.25	ND	130	130	12	542	423
PE2	6.9	- 82	27	0.85	51	471	522	147	938	925
PF1	7.6	220	5.4	0.59	ND	80	80	6	520	380
PF2	7.2	220	1.8	0.83	63	225	288	2	465	252
PG1	7.1	300	7.7	0.79	ND	112	112	8	503	340
PG2	6.4	29	0.65	0.62	62	250	312	6	455	734
PH1	6.5	274	0.45	0.68	ND	91	91	4	400	471
PH2	6.9	199	2.6	0.10	ND	103	103	7	382	179
PI	6.5	368	5.5	0.08	ND	362	362	9	409	290
PJ	7.6	214	1.8	0.63	ND	134	134	9	555	210

APPENDIX J: SOIL AND DREDGED MATERIAL
PESTICIDE AND METALS ANALYSES

TABLE 31
SOIL AND DREDGED MATERIAL PESTICIDES: GRAND HAVEN, MICHIGAN, SITE

(all units are mg/kg)

Sample Code	op' DDE	pp' DDE	op' DDD	pp' DDD	op' DDT	pp' DDT	Total DDD	PCB 1242	PCB 1254	PCB 1260	Total PCB	Dieldrin
MA1	9.5	27.0	8.0	16.5	--	--	61.0	0.11	0.16	0.031	0.30	0.09
MA2	14.3	23.0	4.0	10.0	3.0	4.0	58.0	0.05	0.02	0.002	0.072	3.3
MA3	1.2	4.0	1.3	2.1	4.0	1.3	13.9	0.002	0.03	0.006	0.038	2.0
MA4	--	--	--	--	--	--	--	--	--	--	--	2.5
MB1	13.0	22.1	7.3	12.2	7.0	8.3	69.9	0.05	0.14	0.042	0.23	1.2
MB2	9.3	24.0	4.1	10.3	6.0	4.1	57.9	0.07	0.14	0.041	0.251	0.9
MB3	4.2	14.6	1.4	8.0	4.2	4.0	36.4	0.04	0.08	0.02	0.14	0.9
MB4	--	--	--	--	--	--	--	--	--	--	--	1.8
MC1	2.3	3.0	2.3	3.0	9.0	11.5	20.1	0.017	0.13	0.04	0.18	1.6
MC2	0.5	0.8	0.7	0.5	0.5	2.0	4.0	--	0.006	0.002	0.008	1.0
MD1	10.0	19.0	3.2	3.2	6.4	12.2	54.0	0.023	0.13	0.04	0.193	3.7
MD2	3.0	4.0	0.5	0.5	0.5	0.8	9.3	0.007	0.03	0.002	0.039	2.0
ME1	6.0	36.0	9.0	2.1	3.0	4.2	60.3	0.008	0.06	0.02	0.088	0.5
ME2	4.0	26.0	--	--	--	--	30.0	0.013	0.03	0.008	0.051	0.4
MF1	1.5	5.0	0.4	2.0	.25	4.0	15.4	--	--	--	--	0.4
MF2	2.0	5.0	--	--	--	--	7.0	0.01	0.02	0.006	0.046	0.4
MF3	0.9	6.0	0.3	0.8	1.2	2.0	11.2	0.01	0.04	0.01	0.06	0.5
MG1	1.2	13.0	1.2	4.0	5.0	7.3	31.7	0.02	0.08	0.02	0.12	0.6
MG2	5.0	8.0	1.0	2.3	4.0	6.0	26.3	0.014	0.03	0.01	0.054	0.5
MG3	11.4	112.0	1.0	3.5	4.1	11.0	143.0	0.01	0.2	0.05	0.26	2.4
MG4	10.0	18.0	3.0	6.0	4.0	3.0	44.0	0.05	0.1	0.03	0.18	0.5
MH1	0.8	3.0	0.2	0.4	0.2	1.1	5.7	0.005	0.002	0.0002	0.0072	0.6
MI	1.0	5.0	1.4	7.0	0.7	1.2	16.3	0.02	0.1	0.01	0.13	0.2
MJ	0.5	3.0	0.7	4.0	0.4	0.8	5.8	0.02	0.1	0.01	0.13	0.2

TABLE J2
 SOIL AND DREDGED MATERIAL PESTICIDES: SAYREVILLE, NEW JERSEY, SITE
 (all units are mg/kg)

Sample Code	op' DDE	pp' DDE	op' DDD	pp' DDD	op' DDT	pp' DDT	Total DDD	PCB 1242	PCB 1254	PCB 1260	TOTAL PCB	Dieldrin
NJA1	13.7	32.0	8.0	8.0	14.0	6.2	81.9	0.10	0.11	0.011	0.22	2.3
NJA2	2.3	4.0	5.0	5.7	8.5	2.3	27.8	0.05	0.07	0.007	0.127	1.4
NJA3	2.1	2.9	3.3	5.4	2.1	0.9	15.89	0.01	0.02	0.002	0.032	1.6
NJA4	0.8	0.09	0.11	0.11	0.56	0.22	1.89	--	--	--	--	1.3
NJB1	23.0	44.0	34.0	68.0	23.0	13.0	205.0	0.22	0.12	0.011	0.451	1.2
NJB2	39.0	67.0	40.0	67.0	12.0	5.4	230.4	0.36	0.14	0.01	0.51	4.3
NJB3	10.4	15.1	5.7	8.8	1.7	0.8	42.5	0.08	0.06	0.006	0.145	2.0
NJB4	6.4	1.4	0.5	1.1	6.2	4.0	19.6	0.04	0.08	0.008	0.128	1.8
NJC1	10.0	12.0	3.0	6.0	2.6	1.2	34.8	0.7	0.6	0.06	1.36	1.8
NJC2	10.0	15.0	4.0	7.4	6.3	4.5	47.2	1.0	1.1	0.11	2.21	2.1
NJC3	8.5	12.7	1.6	3.0	1.6	1.1	28.5	0.2	0.23	0.02	0.45	1.5
NJC4	--	--	--	--	--	--	--	--	--	--	--	--
NJD1	37.0	77.0	12.2	27.2	15.0	10.0	178.4	0.22	0.2	0.05	0.47	5.0
NJD2	43.0	87.0	24.0	47.0	24.0	17.0	242.0	0.34	0.52	0.05	0.91	2.4
NJD3	3.1	2.1	3.5	4.1	2.2	3.8	18.8	0.01	0.01	0.002	0.022	1.5
NJD4	--	--	--	--	--	--	--	--	--	--	--	--
NJE1	105.0	217.0	77.0	93.0	79.0	56.0	627.0	0.3	0.2	0.02	0.52	8.1
NJE2	12.4	20.0	4.0	7.1	4.1	3.0	50.6	0.01	0.02	0.004	0.034	0.3
NJF1	61.0	72.0	19.0	39.0	12.0	13.0	216.0	0.16	0.78	0.078	1.018	2.3
NJF2	7.4	8.8	6.1	5.2	6.1	9.2	42.2	0.03	0.04	0.004	0.074	1.4
NJG1	80.0	122.0	31.0	63.0	14.0	27.0	337.0	0.06	0.1	0.03	0.19	2.0
NJG2	16.0	24.0	6.3	10.0	5.0	8.0	69.3	0.01	0.03	0.01	0.05	3.4
NJH1	49.0	50.0	14.0	21.0	5.8	1.1	140.9	0.26	0.35	0.03	0.64	2.4
NJH2	24.0	36.0	7.3	4.6	92.2	--	--	--	--	--	--	1.8
NJI	6.0	4.0	4.2	5.3	4.5	6.2	30.0	0.01	0.01	0.001	0.021	0.7
NJJ	0.78	0.08	1.7	2.8	0.78	0.2	6.34	--	--	--	--	0.2

TABLE J3
 CHLORINATED PESTICIDES IN SOIL AND DREDGED MATERIALS: WYOMING, TEXAS, SITE
 (all units are mg/kg)

Sample Code	op' DDE	pp' DDE	op' DDD	pp' DDD	op' DDT	pp' DDT	Total DDD	PCB 1242	PCB 1254	PCB 1260	Total PCB	Dieldrin
HA1	78.0	198.0	246	36.2	249	44.0	851.2	1.5	1.06	0.32	2.88	3.5
HA2	--	--	--	--	--	--	--	--	--	--	--	--
HA3	23.0	36.2	2.1	2.0	5.0	2.0	70.3	0.22	0.1	0.05	0.37	4.0
HA4	8.2	14.2	13.4	3.0	11.0	4.0	53.8	0.04	0.01	0.001	0.051	0.8
HB1	--	--	--	--	--	--	--	--	--	--	--	--
HB2	4.0	8.0	1.5	1.8	1.1	2.2	18.6	0.01	0.02	0.008	0.038	0.3
HB3	7.1	10.0	1.0	2.0	2.5	2.0	24.6	0.01	0.03	0.01	0.05	1.4
HB4	46.0	72.0	8.0	5.2	10.0	5.0	146.2	0.2	0.1	0.03	0.33	4.2
HC1	1.1	7.0	0.5	2.2	0.4	1.2	11.9	0.02	--	--	0.02	0.4
HC2	6.0	24.0	0.2	0.5	0.1	0.4	31.2	0.01	0.04	0.01	0.06	0.2
HC3	5.4	7.0	4.3	7.0	5.1	4.0	32.8	0.05	0.04	0.01	0.10	0.2
HC4	17.0	21.0	6.2	3.0	8.0	3.1	58.3	0.14	0.07	0.02	0.23	2.9
HD1	3.0	4.7	1.3	2.2	1.2	2.8	15.2	--	0.01	0.002	0.012	0.4
HD2	2.0	5.0	0.4	0.8	0.3	0.8	9.3	--	0.01	0.002	0.012	0.3
HD3	--	--	--	--	--	--	--	--	--	--	--	--
HD4	--	--	--	--	--	--	--	--	--	--	--	--
HE1	--	--	--	--	--	--	--	--	--	--	--	--
HE2	--	--	--	--	--	--	--	--	--	--	--	--
HF1	--	--	--	--	--	--	--	--	--	--	--	--
HF2	--	--	--	--	--	--	--	--	--	--	--	--
HG1	--	--	--	--	--	--	--	--	--	--	--	--
HG2	--	--	--	--	--	--	--	--	--	--	--	--
HH1	31.0	57.4	14.0	4.0	8.0	5.0	119.4	0.23	0.2	0.05	0.48	0.5
HH2	5.3	7.2	6.2	7.4	3.4	6.2	35.7	0.08	0.05	0.005	0.135	0.1
HI	--	--	--	--	--	--	--	--	--	--	--	--
HJ	--	--	--	--	--	--	--	--	--	--	--	--

TABLE J4
 CHLORINATED PESTICIDES IN SOIL AND DREDGED MATERIAL: PINTO ISLAND, ALABAMA, SITE
 (all units are mg/kg)

Sample Code	op' DDE	pp' DDE	op' DDD	pp' DDD	op' DDT	pp' DDT	Total DDD	PCB 1242	PCB 1254	PCB 1260	Total PCB	Dieldrin
PA1	8.0	11.0	2.0	5.1	1.4	3.0	30.9	0.03	0.7	0.2	0.93	--
PA2	6.0	101.0	3.0	4.0	3.0	2.0	119.0	0.01	0.012	0.004	0.026	--
PA3	5.0	7.0	0.5	3.0	2.0	4.0	21.5	0.005	0.007	0.002	0.014	--
PA4	6.0	9.0	2.0	4.0	2.3	4.0	27.3	0.01	0.02	0.005	0.035	--
PB1	3.0	7.1	0.9	3.6	3.1	2.3	39.8	--	0.02	0.002	0.022	2.2
PB2	6.3	7.3	0.6	3.1	2.1	2.1	21.5	0.015	0.04	0.004	0.059	1.8
PB3	2.0	5.6	--	--	0.5	4.0	12.1	--	0.03	0.003	0.033	2.0
PB4	1.4	3.0	--	1.4	--	4.2	10.0	0.01	0.01	0.001	0.021	1.2
PC1	5.0	6.0	5.0	14.0	3.0	14.0	47.0	--	0.14	0.014	0.154	0.43
PC2	3.2	7.0	2.3	6.7	2.3	5.0	26.5	--	0.01	0.001	0.011	0.41
PC3	4.0	9.0	5.0	12.0	4.0	4.0	28.0	--	0.05	0.013	0.063	2.2
PC4	3.0	9.0	2.3	4.7	3.3	2.4	24.7	--	0.08	0.02	0.10	2.6
PD1	17.3	20.0	7.3	24.2	3.2	5.0	57.02	0.02	0.24	0.07	0.33	0.4
PD2	77.5	260.0	--	--	37.0	138.0	512.5	0.9	1.4	0.4	2.7	0.2
PD3	2.2	3.6	0.4	1.8	1.4	1.2	10.6	0.006	0.012	0.001	0.019	0.2
PD4	3.0	6.4	0.6	0.8	0.2	0.6	11.6	--	0.02	0.007	0.027	0.4
PE1	1.7	4.3	--	--	--	--	6.0	0.02	0.002	0.022	--	--
PE2	19.0	21.0	1.6	4.0	1.1	23.0	69.7	0.006	0.012	0.001	0.012	--
PF1	0.7	0.9	--	--	--	--	1.6	--	0.02	0.002	0.022	--
PF2	--	--	--	--	--	--	--	--	--	--	--	--
PG1	--	1.4	--	--	--	--	1.4	--	--	--	--	--
PG2	--	4.4	--	--	--	--	4.4	--	--	--	--	--
PH1	--	1.4	--	--	--	--	1.4	--	0.022	0.002	0.024	--
PH2	--	1.4	--	--	--	--	1.4	--	--	--	--	--
P1	3.0	4.2	0.6	--	0.5	1.5	9.8	--	--	--	--	0.6
PJ	--	0.8	--	--	--	--	0.8	--	--	--	--	0.4

SOIL AND DRILLED MATERIAL METALS - GRAND HAVEN, MICHIGAN, SITE (ALL units are mg/kg)

Sample Code	K			Mg			Mn			Ni		
	Total	H ₂ O Soluble	Exchangeable	Total	H ₂ O Soluble	Exchangeable	Total	H ₂ O Soluble	Exchangeable	Total	H ₂ O Soluble	Exchangeable
MA1	5157	72.70	96.94	12480	157	300	1345	12.602	124.81	151.6	.52	2.06
MA2	--	40.09	120.27	--	120	231	--	.38	34.07	--	.24	4.09
MA3	9618	22.05	38.59	18453	16	91	318	.55	17.64	33.67	.066	.617
MA4	8934	21.65	36.08	17570	36	102	315	.36	18.04	17.4	.05	.36
MB1	--	35.23	96.88	--	123	351	--	.405	26.42	--	.23	2.09
MB2	11939	37.19	74.39	7285	92	262	631	1.64	24.79	70.8	.217	1.34
MB3	9813	20.27	74.33	5547	47	228	356	.304	8.108	50	.14	.959
MB4	16125	20.78	24.94	4097	6	62	184	.17	4.98	25.5	.07	.075
MC1	9481	67.56	185.79	11237	202	260	650	3.55	7.64	188	.37	3.34
MC2	7970	3.13	18.771	1908	37	61	65.7	.30	2.81	4.49	.087	--
MD1	10098	49.41	148.23	13090	--	370	610	.33	4.28	175	.33	2.39
MD2	6029	2.78	11.15	3542	22	61	105	.10	2.50	9.57	.027	.256
ME1	11260	11.89	41.62	7677	59	152	358	.26	2.85	70.8	.101	.945
ME2	8682	7.95	7.95	2224	11	20	75.4	.08	1.90	3.28	.035	.13
MF1	7259	3.735	18.67	3787	19	27	141	.448	4.015	22.5	.084	.877
MF2	--	.803	8.03	--	17	44	--	1.003	4.97	--	.072	1.55
MF3	9724	12.34	4.112	5176	7	72	176	.35	20.15	54.9	.082	.082
MF4	6365	--	--	2765	--	--	79.8	--	--	3.76	--	--
MG1	8178	17.48	40.79	3770	34	138	155	.59	3.26	18.3	.14	1.212
MG2	7352	6.735	20.205	8627	67	98	364	.35	4.17	72	.13	1.30
MG3	15712	--	--	13159	--	--	342	--	--	171	--	--
MG4	5582	44.33	33.25	1374	77	209	200	2.925	31.03	11.6	.12	.155
MI	6821	4.724	4.724	297	7	11	20.4	.089	1.09	2.59	.061	.014
MJ	8224	1.235	6.18	193	2	8	25.5	.065	.37	1.53	.06	.59

TABLE 10 (Continued)

Sample Code	Ca			Cd			Cu			Fe		
	Total	Exchangeable	H ₂ O Soluble	Total	Exchangeable	H ₂ O Soluble	Total	Exchangeable	H ₂ O Soluble	Total	Exchangeable	H ₂ O Soluble
MA1	58171	399.9	872	123	0.24	.508	131	.278	.072	24960	.666	0.24
MA2	--	300.7	1403	--	<.020	1.62	--	.06	1.042	--	.521	0.8
MA3	45323	99.3	380	1.924	0.22	.297	27.7	.022	.25	11721	.231	0.25
MA4	39250	64.9	498	3.454	.050	.34	22.6	.05	.75	12508	.548	0.11
MB1	--	281.9	669	--	<.008	1.215	--	0.26	1.101	--	.246	0.01
MB2	23373	161.2	471	30.2	<.006	.874	120	.018	.25	16695	.241	0.02
MB3	40106	175.7	514	3.13	0.13	.486	50	.047	.69	12800	.371	0.04
MB4	20134	79.0	341	1.48	<.004	.049	11.3	.09	.004	6537	3.32	0.11
MC1	66194	489.8	1216	19.58	<.017	2.63	175.6	.152	3.665	22825	1.06	0.15
MC2	4041	131.4	425	1.63	<.006	.732	3.42	.018	.275	3368	.194	0.02
MD1	61617	278.8	1186	5.14	0.16	2.22	149.6	.23	2.79	20570	1.25	0.4
MD2	--	94.7	368	1.81	<.005	.3	6.78	.016	0.89	4898	.200	0.06
ME1	19704	172.4	440	4.09	.006	1.52	66.5	.07	1.106	11942	2.97	0.01
ME2	4287	39.7	298	0.11	.004	.05	2.06	.063	.024	2984	.353	0.001
MF1	14623	130.7	616	4.42	.018	1.008	24.2	.046	.96	5260	.803	--
MF2	--	112.4	498	--	.008	.722	--	.008	.008	--	.233	--
MF3	18115	41.1	255	5.57	.004	.037	26.7	.016	.43	7058	2.47	--
MF4	4643	--	--	0.10	--	--	--	--	--	3130	--	--
MG1	11692	163.2	420	1.73	.006	1.34	10.9	.105	.536	4472	--	0.03
MG2	28057	195.3	458	0.3	.007	.72	31.5	.013	.188	9753	--	0.01
MG3	46056	--	--	5.4	--	--	149	--	--	14730	--	--
MG4	5067	199.5	798	4.7	.011	.055	11.2	.022	.011	4294	--	0.25
MI	645	37.8	142	0.11	.014	.217	1.76	.014	.005	1650	4.72	0.02
MJ	273	6.2	37	0.40	.006	.108	1.42	.052	.003	1134	.259	0.005

Table 1. A. (Cont'd.)

Sample Code	Pb			Na			Zn			Hg		
	Total	H ₂ O Soluble	Exchangeable	Total	H ₂ O Soluble	Exchangeable	Total	H ₂ O Soluble	Exchangeable	Total	H ₂ O Soluble	Exchangeable
PA1	253.7	.024	.424	4332	302.95	96.94	434	.48	7.51	0.12	--	--
PA2	--	.02	.301	--	400.92	60.14	--	.16	24.51	0.43	--	--
PA3	10.8	.005	.083	6011	27.57	38.59	73.3	.055	4.63	0.29	--	--
PA4	8.64	.007	.014	5658	368.02	72.16	53.6	.064	1.58	0.13	--	--
PB1	60	.009	.097	--	132.12	52.85	--	.105	8.54	0.80	--	--
PB2	109	.006	.062	4553	92.96	49.59	426	.105	6.82	1.00	--	--
PB3	94.6	.006	.101	4978	67.57	27.03	171	.189	4.73	0.42	--	--
PB4	14.8	.004	.008	5665	66.50	20.78	30.5	0.45	.457	0.05	--	--
PC1	139	.017	.068	3951	506.7	33.78	488	.24	18.58	1.46	--	--
PC2	4.21	.006	.025	4210	12.51	6.257	12.9	.075	5.88	0.01	--	--
PD1	113	.016	.066	4395	115.29	296.46	482	.165	13.505	0.94	--	--
PE1	70.8	.006	.018	4436	35.676	17.84	184	.05	3.63	0.48	--	--
PE2	3.80	.004	0.20	3798	39.74	3.974	1.63	.26	.397	--	--	--
PF1	11.3	.009	.140	4103	18.678	9.339	72.6	.093	4.015	0.03	--	--
PF2	--	.016	.064	--	16.06	6.02	--	.056	5.29	0.25	--	--
PF3	20.0	.004	.004	4313	16.45	4.112	145	.107	.74	0.40	--	--
PF4	3.68	--	--	3652	--	--	3.65	--	--	--	--	--
PG1	11.4	.0116	.070	4472	46.62	34.97	103	.22	7.57	0.16	--	--
PG2	16.8	.0067	.020	4651	74.08	20.205	109	.107	3.50	0.41	--	--
PG3	21.6	--	--	4419	--	--	569	--	--	0.88	--	--
PG4	14.2	.011	.122	2748	88.66	22.17	50.7	.775	1.44	0.15	--	--
PH	8.23	.006	.019	2751	9.45	2.36	0.17	.137	.4724	--	--	--
PJ	2.84	.092	.012	2155	6.18	2.32	0.11	.154	.556	--	--	--

SOIL AND BREACHED MATERIAL METALS - SAYREVILLE, NEW JERSEY, SITE
(all units are mg/kg)

Sample Code	Ca			Cd			Cu			Fe		
	Total	H ₂ O Soluble	Exchangeable	Total	H ₂ O Soluble	Exchangeable	Total	H ₂ O Soluble	Exchangeable	Total	H ₂ O Soluble	Exchangeable
NJA1	1479	91	400	74	0.061	0.27	402	0.264	9.66	54360	0.24	0.05
AJA2	1175	133	236	76	0.011	0.29	262	0.103	1.22	51123	4.11	0.19
NJA3	--	152	390	131	0.010	0.18	166	0.032	0.065	46086	23.8	0.26
NJA4	372	61	20	93	0.051	0.31	66	0.579	1.94	21937	0.12	0.54
NJB1	1187	113	328	7	0.012	1.31	399	0.082	17.0	55938	0.34	7.7
NJB2	--	67	692	4	0.202	0.32	346	0.606	0.534	54691	32.0	125
NJB3	1260	217	831	7	0.014	0.85	321	0.099	0.079	38484	475	30
NJB4	--	118	310	5	0.003	0.03	113	0.015	0.005	83344	320	125
NJC1	1817	108	311	26	0.036	6.61	416	0.107	0.138	53250	22.8	0.22
NJC2	--	123	660	--	0.046	0.25	--	0.260	0.015	--	464	40
NJC3	--	122	520	6	0.023	0.34	97	0.020	0.033	163200	567	25
NJC4	--	38	154	2	0.003	0.23	29	0.020	0.705	03184	--	0.009
NJD1	1894	158	621	78	0.013	0.52	245	0.04	0.026	32407	55.1	4
NJD2	879	110	281	5	0.031	0.15	238	0.036	0.018	50726	80.7	33
NJD3	328	39	208	1	0.011	0.084	54	0.022	1.58	19062	0.02	0.02
NJD4	375	--	--	2	--	--	80	--	--	31608	--	--
NJE1	--	676	590	1	0.078	0.05	105	0.93	0.015	34544	161	66
NJE2	--	86	324	2	0.015	0.02	75	0.03	0.007	54536	17.7	0.30
NJF1	1140	38	385	8	0.039	0.58	311	0.65	0.15	66079	34.6	12
NJF2	706	9	42	4	0.042	0.55	125	1.02	3.01	69538	91.8	0.45
NJG1	1208	250	138	9	0.444	--	193	10.1	6.4	12651	3.94	0.08
NJG2	1173	216	--	8	0.010	0.95	174	0.063	--	51051	54.03	--
NJH1	629	68	--	7	0.073	--	151	1.02	--	56730	0.07	--
NJH2	815	36	312	2	0.012	0.21	64	0.12	0.18	41265	25.23	17
NJI	90	1	2	0.3	0.020	0.03	6.34	0.14	0.005	4335	2.5	0.10
NJJ	--	35	35	--	0.230	0.23	--	283	0.194	--	3182	0.45

b1

TABLE J6 (Continued)

Sample Code	Pb			Na			Zn			Hg		
	Total	H ₂ O Soluble	Exchangeable	Total	H ₂ O Soluble	Exchangeable	Total	H ₂ O Soluble	Exchangeable	Total	H ₂ O Soluble	Exchangeable
NJA1	279	0.01	0.20	11050	4017	1586	382	0.244	9.0	3.3	--	--
NJA2	278	0.01	0.08	11154	4416	1047	355	0.308	23	3.8	--	--
NJA3	121	0.01	6.13	9217	3255	607	293	0.477	15	4.8	--	--
NJA4	35	0.006	0.05	3720	808	13	159	10.6	1.41	1.3	--	--
NJB1	240	0.01	0.64	15103	6254	2336	445	0.106	21.2	3.8	--	--
NJB2	270	0.06	0.32	10938	4474	1097	219	0.548	2.74	3.9	--	--
NJB3	290	0.02	0.24	10096	5940	1188	443	0.455	7.92	3.9	--	--
NJB4	63	0.006	0.06	3646	2400	500	182	0.125	0.60	1.3	--	--
NJC1	186	0.01	0.16	11538	4015	1102	402	0.35	4.31	2.8	--	--
NJC2	--	0.09	2.08	--	6035	1145	--	0.216	30.0	4.0	--	--
NJC3	68	0.03	0.14	3528	2717	679	345	0.135	11.0	4.0	--	--
NJC4	85	0.003	0.03	3403	773	145	89	0.029	0.714	0.6	--	--
NJD1	182	0.08	0.25	9074	5155	1057	295	0.502	13.0	3.9	--	--
NJD2	220	0.006	0.04	7960	2629	611	200	0.734	0.018	3.7	--	--
NJD3	31	0.005	0.04	3071	450	161	60	0.095	1.5	0.2	--	--
NJD4	7	--	--	3266	--	--	69	0.03	--	0.1	--	--
NJE1	172	0.03	0.02	10082	2098	357	114	5.69	15.5	4.00	--	--
NJE2	73	0.01	0.10	11504	3094	840	162	0.15	0.007	6.7	--	--
NJF1	288	0.25	0.19	7625	4236	808	357	0.404	72.0	4.2	--	--
NJF2	319	0.03	0.14	5762	141	56	215	0.522	28.0	4.7	--	--
NJG1	175	0.009	0.16	9087	838	197	340	86	20	4.4	--	--
NJG2	240	0.41	--	5364	1671	--	369	0.196	32.0	4.4	--	--
NJH1	238	0.01	--	5200	437	116	235	7.7	14.5	0.05	--	--
NJH2	88	0.06	0.10	7840	1520	696	104	0.106	8.89	0.8	--	--
NJI	65	0.008	0.10	882	50	5	23	12.8	0.015	0.08	--	--
NJJ	--	0.08	0.26	--	1414	460	--	36.6	--	0.3	--	--

TABLE 1 (Continued)

Sample Code	K			M ₁			M ₂			M ₃		
	Total	H ₂ O Soluble	Exchangeable	Total	H ₂ O Soluble	Exchangeable	Total	H ₂ O Soluble	Exchangeable	Total	H ₂ O Soluble	Exchangeable
NJA1	7339	335	793	5980	193	930	296	18	2	63	0.25	0.71
NJA2	8577	875	698	6135	205	600	290	60	8	52	0.21	0.46
NJA3	11675	401	585	4532	217	660	362	4	50	43	0.17	.063
NJA4	2306	108	7	2825	108	240	149	16	4	14	0.45	.022
NJB1	11001	684	849	5501	236	880	217	10	16	52	0.87	0.31
NJB2	11720	418	866	5157	230	990	385	1	16	44	0.17	.053
NJB3	16828	495	891	5097	396	1000	237	6	32	67	0.24	1.05
NJB4	8209	215	305	1459	100	400	1042	8	33	29	0.09	0.43
NJC1	4438	347	467	4704	125	--	386	6	20	59	0.15	0.59
NJC2	--	510	696	--	309	1350	--	11	14	--	0.17	.054
NJC3	9504	280	509	1289	215	600	1259	5	12	29	0.17	0.88
NJC4	5323	92	116	549	53	165	211	0.4	3	10	0.03	0.21
NJD1	12222	722	740	4352	264	910	249	13	39	36	1.07	0.82
NJD2	9073	244	330	3200	122	300	255	4	6	36	0.14	0.45
NJD3	2383	45	51	1483	45	60	104	4	2	10	0.06	0.29
NJD4	3434	--	--	1159	--	--	108	--	--	12	--	--
NJE1	12396	388	844	5454	310	320	258	1	26	26	0.71	0.44
NJE2	11842	368	611	6970	147	560	353	2	16	47	0.06	0.21
NJF1	11386	270	712	4168	134	680	274	120	8	30	0.28	0.86
NJF2	4967	42	141	4669	13	28	259	1	4	30	0.27	0.17
NJG1	11780	443	335	3633	197	160	162	118	56	35	3.05	0.91
NJG2	11138	147	--	3803	206	--	256	0.2	--	31	0.15	--
NJH1	6146	131	277	3593	102	285	247	4	--	38	0.58	0.23
NJH2	4292	180	648	2806	104	600	276	12	11	46	0.04	0.62
NJI	4335	15	10	60	12	4	38	1.7	0.9	4	1.75	0.02
NJJ	--	71	53	--	353	180	--	--	--	--	3.71	0.14

TABLE 1
 SOIL AND DREDGED MATERIAL METALS: HOUSTON, TEXAS, SITE

Element Sample Code	Ca ppm				Mg ppm				K ppm				Na ppm			
	A	B	C	D	A	B	C	D	A	B	C	D	A	B	C	D
HA-1	--	368	--	--	--	265	--	--	--	23	--	--	--	1025	--	--
HA-2	276	230	205	205	270	156	100	111	322	13	28	38	1260	725	650	800
HA-3	418	300	330	300	254	418	490	37	141	23	50	62	1410	1025	1100	1400
HA-4	420	263	370	330	260	150	215	940	329	20	61	68	1410	950	1200	1600
HB-1	--	455	580	--	--	520	427	--	--	36	58	--	--	2125	--	--
HB-2	916	432	750	275	384	358	425	187	180	63	84	34	2290	2400	2650	1100
HB-3	1020	522	790	450	381	433	420	463	450	82	101	99	2090	2750	2750	2900
HB-4	791	420	470	390	640	525	475	784	577	143	135	184	4030	4500	3500	4850
HC-1	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
HC-2	622	462	540	445	360	300	345	480	500	42	57	162	2130	1600	1670	4100
HC-3	524	450	455	350	420	345	355	469	559	63	80	125	2170	2300	2305	3200
HC-4	752	460	455	400	532	845	555	688	638	135	184	166	3560	3625	4300	4200
HD-1	--	312	500	--	--	445	440	--	--	90	91	--	--	2500	2200	--
HD-2	884	600	750	400	356	322	410	421	509	63	85	77	1920	1750	1850	2300
HD-3	791	350	430	430	372	499	420	442	479	65	80	74	2200	2225	2250	2400
HD-4	739	570	750	460	400	378	435	483	511	68	98	90	2291	2525	2500	2600
HE-1	--	332	245	--	--	377	365	--	--	49	75	--	--	2650	2800	--
HE-2	--	314	245	--	--	375	360	--	--	51	80	--	--	2750	2800	--
HF-1	360	304	275	365	332	295	325	421	500	50	80	90	2590	2580	2750	3200
HF-2	390	295	274	430	344	295	330	431	480	48	81	103	2900	2525	2500	3200
HG-1	--	218	--	395	--	282	--	413	--	41	--	115	--	2100	--	2600
HG-2	156	218	--	440	330	280	--	448	480	80	--	118	2130	1998	--	2700
HH-1	--	275	--	--	--	320	--	--	--	42	--	--	--	2415	--	--
HH-2	171	285	245	380	408	432	410	484	563	47	68	74	2500	2325	2200	2700
HI	152	348	455	395	452	418	455	464	610	56	88	79	2510	2530	2800	2800
HJ	--	355	330	305	--	425	425	443	--	59	80	66	--	2825	2300	2800

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TABLE J7 (Continued)

Element Sample Code	Mn ppm				Fe ppm				Cu ppb				Zn ppm			
	A	B	C	D	A	B	C	D	A	B	C	D	A	B	C	D
HA-1	--	3.2	--	--	--	.004	--	--	--	36	--	--	--	.006	--	--
HA-2	3.7	3.6	2.3	0.2	0.27	.003	.007	.0225	0	25	8	7	0.11	1.20	--	0.34
HA-3	3.6	5.3	3.2	0.9	0.33	.004	.017	.075	0	27	6	9	0.14	.013	--	0.06
HA-4	3.6	4.4	3.5	1.7	0.30	.008	.040	.038	0	33	3	4	0.09	.026	--	0.24
NB-1	--	11.6	2.0	--	--	.004	.004	--	--	72	24	--	--	.017	--	--
NB-2	22.5	16.0	3.6	4.3	0.35	.002	--	.030	0	102	5	5	0.14	--	--	0.03
NB-3	25.0	11.8	12.2	3.8	0.30	.046	.065	.038	0	101	6	13	0.16	.005	--	0.29
NB-4	13.2	7.5	5.4	4.6	0.43	.019	.057	.045	0	165	6	9	0.11	.019	--	0.03
HC-1	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
HC-2	9.7	10.0	8.5	5.2	0.35	.006	.013	.070	0	67	10	9	0.11	.085	--	0.05
HC-3	7.8	11.0	9.4	6.8	0.22	.014	.005	.038	0	73	5	9	0.08	.077	--	0.03
HC-4	9.0	7.6	5.6	2.9	0.35	.127	.710	.045	0	79	6	7	0.12	.002	--	0.02
HD-1	--	5.5	11.4	--	--	.003	.005	--	--	58	15	--	--	.022	--	--
HD-2	19.5	19.3	21.2	0.2	0.43	.006	.005	.028	0	88	7	6	0.11	.026	--	0
HD-3	24.8	43.8	30.0	15.5	0.35	.012	.005	.018	0	43	4	10	0.11	.009	--	0.02
HD-4	27.0	21.7	18.7	12.1	0.43	.750	.036	--	--	77	5	9	0.11	.100	--	0.05
HE-1	--	5.2	8.2	--	--	.011	.004	--	--	59	8	--	--	.005	--	--
HE-2	--	3.7	10.3	--	--	.005	.010	--	--	54	6	--	00	.004	--	--
HF-1	18.0	13.5	12.5	2.3	0.35	.004	.010	1.100	20	48	6	10	0.19	.019	--	0.04
HF-2	18.4	18.0	16.0	4.7	.035	.006	.015	.030	30	42	4	13	0.14	.008	--	0.04
HG-1	--	22.8	--	0.7	--	.005	--	.038	--	21	--	10	--	.080	--	--
HG-2	6.6	13.7	--	5.5	0.31	.700	--	.030	20	41	3	10	0.10	.039	--	0.06
HH-1	--	10.0	--	--	--	.008	--	--	--	37	--	--	--	.080	--	--
HH-2	33.0	47.5	39.2	42.0	0.30	.004	--	.038	20	41	3	10	0.10	.039	--	0.06
HI	3.7	23.8	21.0	5.1	0.30	--	.55	.050	20	58	5	4	0.08	.012	--	0.07
HJ	--	30.0	19.0	5.5	--	.003	.016	.070	--	56	6	8	--	.011	--	0.02

TABLE J7 (Continued)

Element Sample Code	Cd ppb				Ni ppm				Pb ppb				Hg ppb			
	A	B	C	D	A	B	C	D	A	B	C	D	A	B	C	D
RA-1	--	0.4	--	--	--	5	--	--	--	2.4	--	--	--	0	--	--
RA-2	1.0	0.4	0.3	0.7	47	3	8	10	80.0	1.9	1.5	6	0.06	--	0.90	--
RA-3	1.0	0.3	0.4	0.5	6	3	9	8	80.0	2.8	2.8	7	0.22	1.20	0.05	--
RA-4	1.0	0.8	0.3	1.2	10	4	7	7	70.9	2.6	.22	5	0.06	0.90	0.36	--
RB-1	--	0.4	0.6	--	--	9	15	--	--	4.9	2.0	--	--	0	0.33	--
RB-2	1.0	0.7	0.1	0.8	7	4	4	8	160	8.7	3.0	3	1.24	1.30	0.20	--
RB-3	1.0	0.8	0.2	1.3	9	2	5	19	120	8.9	2.4	3	0.10	0	0	--
RB-4	1.0	0.9	0.2	0.7	18	4	5	17	280	5.5	2.4	5	0.06	0.55	0.10	--
RC-1	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
RC-2	1.0	1.0	0.2	2.0	14	77	9	10	21.0	1.3	2.1	3	0.30	2.40	0.13	--
RC-3	1.0	0.3	0.2	1.3	13	3	8	11	20.0	5.0	1.4	4	0.07	0.35	0	--
RC-4	1.0	0.4	0.4	1.0	5	5	7	10	20.0	6.2	1.5	4	0.23	1.10	0.85	--
RD-1	--	1.2	1.2	--	--	3	52	--	--	0.7	2.3	--	--	4.65	0	--
RD-2	1.0	0.5	0.3	0.6	1	8	7	8	130	1.0	1.8	1	0.11	10.8	0	--
RD-3	1.0	2.2	0.2	0.8	8	3	3	19	200	0.6	2.0	1	0.22	1.10	0	--
RD-4	1.0	0.4	0.4	1.8	6	5	4	23	210	0.3	1.2	2	0.20	1.85	0	--
RE-1	--	1.2	0.7	--	--	3	18	--	--	6.2	1.3	--	--	0.20	--	--
RE-2	--	1.0	0.8	--	--	4	15	--	--	1.0	1.2	--	--	1.10	0	--
RF-1	2.0	0.8	0.2	0.8	10	6	11	30	200	7.0	1.5	1	0.10	0.14	0.05	--
RF-2	6.0	0.8	0.2	1.3	23	6	12	22	240	7.1	1.6	1	0.10	.080	0	--
RG-1	--	0.7	--	--	--	5	--	20	--	5.5	--	1	--	0.07	--	--
RG-2	8.0	0.7	--	1.0	11	8	--	10	180	4.8	--	1	0.08	0.20	--	--
RH-1	--	0.9	--	--	--	6	--	--	--	5.4	--	--	--	--	--	--
RH-2	1.0	1.4	0.4	1.0	83	8	19	22	170	4.0	1.5	3	0.08	0.32	0	--
RI	1.0	0.6	0.2	1.0	46	9	12	17	180	4.8	1.9	1	0.19	0	0	--
RJ	--	.24	0.2	10	--	12	11	19	--	5.4	1.0	2	--	0	0.5	--

TABLE J7 (Continued)

Element Sample Code	pH				Eh mV				Sulfate, mg/l				Chloride, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D	A	B	C	D
HA-1	--	6.83	--	--	--	--	--	--	--	--	--	--	--	--	--	--
HA-2	6.76	6.33	6.7	6.5	--	--	-60	-69	575	675	165	--	3179	2229	1198	--
HA-3	6.97	6.26	6.5	6.2	--	--	-40	-2.4	184	600	24	250	2970	2293	2084	2571
HA-4	7.18	6.85	6.7	7.3	--	--	+60	-45	137	--	170	--	2970	--	2188	2772
HB-1	--	7.09	7.4	--	--	--	-30	--	--	--	555	--	--	--	4221	--
HB-2	6.90	6.46	6.5	5.9	--	--	+90	20	144	48	75	80	5628	4844	5159	2215
HB-3	6.87	6.94	6.7	6.4	--	--	+200	190	168	75	200	10	5263	5408	5471	4965
HB-4	7.08	6.46	6.3	6.5	--	--	+30	25	21	55	--	1.5	8963	8612	6201	8794
HC-1	--	--	--	--	--	--	--	--	--	--	--	144	--	--	--	--
HC-2	7.19	6.34	7.0	7.3	--	--	+20	-100	300	385	225	--	4334	3768	2595	3776
HC-3	7.23	6.69	--	--	--	--	--	--	69	290	140	48	6410	4716	4481	5443
HC-4	7.10	6.90	7.5	5.6	--	--	-40	-10	100	50	2.5	5.5	7452	7556	8233	7681
HD-1	--	7.24	6.6	--	--	--	+80	--	--	--	525	--	--	--	4794	--
HD-2	7.13	6.85	8.0	5.6	--	--	+210	350	55	160	380	31	5054	4460	4533	4998
HD-3	7.22	6.20	6.8	5.8	--	--	+50	50	283	1000	420	425	5419	5380	4585	5065
HD-4	7.09	6.39	7.5	5.6	--	--	-100	+70	283	280	245	475	5367	5075	4898	5321
HE-1	--	6.77	7.3	--	--	--	+50	--	--	250	--	--	--	--	4690	--
HE-2	--	6.62	6.4	8.1	--	--	+100	15	--	--	330	475	--	--	4481	5221
HF-1	7.53	6.15	6.4	7.2	--	--	+150	10	--	305	420	88	--	5357	4950	5699
HF-2	7.24	6.47	7.1	8.1	--	--	-10	35	--	650	200	238	--	5993	5106	--
HG-1	--	7.10	--	7.4	--	--	--	-5	--	750	--	1388	--	4511	--	4341
HG-2	7.05	7.03	--	8.2	--	--	--	57	--	988	--	938	--	4203	--	4319
HH-1	--	6.37	--	7.4	--	--	--	5	--	--	--	1075	--	--	--	556
HH-2	6.98	6.21	6.8	7.5	--	--	+60	65	--	813	1000	700	--	5023	4168	4486
HI	7.54	6.88	6.8	6.8	--	--	+50	36	--	1100	490	250	--	4767	4950	5042
HJ	--	6.92	6.2	7.6	--	--	+20	58	--	--	380	357	--	--	--	5009

TABLE J7 (Continued)

Element Sample Code	Alkalinity, mg/l				TOC, mg/l				TIC, mg/l							
	A	B	C	D	A	B	C	D	A	B	C	D	A	B	C	D
HA-1	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
HA-2	707	559	256	--	30	45	150	--	200	110	60	--	230	155	210	--
HA-3	1700	--	1229	747	110	40	760	240	270	150	260	190	380	190	1020	430
HA-4	1,000	--	943	1049	120	--	630	315	260	--	240	245	380	--	870	560
HB-1	--	--	408	--	--	--	245	--	--	--	110	--	--	--	355	--
HB-2	972	1606	1800	465	100	70	1070	90	210	450	400	110	310	420	1470	200
HB-3	1392	1967	1517	1017	70	110	920	315	270	430	330	245	340	540	1250	560
HB-4	2056	2169	2275	2294	260	200	1190	540	240	530	530	540	600	730	1720	1080
HC-1	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
HC-2	1108	713	874	738	110	30	620	600	250	150	200	480	360	180	820	1080
HC-3	1732	1078	1152	738	110	40	745	420	400	190	255	290	510	730	1000	710
HC-4	1800	2385	2270	2280	260	100	370	230	380	510	540	170	640	610	910	400
HD-1	--	--	557	--	--	--	400	--	--	--	110	--	--	--	510	--
HD-2	--	691	250	406	40	30	180	150	100	170	60	110	140	200	240	260
HD-3	828	1179	797	855	10	55	575	270	190	275	200	200	200	330	775	470
HD-4	1152	1676	1625	923	280	130	1090	330	220	320	350	210	500	450	1440	540
HE-1	--	--	626	--	--	--	410	--	--	--	160	--	--	--	570	--
HE-2	--	--	768	667	--	--	555	220	--	--	180	140	--	--	735	340
HF-1	--	792	696	1020	--	45	485	350	--	205	165	210	--	250	650	560
HF-2	--	761	1003	870	--	30	630	290	--	200	240	210	--	230	870	500
FG-1	--	616	--	604	--	40	--	230	--	1,0	--	110	--	200	--	340
HG-1	--	757	--	1077	--	35	--	355	--	125	--	245	--	160	--	600
HH-1	--	--	--	556	--	--	--	170	--	--	--	130	--	--	--	300
HH-2	--	1131	1061	929	--	40	695	290	--	250	255	210	--	290	950	500
HI	--	1052	898	1035	--	100	620	365	--	90	210	235	--	190	830	600
HJ	--	--	614	790	--	--	400	230	--	--	160	200	--	--	560	430

TABLE J7 (Concluded)

Element Sample Code	Phosphate ppm			
	A	B	C	D
HA-1	--	--	--	--
HA-2	0.019	--	0.01	--
HA-3	0.054	--	0.10	--
HA-4	0.023	--	0	0.075
HB-1	--	--	0.32	--
HB-2	0.099	--	0.36	--
HB-3	0.012	--	0	0.04
HB-4	--	--	0.2	0.42
HC-1	--	--	--	--
HC-2	0.128	--	0.03	0.14
HC-3	--	--	0.06	0.91
HC-4	0.59	--	0.55	0.335
HD-1	--	--	--	--
HD-2	0.011	--	0.02	--
HD-3	0.054	--	0	0.1
HD-4	0.015	--	0.11	0.04
HE-1	--	--	--	--
HE-2	--	--	--	--
HF-1	--	--	0.01	0.035
HF-2	--	--	0.22	0
HG-1	--	--	--	--
HG-2	--	--	--	0.570
HH-1	--	--	--	--
HH-2	--	--	0.02	0.09
HI	--	--	0	0.065
HJ	--	--	--	0.065

SOIL AND DREDGED MATERIAL METALS - WETPOND, ALABAMA, SITE (all units are mg/kg)

Sample Code	K			Hg			Mn			Ni		
	Total	Exchangeable	H ₂ O Soluble	Total	Exchangeable	H ₂ O Soluble	Total	Exchangeable	H ₂ O Soluble	Total	Exchangeable	H ₂ O Soluble
PA1	93905	576.7	192.2	5499.0	1507	80	253.80	120.1	2.400	38.070	0.104	0.120
PA2	1043.7	17.6	23.5	397.	54	9	168.98	9.4	0.112	4.6221	0.059	0.050
PA3	2816.5	118.9	75.1	1179.0	261	29	222.70	16.5	0.542	8.7115	0.042	0.042
PA4	2848.2	103.8	107.9	1090.8	18	36	242.40	17.8	0.133	6.7872	0.042	0.013
PB1	1964.8	5610	5610	706.10	112	12	184.2	18.6	0.134	4.2365	0.045	0.078
PB2	2441.4	133.7	9618	88.92	295	92	125.2	30.5	8.000	5.5714	0.138	0.368
PB3	1004.7	52.5	94.5	395.97	168	131	100.47	16.0	8.00	5.4963	0.110	0.074
PB4	1276.6	21.2	63.6	545.01	93	92	88.380	9.3	4.242	4.5663	0.092	0.028
PC1	3292.8	7.9	5.1	635.	4	4	164.64	3.3	3.136	6.7032	0.119	0.044
PC2	6446.7	404.8	116.2	2593.5	774	8	214.89	21.5	0.352	14.598	0.039	0.352
PC3	4060.0	162.3	59.8	1957.5	350	12	304.50	46.8	0.743	9.2800	0.068	0.171
PC4	2473.8	66.4	55.0	937	174	9	227.85	1.96	--	7.1610	0.039	0.14
PD1	5177.7	6.92	4.5	2144.5	22	7	193.51	2.4	0.273	73.220	0.118	0.010
PD2	8512.0	--	--	4043.2	--	--	313.88	--	--	180.88	--	--
PD3	2105.3	18.1	13.5	893.33	61	11	79.660	2.3	0.036	9.5592	0.066	0.058
PD4	3607.5	218.0	31.1	1924.0	480	14	81.770	3.5	0.036	9.0428	0.026	0.093
PE1	1277.2	18.0	16.2	535.60	67	11	41.350	1.1	0.171	3.6256	0.099	0.036
PE2	10488	683.77	127.7	4457.4	1117	31	393.30	0.04	1.368	17.917	0.100	0.192
PF1	1184.4	13.4	2.0	434.28	42	48	49.350	1.0	0.000	6.5142	0.027	0.007
PF2	849.80	7.8	2.0	121.40	14	4	30.350	0.2	0.004	2.7315	0.031	0.016
PG1	2887.8	27.4	39.2	98.00	118	80	43.750	0.27	0.063	3.7625	0.031	0.062
PG2	3867.4	142.6	92.7	1711.8	535	71	63.40	0.21	3.6	6.2766	0.078	0.449
PH1	1888.0	--	--	396.48	--	--	47.200	3.6	--	2.4072	--	--
PH2	1477.5	20.2	12.1	242.31	69	6	53.190	82.1	0.174	2.9550	0.016	0.065
PI	5198.4	9.4	3.12	1710.0	11	3	54.720	0.69	0.234	5.472	0.041	0.022
PJ	521.60	3.3	1.0	247.68	9	1	46.080	2.6	0.007	0.8640	0.026	0.030

81C

TABLE JH (Continued)

Sample Code	Ca			Cd			Cu			Fe		
	Total	Exchangeable	H ₂ O Soluble	Total	Exchangeable	H ₂ O Soluble	Total	Exchangeable	H ₂ O Soluble	Total	Exchangeable	H ₂ O Soluble
PA1	--	1032	25	135.36	3.2	3.2	67.680	0.032	0.136	38323	2.965	6.3
PA2	--	371	14	14.910	8.8	2.4	8.4490	0.047	0.141	33448	0.059	6.5
PA3	--	370	8	65.500	0.0	0.8	16.375	--	0.029	11594	0.048	6.9
PA4	--	407	20	115.14	2.1	0.2	9.6960	0.017	2.025	12726	1.702	.2
PB1	--	689	15	24.560	7.8	2.8	4.9120	0.034	0.017	12894	0.017	19.7
PB2	--	363	83	62.600	12.9	2.8	8.7640	0.101	0.180	11268	0.005	1.3
PB3	--	252	48	35.460	4.7	1.6	8.2740	0.373	0.037	6678.3	0.001	1.9
PB4	--	156	47	39.280	2.8	1.4	8.3470	0.389	0.014	5892.0	0.014	1.2
PC1	--	176	15	70.560	17.9	2.4	104.08	15.4	0.520	8996.4	0.020	0.6
PC2	--	578	2	14.820	1.8	7.4	6.6690	0.025	0.338	28899	0.081	28.1
PC3	--	544	7	72.500	3.4	3.4	74.675	0.026	0.196	14500	0.047	66.4
PC4	--	450	13	52.080	--	--	27.993	--	--	7616.7	0.086	262
PD1	--	253	17	78.450	13.2	0.6	117.15	10.0	0.045	5753.0	0.017	0.9
PD2	--	--	--	180.88	--	--	278.77	--	--	92036	--	--
PD3	--	289	12	68.280	6.8	0.5	14.794	0.144	0.023	14623	0.014	0.14
PD4	--	410	16	62.530	1.0	1.0	14.430	0.000	0.042	15392	0.026	1.3
PE1	--	396	26	53.560	27.9	0.9	4.5320	0.324	0.045	4532.0	0.027	14.5
PE2	--	1246	14	157.32	0.0	15.5	19.228	0.046	1.295	25958	1.641	34.8
PF1	--	393	29	98.700	12.4	0	6.9090	0.077	0.120	987.00	0.013	0.67
PF2	--	234	33	36.420	8.2	1.4	3.6420	0.074	0.008	3217.1	0.023	0.9
PG1	--	585	27	61.250	5.1	3.1	3.5000	0.047	0.082	6125.0	0.016	3.3
PG2	--	1030	6	57.060	5.7	-	5.072	0.078	--	25740	0.371	8.9
PH1	--	--	--	14.160	--	--	2.8320	--	--	3634.4	--	--
PH2	00	320	4	23.640	4.4	1.6	3.5460	0.052	0.032	3959.7	0.077	5.2
PI	--	60	4	47.880	3.1	1.6	8.8920	0.022	0.013	11833	0.041	0.2
PJ	--	227	16	28.800	1.6	0.7	2.8800	0.001	0.007	3340.8	0.026	1.7

b LP

TABLE JB (Concluded)

Sample Code	Pb			Na			Zn			Hg		
	Total	Exchangeable	H ₂ O Soluble	Total	Exchangeable	H ₂ O Soluble	Total	Exchangeable	H ₂ O Soluble	Total	Exchangeable	H ₂ O Soluble
PA1	94.752	0.064	0.328	7021.8	1562.0	3044	14.67	0.48	0.032	2.21	--	--
PA2	3.0317	0.015	0.153	369.98	29.4	90	10.437	0.23	0.059	0.16	--	--
PA3	5.3055	0.016	0.071	1768.5	178.5	1001	53.710	0.08	0.017	0.33	--	--
PA4	6.3630	0.021	0.075	1696.8	161.9	1029	73.932	0.75	0.008	0.60	--	--
PB1	4.2980	0.017	0.034	42.980	39.2	129	14.736	0.78	0.067	0.40	--	--
PB2	8.3258	0.037	0.203	1627.6	322.7	847	24.414	3.09	1.708	0.49	--	--
PB3	15.957	0.735	0.215	1595.7	128.6	336	18.321	1.21	0.021	0.45	--	--
PB4	12.422	0.460	0.035	1325.7	53.0	157	35.352	1.27	0.021	1.55	--	--
PC1	90.560	1.925	0.016	705.60	6.75	67	51.744	4.13	1.191	0.32	--	--
PC2	5.0388	0.071	0.341	2000.7	792.0	217	34.827	0.11	2.182	0.11	--	--
PC3	181.25	0.724	0.461	1160.0	121.3	243	91.350	1.37	0.103	2.58	--	--
PC4	84.630	0.785	--	716.10	48.7	542	54.449	0.94	--	1.90	--	--
PD1	78.450	0.027	0.028	941.40	1.7	3.5	81.065	3.42	0.024	1.32	--	--
PD2	186.20	--	--	1649.2	--	--	212.80	--	--	2.32	--	--
PE1	5.3972	0.135	0.063	206.00	6.3	45	21.424	8.65	0.081	0.59	--	--
PE2	13.023	0.027	0.438	4544.8	1213.0	1186	98.762	0.45	4.925	1.02	--	--
PF1	7.5012	0.075	0.027	730.38	13.4	1.7	15.792	0.26	0.027	0.57	--	--
PF2	4.9167	0.070	0.012	127.47	3.9	1.2	7.2840	0.20	0.023	0.43	--	--
PG1	3.2375	0.047	0.059	297.50	7.8	7.8	9.6250	0.27	0.118	0.02	--	--
PG2	18.386	0.005	0.083	564.26	101.3	46	20.922	0.50	1.283	0.56	--	--
PH1	3.7288	--	--	273.75	--	--	12.744	0.04	0.033	0.04	--	--
PI	8.7552	0.019	0.031	677.16	1.6	3.1	25.308	0.13	0.025	1.71	--	--
PJ	2.0160	0.001	0.020	149.76	0.7	6.6	8.6400	0.13	0.026	0.14	--	--

APPENDIX K: LEACHATE/INTERSTITIAL WATER ANALYSES

TABLE K1
LEACHATE/INTERSTITIAL WATER: GRAND HAVEN, MICHIGAN, SITE

Sample Code	Ca, mg/l				Cd, mg/l				Cu, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
MA1	-	-	360	-	-	-	0.9	-	-	-	62	-
MA2	-	-	360	-	-	-	0.7	-	-	-	25	-
MA3	132	-	-	345	0.1	-	-	3	24	-	-	42
MA4	284	-	150	310	1	-	0.6	0.5	22	-	3	59
MB1	-	-	610	310	-	-	0.8	0.5	-	-	37	2
MB2	-	-	-	-	-	-	-	-	-	-	-	-
MB3	350	-	430	420	1	-	0.8	0.5	1	-	25	3
MB4	170	-	170	365	1	-	0.9	-0.5	1	-	14	1
MC1	-	430	480	420	-	0.5	1.4	4	-	23	33	7
MC2	-	567	460	370	-	0.5	0.9	1	-	0.3	10	7
MD1	-	367	210	250	-	0.7	0.8	2	-	10	25	10
MD2	-	530	170	230	-	0.3	0.9	0.5	-	6	10	2
ME1	-	390	250	320	-	0.8	0.8	1	-	7	8	1
ME2	-	437	220	310	-	0.5	0.9	0.5	-	6	1	9
MF1	-	-	-	-	-	-	0.6	0.4	-	-	8	18
MF2	-	-	440	420	-	-	1.0	1	-	-	18	37
MF3	-	-	400	-	-	-	0.8	-	-	-	8	-
MF4	-	-	400	480	-	-	1.0	0.2	-	-	3	37

A = December 1, 1976; B = April 8, 1977; C = May 30, 1977; D = August 5, 1977.

TABLE K1 (Continued)

Sample Code	Ca, mg/l				Cd, mg/l				Cu, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
MG1	-	-	-	-	-	-	-	-	-	-	-	-
MG2	-	-	380	350	-	-	1.0	0.5	-	-	8	2
MG3	200	-	490	-	0.2	-	0.8	-	18	-	4	-
MG4	170	-	480	330	0.1	-	0.9	1	21	-	5	4
MH1	-	273	140	320	-	0.3	0.8	0.5	-	3	24	3
MH2	-	250	320	310	-	0.7	0.8	2	-	12	3	9
MI	113	-	560	-	0.3	0.8	0.9	-	22	11	9	-
MJ	37	-	-	70	1	0.9	-	4	17	2	-	9

TABLE K1 (Continued)

Sample Code	Fe, mg/l				Hg, mg/l				K, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
MA1	-	-	6	-	-	-	0.1	-	-	-	39	-
MA2	-	-	56	-	-	-	0.1	-	-	-	28	-
MA3	210	-	-	25	0.6	-	-	0.4	110	-	-	27
MA4	170	-	ND	11	ND	-	0.3	-	110	-	26	25
MB1	-	-	7	45	-	-	0.4	0.3	-	-	24	23
MB2	-	-	-	-	-	-	-	-	-	-	-	-
MB3	310	-	4	4	0.2	-	0.4	0.4	80	-	25	23
MB4	830	-	17	6	0.2	-	1.0	0.8	48	-	15	24
MC1	-	19	34	16	-	0.7	0.6	0.4	-	8	30	22
MC2	-	27	7	31	-	0.9	0.3	0.6	-	6	20	13
MD1	-	12	4	198	-	0	0.6	0.3	-	7	28	12
MD2	-	19	40	7	-	0.1	0.6	0.8	-	8	14	11
ME1	-	18	10	17	-	0.9	0.5	0.1	-	10	13	8
ME2	-	7	2	45	-	0.2	0.4	0.1	-	9	12	12
MF1	-	-	6	18	-	-	0.5	0.8	-	-	4	5
MF2	-	-	ND	37	-	-	0.7	0.1	-	-	7	-
MF3	-	-	6	-	-	-	0.5	-	-	-	7	-
MF4	-	-	1	37	-	-	0.5	0.1	-	-	7	7

TABLE 11 (continued)

Sample Code	Fe, mg/l				Hg, mg/l				K, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
MG1	-	-	-	-	-	-	-	0.01	-	-	-	13
MG2	-	-	-	2	6	-	-	0.4	-	-	13	-
MG3	240	-	2	-	0.2	-	0.7	0.3	67	-	14	28
MG4	24C	-	6	64	0.1	-	0.8	0.7	61	-	14	-
MH1	-	23	26	23	-	-	0.2	0.2	-	4	1	9
MH2	-	7	4	25	-	-	0.6	0.3	-	1	7	6
MJ	320	8	34	-	0.3	0.8	0.4	-	39	4	11	-
MJ	240	180	-	158	0.6	1.1	-	0.6	17	5	-	3

TABLE K1 (Continued)

Sample Code	Mn, mg/l				Mg, mg/l				Ni, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
MA1	-	-	70	-	-	-	3.19	-	-	-	116	-
MA2	-	-	80	-	-	-	0.005	-	-	-	38	-
MA3	47	-	-	112	0.4	-	-	0.10	200	ND	0	43
MA4	60	ND	89	93	1.8	-	0.037	0.15	130	ND	93	36
MB1	-	-	70	72	-	-	0.4	0.051	-	-	160	93
MB2	-	-	-	-	-	-	-	-	-	-	-	-
MB3	47	-	80	93	1.1	-	0.001	0.11	100	-	37	87
MB4	20	-	70	85	0.6	-	0.002	0.57	100	-	25	59
MC1	-	42	90	75	-	0.02	0.012	0.48	-	92	42	61
MC2	-	64	65	59	-	1.9	0.016	0.63	-	77	33	25
MD1	-	46	70	38	-	2.6	0.094	0.060	ND	50	27	22
MD2	-	37	35	36	-	2.7	0.065	0.020	-	32	15	6
ME1	-	44	40	54	-	3.7	2.08	1.05	-	32	25	17
ME2	-	44	35	54	-	4.8	3.22	1.05	-	29	12	9
MF1	-	-	60	-	-	-	0.86	1.27	-	-	190	342
MF2	-	-	60	70	-	-	4.68	1.0	-	-	152	317
MF3	-	-	50	-	-	-	1.73	-	-	-	45	-
MF4	-	-	45	59	-	-	0.10	0.50	-	-	18	2

TABLE K1 (continued)

Sample Code	Mg, mg/l				Mn, ppm				Ni, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
MG1	-	-	-	-	-	-	-	0.68	-	-	-	-
MG2	-	-	70	88	-	-	3.21	-	-	-	108	24
MG3	59	-	80	-	2.6	-	0.92	0.76	190	-	55	-
MG4	60	-	75	72	2.7	-	1.14	-	190	-	60	1
MH1	-	25	15	38	-	2.8	0.004	0.15	-	14	11	3
MH2	-	13	35	36	-	0.03	3.64	0.097	-	7	9	7
MI	38	47	75	-	2.6	2.8	5.9	-	120	319	412	-
MJ	9	8	-	8	0.1	0.01	-	0.047	150	20	-	0

TABLE K1 (Continued)

Sample Code	Pb, mg/l				Na, mg/l				Zn, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
MA1	-	-	<1	-	-	-	100	-	-	-	20	-
MA2	-	-	<1	-	-	-	100	-	-	-	5	-
MA3	3	-	-	<1	790	-	-	110	80	-	-	1
MA4	3	-	<1	<1	680	-	84	60	14	-	0.1	3
MB1	-	-	3	<1	-	-	75	-	-	-	10	8
MB2	-	-	-	-	-	-	-	-	-	-	-	-
MB3	1	-	<1	<1	75	-	72	42	70	-	7	1
MB4	1	-	<1	<1	80	-	45	55	22	-	18	1
MC1	-	<1	3	<1	-	35	68	72	-	94	25	350
MC2	-	<1	<1	<1	-	34	42	55	-	126	13	12
MD1	-	<1	2	<1	-	40	500	85	-	66	7	100
MD2	-	<1	<1	<1	-	39	75	48	-	54	25	2
ME1	-	<1	<1	<1	-	22	43	55	-	111	21	12
ME2	-	<1	<1	<1	-	27	45	55	-	16	4	4
MF1	-	-	<1	<1	-	-	52	55	-	-	4	100
MF2	-	-	<1	<1	-	-	55	75	-	-	230	5
MF3	-	-	<1	<1	-	-	48	-	-	-	17	-
MF4	-	-	1	2	-	-	48	70	-	-	8	70

TABLE K1 (Continued)

Sample Code	Pb, mg/l				Na, mg/l				Zn, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
MG1	-	-	-	-	-	-	-	-	-	-	-	-
MG2	-	-	<1	<1	-	-	108	45	-	-	67	1
MG3	1	-	<1	-	32	-	55	-	40	-	6	-
MG4	1	-	<1	<1	31	-	60	40	50	-	22	1
MH1	-	<1	<1	<1	-	12	7	35	-	76	27	2
MH2	-	<1	<1	<1	-	6	23	25	-	106	15	3
MI	1	<1	<1	-	10	15	20	-	640	131	180	-
MJ	2	<1	-	1	9	12	-	10	40	36	-	30

TABLE K1 (Continued)

Sample Code	pH				Eh, mV				SO ₄ , mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
MA1	-	-	-	-	-	-	-	-	-	-	-	-
MA2	-	-	-	-	-	-	-	-	-	-	525	-
MA3	7.7	-	-	6.7	-	-	-	300	-	-	-	838
MA4	7.1	-	-	6.8	-	-	-	140	61	-	525	110
MB1	-	-	-	-	-	-	-	-	-	-	-	100
MB2	-	-	-	-	-	-	-	-	-	-	-	-
MB3	7.1	-	-	6.5	-	-	-	183	-	-	800	650
MB4	7.2	-	-	6.6	-	-	-	146	323	-	430	450
MC1	-	7.5	-	6.8	-	85	-	160	-	1220	-	1175
MC2	-	7.0	-	6.1	-	39	-	190	-	1550	1700	475
MD1	-	6.8	-	-	-	-61	-	-	-	551	363	425
MD2	-	6.7	-	-	-	2	-	-	-	490	136	425
ME1	-	6.8	-	6.1	-	-34	-	33	-	-	375	713
ME2	-	6.7	-	6.4	-	-64	-	17	-	-	-	1325
MF1	-	-	-	6.1	-	-	-	200	-	-	750	525
MF2	-	-	-	6.0	-	-	-	43	-	-	750	-
MF3	-	-	-	5.8	-	-	-	300	-	-	600	1000
MF4	-	-	-	6.3	-	-	-	90	-	-	525	463

K10

TABLE K1 (Continued)

Sample Code	pH				Eh, mV				SO ₄ , mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
MG1	-	-	-	-	-	-	-	-	-	-	-	-
MG2	-	-	-	-	-	-	-	-	-	-	-	990
MG3	6.8	-	-	-	-	-	-	-	14	-	1238	-
MG4	6.9	-	-	-	-	-	-	-	9	-	1115	575
MH1	-	7.0	-	-	-	-80	-	-	-	1900	1562	-
MH2	-	7.3	-	-	-	46	-	-	-	200	192	938
MI	6.8	6.2	-	-	-	22	-	-	-	1400	-	-
MJ	6.7	7.3	-	6.5	-	-75	-	70	39	110	43	50

TABLE K1 (Continued)

Sample Code	Cl. mg/l				Alk. mg/l				TOC. mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
MA1	-	-	-	-	-	-	614	-	-	-	260	-
MA2	-	-	133	-	-	-	960	-	-	-	610	-
MA3	1000	-	-	165	681	-	-	376	815	-	-	150
MA4	1051	-	117	88	-	-	577	1245	200	-	370	-
MB1	-	-	-	157	-	-	-	593	-	-	-	175
MB2	-	-	-	-	-	-	-	-	-	-	-	-
MB3	168	-	112	117	180	-	485	935	35	-	290	210
MB4	168	-	64	69	264	-	518	963	50	-	280	160
MC1	-	104	-	237	-	209	ND	131	-	50	23	40
MC2	-	104	90	122	-	180	276	536	-	50	135	130
MD1	-	125	739	191	-	471	365	154	-	130	-	-
MD2	-	99	64	122	-	431	348	382	-	70	160	-
ME1	-	67	69	90	-	392	379	245	-	110	160	85
ME2	ND	109	53	112	-	569	230	228	-	105	115	55
MF1	-	-	58	48	-	-	-	234	-	-	48	-
MF2	-	-	74	-	-	-	-	-	-	-	210	-
MF3	-	-	93	37	-	-	490	217	-	-	245	-
MF4	78	-	74	165	-	-	466	1009	-	-	235	290

TABLE K1 (Continued)

Sample Code	Cl, mg/l				Alk, mg/l				TOC, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
MG1	-	-	-	146	-	-	-	-	-	-	-	-
MG2	-	-	69	-	-	-	682	735	-	-	350	220
MG3	88	-	74	85	1127	-	528	-	95	-	250	-
MG4	93	-	72	-	1120	-	461	741	75	-	235	-
MH1	-	104	16	-	-	176	134	-	-	20	40	-
MH2	-	104	40	77	-	141	408	182	-	30	140	-
MI	-	40	21	-	-	400	715	-	-	135	345	-
MJ	-	104	21	74	24	35	70	91	30	35	35	30

K13

TABLE K 1 (Continued)

Sample Code	TC, mg/l				TIC, mg/l				P, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
MA1	-	-	420	-	-	-	160	-	-	-	-	-
MA2	-	-	860	-	-	-	250	-	-	-	0.01	-
MA3	955	-	-	230	140	-	-	80	0.005	-	-	0.07
MA4	340	-	520	-	140	-	150	-	0.021	-	0	ND
MB1	-	-	-	300	-	-	-	125	-	-	-	-
MB2	-	-	-	-	-	-	-	-	-	-	-	-
MB3	100	-	410	410	65	-	120	200	-	-	0.015	0.01
MB4	130	-	380	390	80	-	100	230	-	-	0.01	0.005
MC1	-	110	25	80	-	60	2	40	-	0.15	-	ND
MC2	-	100	195	250	-	50	20	120	-	-	ND	0.36
MD1	-	255	-	-	-	125	-	50	-	0.02	0.01	-
MD2	-	160	250	0	0	90	90	110	-	ND	0.025	0.01
ME1	-	210	240	135	-	100	80	50	-	ND	0.01	-
ME2	-	230	180	90	-	125	65	35	-	0.003	-	-
MF1	-	-	60	-	-	-	12	65	-	-	-	ND
MF2	-	-	310	-	-	-	100	-	-	-	0.03	-
MF3	-	-	365	-	-	-	120	55	-	-	-	0
MF4	-	-	340	500	-	-	105	210	-	-	0.02	0.8

TABLE K1 (Concluded)

Sample Code	TC, mg/l				TIC, mg/l				P, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
MG1	-	-	-	-	-	-	-	-	-	-	-	-
MG2	-	-	500	400	-	-	150	180	-	-	-	0.2
MG3	345	-	370	-	250	-	120	-	-	-	0.02	-
MG4	300	-	335	-	225	-	100	165	-	-	0.015	ND
MH1	-	70	95	-	-	50	55	-	-	ND	-0.01	0
MH2	-	70	220	-	-	40	80	50	-	0.01	0.02	ND
MI	-	250	480	-	20	115	135	-	-	0.007	0.03	-
MJ	50	35	50	55	-	10	15	25	-	0.03	-	0.01

K15

TABLE K2
LEACHATE/INTERSTITIAL WATER: SAYREVILLE, NEW JERSEY, SITE

Sample Code	Ca, mg/l				Cd, ug/l				Cu, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
NJA1	-	390	410	-	-	104	82	-	-	800	118	-
NJA2	-	308	360	300	-	5	47	9	-	400	258	93
NJA3	101	228	340	-	1	3	53	-	2	29	65	-
NJA4	98	228	340	-	2	1	51	9	2	400	42	-
NJB1	-	563	530	200	-	204	83	8	-	350	64	270
NJB2	-	470	-	250	-	166	56	4	-	3000	36	220
NJB3	-	446	380	250	-	-	100	5	-	29	38	376
NJB4	319	353	-	100	1	1	-	2	23	3	-	135
NJC1	-	553	540	-	-	154	39	-	-	62	32	-
NJC2	-	544	540	50	-	129	6	5	-	14	10	45
NJC3	271	573	440	-	1	179	5	-	21	-	47	-
NJC4	292	670	500	-	1	129	7	-	20	82	16	-
NJD1	-	398	450	350	-	104	46	69	-	150	46	32
NJD2	-	427	420	350	-	1	9	7	-	9	1	58
NJD3	-	390	390	-	-	117	23	-	-	50	650	-
NJD4	560	437	390	-	52	5	11	-	240	61	2050	-
NJE1	119	754	240	200	1	0.1	1	16	20	1	17	18
NJE2	320	367	240	150	0	-	7	1	60	1	1	11
NJF1	38	157	70	75	2	2	8	9	30	112	145	49
NJF2	-	68	40	16	-	154	109	92	-	4600	6100	492

A = November 28, 1976; B = April 6, 1977; C = June 2, 1977; D = August 5, 1977.

K16

TABLE K2 (Continued)

Sample Code	Ca, mg/l				Cd, µg/l				Cu, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
NJG1	111	320	-	80	10	3	4	28	790	250	15	20
NJG2	152	367	15	100	4	1	-	2	20	54	-	-
NJH1	40	19	250	54	1	1	1	21	-	37	8	40
NJH2	-	27	20	11	-	2	10	135	-	99	191	786
NJI	2	16	140	3	1	104	67	5	20	2100	3100	1320
NJJ	10	.6	10	27	0.1	5	69	147	60	2600	1400	330

K17

TABLE K2 (Continued)

Sample Code	Fe, mg/l				Hg, ug/l				K, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
NJA1	ND	0.044	0.006	-	-	0.1	0.07	-	-	185	259	-
NJA2	-	0.015	0.22	0.046	-	0.8	0.2	0.4	-	201	228	251
NJA3	49.6	0.056	0.144	-	0.0	0.4	1.0	-	861	162	274	-
NJA4	0.39	0.038	0.082	-	0.2	0.8	0.4	-	859	135	296	-
NJB1	-	0.019	0.007	0.006	-	0	0.04	0.02	-	208	259	274
NJB2	-	0.152	0.014	0.005	-	0.26	0.00	0.13	-	182	236	266
NJB3	-	0.106	0.20	0.085	-	0.48	0.5	0.31	-	181	259	198
NJB4	72.4	0.073	-	0.085	0.1	0.08	-	0.9	959	209	-	198
NJC1	-	0.018	0.076	-	-	0	0.2	-	-	244	251	-
NJC2	-	0.102	0.008	0.100	-	0	0.9	-	769	232	243	-
NJC3	0.40	0.023	0.011	-	0.1	0	0.9	-	769	232	243	-
NJC4	0.35	0.061	0.020	-	0.3	0.3	0	-	740	279	198	-
NJD1	-	0.017	0.128	0.106	-	0.008	0	0.01	-	162	183	236
NJD2	-	-	47.1	0.220	-	-	0	-	-	154	175	228
NJD3	-	0.056	13.1	-	-	0.08	0	-	-	142	180	-
NJD4	220	0.025	63.6	-	0.1	0.2	1.6	-	698	99	183	-
NJE1	0.31	0.89	0.040	0.021	0.1	0.56	0.03	0.12	680	240	198	206
NJE2	0.24	-	0.016	0.036	0.0	0.68	0.3	0.15	441	75	50	38
NJF1	6.1	0.139	0.162	0.212	0.2	0.6	1.3	0.8	438	83	115	110
NJF2	-	-	0.174	0.220	-	0.9	0.3	0.7	-	18	28	43

TABLE K2 (Continued)

Sample Code	Fe, mg/l				Hg, µg/l				K, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
NJG1	71.6	0.29	-	0.096	0.1	0.28	ND	-	480	54	90	78
NJG2	13.8	-	0.004	0.110	0.2	0.48	-	-	650	75	-	80
NJH1	1.6	0.058	0.024	0.144	0.1	0.4	ND	-	219	61	184	73
NJH2	-	0.027	0.004	0.062	-	0	ND	ND	-	12	20	27
NJI	38.8	-	5.9	0.288	0.1	0.32	ND	0.03	29	8	37	2
NJJ	2500	-	685	0.166	0.0	0.32	0.2	0.05	923	11	<1	2

K19

K20

TABLE K 2 (Continued)

Sample Code	Mg, mg/l				Mn, mg/l				Ni, ug/l			
	A	B	C	D	A	B	C	D	A	B	C	D
NJA1	-	818	820	-	-	2.8	5.0	-	-	570	298	-
NJA2	-	800	760	640	-	3.1	4.6	12.6	-	730	180	113
NJA3	560	629	840	-	5.5	2.2	5.0	-	100	420	177	-
NJA4	552	606	940	-	4.9	2.2	3.6	-	63	420	115	-
NJB1	-	790	780	700	-	8.4	9.0	4.0	-	890	378	30
NJB2	-	744	-	700	-	7.5	7.3	8.9	-	890	305	80
NJB3	-	734	600	360	-	-	8.3	4.0	-	350	445	14
NJB4	624	720	-	440	5.4	2.3	-	1.3	100	420	-	30
NJC1	-	986	1020	-	-	6.9	6.8	-	-	890	226	-
NJC2	-	1040	1010	195	-	6.2	6.4	0.7	-	730	153	105
NJC3	440	1050	910	-	2.6	6.0	8.6	-	80	1040	186	-
NJC4	468	1050	790	-	3.9	5.9	9.5	-	100	890	135	-
NJD1	-	622	710	680	-	4.4	6.2	12.6	-	800	505	270
NJD2	-	762	650	700	-	6.4	7.2	11.7	-	1200	526	270
NJD3	-	664	690	0	-	4.8	7.8	-	-	650	290	-
NJD4	448	594	670	0	16.2	5.2	9.5	-	510	810	304	-
NJE1	396	734	580	600	2.7	2.7	1.7	2.8	390	490	45	7
NJE2	293	370	90	60	4.3	-	2.1	1.5	90	340	62	8

TABLE K 2 (Continued)

Sample Code	Mg, mg/l				Mn, mg/l				Ni, µg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
NJF1	259	398	140	175	0.6	1.1	0.91	0.5	140	570	104	28
NJF2	-	29	50	110	-	2.0	1.9	1.1	-	490	355	134
NJG1	341	314	160	165	22.2	4.8	4.11	4.0	920	420	142	37
NJG2	504	440	-	190	15.6	11.1	-	3.5	460	450	-	75
NJH1	112	68	550	85	1.2	7.3	45	11.7	150	-	50	54
NJH2	-	20	15	15	-	20	3.3	9.7	-	340	119	163
NJI	16	35	120	4	2.3	7.8	14.0	0.5	80	420	370	100
NJJ	362	40	140	70	36.7	2.6	21.6	10.5	1790	340	628	390

K21

K22

Table
TABLE K2 (Continued)

Sample Code	Pb, $\mu\text{g/l}$				Na, mg/l				Zn, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
NJA1	-	16	7	-	-	3456	5400	-	-	2.22	5.06	-
NJA2	-	27	9	-	-	4444	5000	-	-	2.38	3.28	0.34
NJA3	34	12	13	-	3730	3838	5800	-	0.32	0.59	2.48	-
NJA4	33	7	1	-	3940	3535	6700	-	0.37	1.6	1.24	-
NJB1	-	28	7	1	-	3300	5000	6400	-	5.81	4.96	0.12
NJB2	-	27	5	1	-	3737	5000	6400	-	6.48	4.08	0.90
NJB3	-	10	9	4	-	3256	4600	4000	-	0.18	5.04	0.62
NJB4	34	16	-	5	4200	2970	--	4600	0.15	0.141	-	0.14
NJC1	-	39	9	-	-	2856	5000	-	-	4.55	2.38	-
NJC2	-	13	8	6	-	3456	5400	2000	-	0.185	0.72	0.34
NJC3	31	31	12	-	3390	5858	5400	3700	0.20	3.80	0.66	-
NJC4	31	19	11	-	2980	4256	4700	-	0.15	4.16	0.79	-
NJD1	-	15	11	3	-	2900	4300	6800	-	4.47	3.60	1.36
NJD2	-	18	11	3	-	3200	4300	6400	-	3.87	1.32	-
NJD3	-	15	15	-	-	2640	4300	-	-	3.27	2.56	-
NJD4	17	22	14	-	3300	2770	4600	-	2.38	1.41	1.82	-
NJE1	21	14	12	-	3000	3440	4600	5400	0.22	0.019	0.005	0.08
NJE2	12	2	4	3	1570	900	700	500	0.14	0.200	0.002	0.30
NJF1	13	1	11	10	2000	1640	2000	2300	0.22	0.74	0.59	0.18
NJF2	-	1	2	5	-	121	300	1000	-	77.3	10.8	3.96

TABLE K2 (Continued)

Sample Code	Pb, ug/l				Na, mg/l				Zn, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
NJG1	20	2	8	6	1050	640	1700	1500	8.58	1.93	0.64	0.58
NJG2	16	-	-	6	2670	1000	-	1300	3.97	2.23	-	0.10
NJH1	50	2	14	5	1100	600	4300	900	-	0.032	0.004	1.08
NJH2	-	1	<1	2	-	32	103	30	0.06	0.81	1.58	4.40
NJI	20	2	6	32	70	55.1	1000	25	0.23	5.0	6.9	0.40
NJJ	10	7	4	16	790	220	1700	300	0.98	1.63	7.6	7.36

K23

TABLE K2 (Continued)

Sample Code	Cl, mg/l				Atk., mg/l				TOC, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
NJA1	-	7433	9294	-	-	16	77	-	-	39	25	-
NJA2	-	7581	-	-	-	9	24	-	-	31	15	-
NJA3	-	6408	11520	-	-	132	235	-	-	60	180	-
NJA4	7817	5946	12188	-	72	167	338	-	15	90	220	-
NJB1	-	6562	9405	11131	-	18	154	-	-	15	90	100
NJB2	-	6562	8793	11243	-	4	31	672	-	20	35	90
NJB3	-	6049	9072	-	-	7	139	382	-	30	92	90
NJB4	9328	7690	8237	9072	344	572	816	-	390	230	490	350
NJC1	-	9893	10797	-	-	132	365	-	-	60	180	60
NJC2	-	9612	10686	3673	-	506	533	191	-	205	280	120
NJC3	8025	9355	10352	-	794	57	444	493	180	29	260	-
NJC4	8129	9304	8682	-	612	48	566	-	285	36	280	-
NJD1	-	4768	7346	10129	-	106	240	130	-	55	140	75
NJD2	-	6459	7402	8916	-	57	24	40	-	35	27	36
NJD3	-	4511	8682	-	-	70	24	-	-	45	32	-
NJD4	6931	4819	8793	-	ND	70	ND	-	25	40	35	-
NJE1	5732	-	9752	-	700	1276	1430	-	550	460	780	-
NJE2	-	1876	1224	790	-	343	216	100	0	150	165	60
NJF1	-	-	3728	2896	-	40	20	160	-	52	96	155
NJF2	-	2020	2059	1781	-	ND	ND	50	-	17	15	47

TABLE K2 (Continued)

Sample Code	Cl, mg/l				Alk., mg/l				TOC, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
NJG1	1668	-	-	1781	ND	57	178	-	10	20	120	-
NJG2	-	1511	-	-	-	ND	-	-	-	18	-	-
NJH1	2189	938	2560	1224	300	70	336	130	170	35	295	80
NJH2	-	61	143	69	-	20	10	10	-	11	1	7
NJI	168	138	-	101	ND	ND	ND	10	25	9	12	4
NJJ	1407	70	-	534	ND	ND	ND	10	90	ND	12	9

K25

TABLE K2 (Continued)

Sample Code	pH				Eh, mV				SO ₄ , mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
NJA1	-	5.2	5.6	5.5	-	285	62	80	-	2750	2800	-
NJA2	-	5.6	5.1	-	-	182	200	-	-	3050	2700	-
NJA3	6.3	6.1	6.2	-	-	140	15	-	-	2750	2550	-
NJA4	6.2	6.1	6.2	-	-	100	-40	-	1801	2750	2200	-
NJB1	-	5.7	5.1	5.7	-	365	310	250	-	3300	3600	1800
NJB2	-	6.0	5.3	5.3	-	190	100	190	-	4000	3300	1763
NJB3	-	6.3	5.8	6.2	-	140	-20	110	-	3300	2375	1150
NJB4	6.3	6.4	5.9	6.7	-	-100	-180	120	1836	1800	1350	925
NJC1	-	6.3	5.4	-	-	260	11	-	-	4213	2900	-
NJC2	-	6.3	6.5	6.5	-	270	-60	55	-	2375	-	313
NJC3	6.8	6.2	5.9	5.7	-	350	-90	120	843	4000	-	1775
NJC4	6.7	6.3	5.9	-	-	290	-44	-	980	3700	2200	-
NJD1	-	7.3	5.2	6.0	-	230	14	4	-	2450	3250	2800
NJD2	-	7.7	5.4	5.3	-	315	-4	130	-	3150	3100	3500
NJD3	-	6.3	5.2	-	-	46	-16	-	-	2750	3100	-
NJD4	4.1	6.7	5.3	-	-	130	-6	-	2589	2750	2400	-
NJE1	6.6	6.0	5.6	7.2	-	-75	-90	-	1117	450	38	-
NJE2	6.4	6.4	6.3	6.8	-	160	-61	230	-	1400	825	825
NJF1	5.8	6.4	5.8	6.4	-	-52	-120	14	-	700	400	350
NJF2	-	5.6	4.2	5.3	-	150	180	90	-	600	275	288

TABLE K2 (Continued)

Sample Code	pH				Eh, mV				SO ₄ , mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
NJG1	3.0	4.7	5.5	6.4	-	2	-80	42	3239	1600	900	-
NJG2	5.6	4.6	4.8	5.6	-	120	135	10	-	2600	-	-
NJH1	6.5	6.3	6.0	5.8	-	-50	0110	170	440	500	288	525
NJH2	-	5.8	6.4	5.5	-	200	120	180	-	450	225	325
NJI	3.0	4.3	2.8	4.6	-	210	380	320	500	600	-	75
NJJ	3.0	2.8	3.4	7.2	-	210	240	320	6600	8500	5100	1100

K27

TABLE K2 (Continued)

Sample Code	TIC, mg/l				TC, mg/l				P, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
NJA1	-	11	30	-	-	50	55	-	-	-	ND	-
NJA2	-	9	25	-	-	40	40	-	-	-	ND	-
NJA3	-	40	40	-	-	100	220	-	-	-	-	-
NJA4	40	55	100	-	55	145	320	-	0.006	-	ND	-
NJB1	-	10	35	190	-	25	125	290	-	0.04	ND	0.07
NJB2	-	5	20	110	-	25	55	200	-	-	ND	0.065
NJB3	-	10	28	90	-	40	120	180	-	0.009	ND	0.02
NJB4	110	180	190	450	500	410	680	800	0.004	-	ND	0.01
NJC1	-	40	90	-	-	100	270	-	-	-	ND	-
NJC2	-	150	110	50	-	355	390	110	-	-	ND	0.04
NJC3	200	11	100	170	380	40	360	290	-0.019	0.013	0.01	0.01
NJC4	165	14	120	-	450	50	400	-	0.011	0.003	0.02	-
NJD1	-	35	53	55	-	90	190	130	-	-	ND	0.025
NJD2	-	10	3	4	-	45	30	40	-	-	0.02	0.07
NJD3	-	40	8	-	-	85	40	-	-	0.004	0.015	-
NJD4	25	40	10	-	50	80	45	-	0.008	-	ND	-
NJE1	200	340	360	-	750	800	1140	-	0.19	-	0.01	-
NJE2	-	120	60	40	-	270	225	100	-	0.01	ND	ND
NJF1	-	18	4	5	-	70	100	160	-	-	ND	0.03
NJF2	0	1	5	3	-	18	20	50	-	0.037	ND	0.01

K28

TABLE K2 (Concluded)

Sample Code	TIC, mg/l				TC, mg/l				P, mg/l			
	A	R	C	D	A	R	C	D	A	B	C	D
NJG1	20	20	40	-	30	40	160	-	0.047	-	ND	0.39
NJG2	-	ND	-	-	-	18	-	-	-	-	-	-
NJH1	90	30	85	50	260	65	380	130	0.006	-	0.01	0.01
NJH2	-	1	2	3	-	12	3	10	-	0.007	-	0.01
NJI	30	1	3	1.5	55	10	15	10	ND	-	0.02	ND
NJJ	20	ND	8	6	110	ND	20	10	0.043	0.007	-	0.11

K29

TABLE K3

LEACHATE/INTERSTITIAL WATER: HOUSTON, TEXAS, SITE

Element Sample	CA, mg/l				Mg, mg/l			
	A	B	C	D	A	B	C	D
HA-1	---	368	---	---	---	265	---	---
HA-2	276	230	205	205	270	155	100	131
HA-3	418	300	330	300	254	218	195	237
HA-4	420	263	370	330	260	182	215	285
HB-1	---	455	580	---	---	520	427	---
HB-2	916	432	750	275	384	358	425	187
HB-3	1,020	522	790	450	381	433	420	463
HB-4	791	420	470	390	640	525	475	784
HC-1	---	---	---	---	---	---	---	---
HC-2	622	462	540	445	360	300	345	480
HC-3	524	450	455	350	420	345	355	469
HC-4	752	460	455	400	532	845	585	688
HD-1	---	312	500	---	---	445	440	---
HD-2	884	600	750	400	356	322	410	421
HD-3	791	350	430	430	372	499	420	442
HD-4	739	570	750	460	400	378	435	483
HE-1	---	332	245	---	---	377	365	---
HE-2	---	314	245	---	---	375	360	---
HF-1	360	304	275	365	332	295	325	421
HF-2	390	295	275	430	344	295	330	431
HG-1	---	218	---	395	---	282	---	413
HG-2	156	218	---	440	330	280	---	448
HH-1	---	275	---	---	---	320	---	---
HH-2	171	285	245	380	408	432	410	484
HI	152	348	455	395	452	418	455	464
HJ	---	355	330	305	---	425	425	443

A - Sampling data 12/1
 B - Sampling date 3/25
 C - Sampling date 6/12
 D - Sampling date 7/3
 - No sample available

(Continued)

TABLE K3. (Continued)

Element Sample	K, mg/l				Na, mg/l			
	A	B	C	D	A	B	C	D
HA-1	---	23	---	---	---	1025	---	---
HA-2	322	13	28	38	1210	725	650	800
HA-3	343	23	50	62	1410	1025	1100	1400
HA-4	329	20	61	68	1410	950	1200	1600
HB-1	---	36	58	---	---	2125	1750	---
HB-2	480	63	84	34	2290	2400	2650	1100
HB-3	480	82	101	99	2090	2750	2750	2900
HB-4	677	143	135	184	4030	4500	3500	4850
HC-1	---	---	---	---	---	---	---	---
HC-2	500	42	57	162	2130	1600	1670	4100
HC-3	559	63	80	125	2090	2300	2325	3200
HC-4	638	135	184	166	3560	3625	4300	4200
HD-1	---	90	91	---	---	2500	2200	---
HD-2	509	63	85	77	1920	1750	1850	2300
HD-3	479	65	80	74	2200	2225	2250	2400
HD-4	511	68	98	90	2291	2525	2500	2600
HE-1	---	49	75	---	---	2650	2800	---
HE-2	---	51	80	---	---	2750	2800	---
HF-1	500	50	80	90	2590	2580	2750	3200
HF-2	480	48	81	103	2900	2525	2500	3200
HG-1	---	41	---	115	---	2100	---	2600
HG-2	480	80	---	118	2130	1998	---	2700
HH-1	---	42	---	---	---	2415	---	---
HH-2	563	47	68	74	2500	2325	2200	2700
HI	610	56	88	79	2510	2530	2800	2800
HJ	---	59	80	66	---	2825	2300	2800

A - Sampling date 12/1
 B - Sampling date 3/25
 C - Sampling date 6/12
 D - Sampling date 7/3
 - No sample available

(Continued)

TABLE K3 (Continued)

Element Sample	Mn, mg/l				Fe, mg/l			
	A	B	C	D	A	B	C	D
HA-1	---	3.2	---	---	---	.004	---	---
HA-2	3.7	3.6	2.3	0.2	0.27	.003	.007	0.0225
HA-3	3.6	5.3	3.2	0.9	0.33	.004	.017	0.075
HA-4	3.6	4.4	3.5	1.7	0.30	.008	.040	0.038
HB-1	---	11.6	2.0	---	---	.004	.004	---
HB-2	22.5	16.0	3.6	4.3	0.35	.002	---	0.030
HB-3	25.0	11.8	12.2	3.8	0.30	.046	.065	0.038
HB-4	13.2	7.5	5.4	4.6	0.43	.019	.057	0.045
HC-1	---	---	---	---	---	---	---	---
HC-2	9.7	10.0	8.5	5.2	0.35	.006	.013	0.070
HC-3	7.8	11.0	9.4	6.8	0.32	.014	.005	0.038
HC-4	9.0	7.6	5.6	2.9	0.35	.127	.057	0.045
HD-1	---	5.5	11.4	---	---	.003	.005	---
HD-2	19.5	19.3	21.2	0.2	0.43	.006	.005	0.028
HD-3	24.8	43.8	30.0	15.5	0.35	.012	.005	0.038
HD-4	27.0	21.7	18.7	12.1	0.43	.750	.036	---
HE-1	---	3.2	8.3	---	---	.011	.004	---
HE-2	---	3.7	10.3	---	---	.005	.010	---
HF-1	18.0	13.5	12.5	2.3	0.35	.004	.010	1.100
HF-2	18.4	18.0	16.0	4.7	0.35	.006	.015	0.030
HG-1	---	22.8	---	0.7	---	.005	---	0.038
HG-2	6.6	13.7	---	5.5	0.31	.007	---	0.030
HH-1	---	10.0	---	---	---	.008	---	---
HH-2	33.0	47.5	39.2	42.0	0.30	.004	---	0.038
HI	3.7	23.8	21.0	5.1	0.30	.058	.55	0.050
HJ	---	30.0	19.0	5.5	---	.003	.016	0.070

A - Sampling date 12/1
 B - Sampling date 3/25
 C - Sampling date 6/12
 D - Sampling date 7/3
 - No sample available

(Continued)

TABLE K3. (Continued)

Element Sample	Cu, µg/l				Zn, mg/l			
	A	B	C	D	A	B	C	D
HA-1	--	36	--	--	---	.006	--	--
HA-2	10	25	8	7	0.11	1.20	--	0.34
HA-3	10	27	6	9	0.14	.013	--	0.06
HA-4	10	33	2	4	0.09	.026	--	0.24
HB-1	10	72	24	--	---	.017	--	--
HB-2	10	102	5	5	0.14	--	--	0.03
HB-3	10	101	6	13	0.16	.005	--	0.29
HB-4	20	165	6	9	0.11	.019	--	0.03
HC-1	---	---	--	--	---	--	--	--
HC-2	10	67	10	9	0.11	.085	--	0.05
HC-3	20	73	5	9	0.08	.077	--	0.03
HC-4	20	79	6	7	0.12	.002	--	0.02
HD-1	--	58	15	--	---	.022	--	--
HD-2	20	88	7	6	0.11	.026	--	0
HD-3	10	43	4	10	0.11	.009	--	0.02
HD-4	10	77	5	9	0.11	.100	--	0.05
HE-1	--	59	8	--	---	.005	--	--
HE-2	--	43	6	--	---	.004	--	--
HF-1	20	48	6	10	0.19	.019	--	0.04
HF-2	30	42	4	13	0.14	.008	--	0.04
HG-1	--	21	--	10	----	.010	--	0.04
HG-2	20	24	--	5	0.24	.004	--	0.02
HH-1	--	37	--	--	----	.080	--	--
HH-2	20	41	3	10	1.10	.039	--	0.06
HI	20	58	5	4	0.08	.012	--	0.07
HJ	--	56	6	8	----	.011	--	0.02

A - Sampling date 12/1
 B - Sampling date 3/25
 C - Sampling date 6/12
 D - Sampling date 7/3
 - No sample available

(Continued)

TABLE K3. (Continued)

Element Sample	Cd, mg/l				Ni, mg/l			
	A	B	C	D	A	B	C	D
HA-1	---	0.4	---	---	---	5	--	--
HA-2	1.0	0.4	0.3	0.7	47	3	8	10
HA-3	1.0	0.3	0.4	0.5	6	3	9	8
HA-4	1.0	0.8	0.3	1.2	10	4	7	7
HB-1	---	0.4	0.6	---	---	9	14	--
HB-2	1.0	0.7	0.1	0.8	7	4	4	8
HB-3	1.0	0.8	0.2	1.3	9	2	5	19
HB-4	1.0	0.9	0.2	0.7	.18	4	5	17
HC-1	---	---	---	---	---	--	--	--
HC-2	1.0	1.0	0.2	2.0	14	77	9	10
HC-3	1.0	0.3	0.2	1.3	13	3	8	11
HC-4	1.0	0.4	0.4	1.0	5	5	7	10
HD-1	---	1.2	1.2	---	---	3	52	--
HD-2	1.0	0.5	0.3	0.6	1.0	8	7	8
HD-3	1.0	3.2	0.2	0.8	8	3	3	19
HD-4	1.0	0.4	0.4	1.8	6	5	4	23
HE-1	---	1.2	0.2	---	---	4	18	--
HE-2	---	1.0	0.8	---	---	4	15	--
HF-1	2.0	0.8	0.2	0.8	10	6	11	30
HF-2	6.0	0.8	0.2	1.3	23	6	12	22
HG-1	---	0.7	---	---	---	5	--	20
HG-2	8.0	0.7	---	1.0	11	8	--	10
HH-1	---	0.9	---	---	---	6	--	--
HH-2	1.0	1.4	0.4	1.0	83	8	19	22
HI	1.0	0.6	0.2	1.0	46	9	12	17
HJ	---	2.4	0.2	1.0	---	12	11	19

A - Sampling date 12/1
 B - Sampling date 3/25
 C - Sampling date 6/12
 D - Sampling date 7/3
 - No sample available

(Continued)

TABLE K3. (Continued)

Element Sample	pH				Eh, mV			
	A	B	C	D	A	B	C	D
HA-1	--	6.83	---	---	---	---	---	---
HA-2	6.76	6.33	6.7	6.5	---	---	-60	-69
HA-3	6.79	6.26	6.5	6.2	---	---	-40	-2.4
HA-4	7.18	6.85	6.7	7.3	---	---	+60	-45
HB-1	--	7.98	7.4	---	---	---	+30	---
HB-2	6.90	6.46	6.5	5.9	---	---	+90	20
HB-3	6.87	6.94	6.7	6.4	---	---	+200	190
HB-4	7.08	6.46	6.3	6.5	---	---	+30	25
HC-1	--	---	---	---	---	---	---	---
HC-2	7.19	6.34	7.0	7.3	---	---	+20	-100
HC-3	7.23	6.69	---	---	---	---	---	---
HC-4	7.10	6.90	7.5	5.6	---	---	-40	-10
HD-1	--	7.24	6.6	---	---	---	+80	---
HD-2	7.13	6.85	8.0	5.6	---	---	+210	350
HD-3	7.22	6.20	6.8	5.8	---	---	+50	50
HD-4	7.90	6.39	7.5	5.6	---	---	-100	+70
HE-1	--	6.77	7.3	---	---	---	+50	---
HE-2	--	6.62	6.4	8.1	---	---	+100	15
HF-1	7.53	6.15	6.4	7.2	---	---	+150	10
HF-2	7.24	6.47	7.1	8.1	---	---	-10	35
HG-1	--	7.10	---	7.4	---	---	---	-5
HG-2	7.05	7.03	---	8.2	---	---	---	57
HH-1	--	6.37	---	7.4	---	---	---	5
HH-2	6.98	6.21	6.8	7.5	---	---	+60	65
HI	7.54	6.88	6.8	6.8	---	---	+50	30
HJ	--	6.92	6.2	7.6	---	---	+20	58

A - Sampling date 12/1
 B - Sampling date 3/25
 C - Sampling date 6/12
 D - Sampling date 7/3
 - No sample available

(Continued)

TABLE K3. (Continued)

Element Sample	Pb, µg/l				Hg, µg/l			
	A	B	C	D	A	B	C	D
HA-1	--	2.4	---	--	--	0	--	--
HA-2	80.0	1.9	1.5	6	0.06	--	0.90	--
HA-3	80.0	2.6	2.8	7	0.22	1.20	0.05	--
HA-4	70.0	2.6	2.2	5	0.06	0.90	0.36	--
HB-1	--	4.9	2.0	--	--	0	0.33	--
HB-2	160.	8.7	3.0	3	1.24	1.30	0.20	--
HB-3	120.	8.9	2.4	3	1.10	0	0	--
HB-4	280.	5.5	2.4	5	0.06	0.53	0.10	--
HC-1	--	--	---	--	--	--	--	--
HC-2	21.0	1.3	2.1	3	0.30	2.40	0.13	--
HC-3	20.0	5.0	1.4	4	0.07	0.35	0	--
HC-4	20.0	6.2	1.5	4	0.23	1.10	0.85	--
HD-1	--	0.7	2.3	--	--	4.65	0	--
HD-2	130.	1.0	1.8	1	0.11	10.8	0	--
HD-3	200.	0.6	2.0	1	0.22	1.10	0	--
HD-4	210.	0.3	1.2	2	0.20	1.85	0	--
HE-1	--	6.2	1.3	--	--	0.20	--	--
HE-2	--	1.0	1.2	--	--	1.10	0	--
HF-1	200.	7.0	1.5	1	0.10	0.14	0.05	--
HF-2	240.	7.1	1.6	1	0.10	0.80	0	--
HG-1	--	5.5	---	1	--	0.07	--	--
HG-2	180.	4.8	---	1	0.08	0.20	--	--
HH-1	--	5.4	---	--	--	--	--	--
HH-2	170.	4.0	1.5	3	0.08	0.32	0	--
HI	120.	4.8	1.9	1	0.19	0	0	--
HJ	--	5.4	1.0	2	--	0	0.05	--

A - Sampling date 12/1
 B - Sampling date 3/25
 C - Sampling date 6/12
 D - Sampling date 7/3
 - No sample available

(Continued)

TABLE K3. (Continued)

Element Sample	Sulfate mg/l				Chloride, mg/l			
	A	B	C	D	A	B	C	D
HA-1	---	---	---	---	---	---	---	---
HA-2	575	675	165	---	3179	2229	1198	---
HA-3	184	600	24	250	2970	2293	2084	2571
HA-4	137	---	170	---	2970	---	2188	2772
HB-1	---	---	555	---	---	---	4221	---
HB-2	144	48	75	80	5628	4844	5159	2215
HB-3	168	75	200	10	5263	5408	5471	4965
HB-4	21	55	0	1.5	8963	8612	6201	8794
HC-1	---	---	---	144	---	---	---	---
HC-2	300	385	225	---	4334	3768	3595	3776
HC-3	69	290	140	4.8	6410	4716	4481	5443
HC-4	100	50	2.5	5.5	7452	7556	8233	7681
HD-1	---	---	525	---	---	---	4794	---
HD-2	55	160	380	31	5.54	4460	4533	4998
HD-3	283	1000	420	425	5419	5380	4585	5065
HD-4	283	280	245	475	5367	5075	4898	5321
HE-1	---	---	250	---	---	---	4690	---
HE-2	---	---	330	475	---	---	4481	5221
HF-1	---	305	420	88	---	5357	4950	5699
HF-2	---	650	200	238	---	5993	5106	---
HG-1	---	750	---	1388	---	4511	---	4341
HG-2	---	988	---	938	---	4203	---	4319
HH-1	---	---	---	1075	---	---	---	4664
HH-2	---	813	1000	700	---	5023	4168	4486
HI	---	1100	490	250	---	4767	4950	5042
HJ	---	---	380	357	---	---	---	5009

A - Sampling date 12/1
 B - Sampling date 3/25
 C - Sampling date 6/12
 D - Sampling date 7/3
 - No sample available

(Continued)

TABLE K3. (Continued)

Element Sample	Alk, mg/l				TOC, mg/l			
	A	B	C	D	A	B	C	D
HA-1	---	---	---	---	---	---	---	---
HA-2	707	559	256	---	30	45	150	---
HA-3	1300	---	1229	747	110	40	760	240
HA-4	1300	---	943	1049	120	----	630	315
HB-1	---	---	408	---	---	---	245	---
HB-2	972	1606	1800	465	100	70	1070	90
HB-3	1392	1967	1517	1-17	70	110	920	315
HB-4	2056	2169	2275	2294	260	200	1190	540
HC-1	---	---	---	---	---	---	---	---
HC-2	1108	713	874	738	110	30	620	600
HC-3	1732	1078	1152	738	110	40	745	420
HC-4	1800	2385	2270	2280	260	100	370	230
HD-1	---	---	557	---	---	---	400	---
HD-2	---	691	250	496	40	30	180	150
HD-3	828	1179	797	855	10	55	575	270
HD-4	1152	1676	1625	923	280	130	1090	330
HE-1	---	---	626	---	---	---	410	---
HE-2	---	---	768	667	---	---	555	220
HF-1	---	792	696	1020	---	45	485	350
HF-2	---	761	1003	870	---	30	630	290
HG-1	---	616	---	604	---	40	---	230
HG-2	---	757	---	1077	---	35	---	355
HH-1	---	---	---	556	---	---	---	170
HH-2	---	1131	1061	929	---	40	695	290
HI	---	1052	898	1035	---	100	620	365
HJ	---	---	614	790	---	---	400	230

A - Sampling date 12/1
 B - Sampling date 3/25
 C - Sampling date 6/12
 D - Sampling date 7/3
 - No sample available

(Continued)

TABLE K3. (Continued)

Element Sample	TIC, mg/l				Total Carbon, mg/l			
	A	B	C	D	A	B	C	D
HA-1	---	---	---	---	---	---	---	---
HA-2	200	11-	60	---	230	155	210	---
HA-3	270	150	260	190	380	190	1020	430
HA-4	260	---	240	245	380	---	870	560
HB-1	---	---	110	---	---	---	355	---
HB-2	210	350	400	110	310	420	1470	200
HB-3	270	430	330	245	340	540	1250	560
HB-4	240	530	530	540	600	730	1720	1080
HC-1	---	---	---	---	---	---	---	---
HC-2	250	150	200	480	360	180	820	1080
HC-3	400	190	255	290	510	230	1000	710
HC-4	380	510	540	170	640	610	910	400
HD-1	---	---	100	---	---	---	510	---
HD-2	100	170	60	110	140	200	240	260
HD-3	190	275	200	200	200	330	775	470
HD-4	220	320	350	210	500	450	1440	540
HE-1	---	---	160	---	---	---	570	---
HE-2	---	---	180	140	---	---	735	340
HF-1	---	2-5	165	210	---	250	650	560
HF-2	---	200	240	210	---	230	870	500
HG-1	---	100	---	110	---	200	---	340
HG-2	---	125	---	245	---	160	---	600
HH-1	---	---	---	130	---	---	---	300
HH-2	---	250	255	210	---	290	950	500
HI	---	90	210	235	---	190	830	600
HJ	---	---	160	200	---	---	560	430

A - Sampling date 12/1
 B - Sampling date 3/25
 C - Sampling date 6/12
 D - Sampling date 7/3
 - No sample available

(Continued)

TABLE K3. (Concluded)

Sample	Element Phosphate, mg/l			
	A	B	C	D
HA-1	---	---	--	----
HA-2	0.019	---	0.01	---
HA-3	0.054	---	0.10	---
HA-4	0.023	---	0	0.075
HB-1	---	---	0.32	---
HB-2	0.099	---	0.36	---
HB-3	0.012	---	0	0.04
HB-4	---	---	0.2	0.42
HC-1	---	---	--	---
HC-2	0.128	---	0.03	0.14
HC-3	---	---	0.06	0.91
HC-4	0.59	---	0.55	0.335
HD-1	---	---	--	---
HD-2	0.011	---	0.02	---
HD-3	0.054	---	0	0.1
HD-4	0.015	---	0.11	0.04
HE-1	---	---	--	---
HE-2	---	---	--	---
HF-1	---	---	0.01	0.035
HF-2	---	---	0.22	0
HG-1	---	---	--	---
HG-2	---	---	--	0.570
HH-1	---	---	--	---
HH-2	---	---	0.02	0.09
HI	---	---	0	0.065
HJ	---	---	--	0.065

A - Sampling date 12/1
 B - Sampling date 3/25
 C - Sampling date 6/25
 D - Sampling date 7/3
 - No sample available

TABLE K4
LEACHATE/INTERSTITIAL WATER: PINTO ISLAND, ALABAMA, SITE

Sample Code	Ca, mg/l				Mg, mg/l				K, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
PA1	-	-	86	166	-	75	79	118	--	52	64	75
PA2	340	70	51	278	489	124	101	465	210	71	80	141
PA3	345	120	170	302	480	312	317	503	200	129	169	181
PA4	350	125	150	278	470	300	296	378	200	130	154	161
PB1	-	78	-	263	-	103	-	212	-	41	-	96
PB2	375	155	124	-	500	287	178	-	200	91	112	-
PB3	440	165	136	-	950	287	178	-	330	92	112	-
PB4	345	245	93	198	550	487	117	252	200	140	112	106
PC1	9	30	68	-	20	10	22	-	8	6	21	-
PC2	32	38	25	164	40	52	26	174	20	36	44	73
PC3	63	67	35	231	120	105	73	242	44	52	66	88
PC4	63	65	35	150	120	144	73	182	40	53	65	75
PD1	-	69	126	189	-	25	26	47	-	7	12	25
PD2	57	78	101	198	18	22	26	42	10	23	30	58
PD3	35	109	157	-	40	110	192	-	19	53	122	-
PD4	29	167	157	320	12	131	143	218	17	52	112	106

A = January 17, 1977; B = March 26, 1977; C = June 7, 1977; D = August 1, 1977.

TABLE K4 (Continued)

Sample Code	Ca, mg/l				Mg, mg/l				K, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
PE1	110	162	151	-	74	105	109	-	30	17	52	-
PE2	150	-	157	166	93	118	133	140	48	33	56	75
PFT	53	56	20	-	13	9	8	-	4	180	4	-
PF2	100	53	45	-	17	10	15	-	7	165	27	-
PG1	-	-	2	-	-	-	8	-	-	-	13	-
PG2	-	26	8	-	4	9	6	-	10	9	15	-
PH1	57	-	15	-	15	-	16	-	10	-	6	-
PH2	59	84	68	81	22	20	2	20	3	15	18	20
PI	56	45	61	-	9	15	34	-	8	10	3	-
PJ	55	21	-	81	2	1	-	40	2	1	-	3

K42

TABLE K4 (Continued)

Sample Code	Na, mg/l				Mn, mg/l				Fe, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
PA1	-	900	546	1061	--	2.82	1.6	6.2	-	230	25	34
PA2	4500	1450	1144	2211	25.3	3.76	2.6	15.6	15	68	165	3
PA3	3900	3250	2596	3136	24.4	4.16	5.3	14.4	7	65	67	12
PA4	3700	3200	2266	2653	36.2	6.50	2.8	9.8	7	120	20	4
PB1	--	700	-	1485	-	2.70	--	0.066	-	28	-	12
PB2	5800	2400	1936	-	68.1	21.0	19.5	-	5	99	55	-
PB3	5250	2400	1892	-	68.2	20.0	14.0	-	4	8	30	-
PB4	5800	3950	1826	1888	53.6	27.0	12.3	10.4	4	16	25	210
PC1	95	37	196	-	0.8	0.70	1.3	-	800	11	12	-
PC2	553	750	440	2211	2.1	2.24	2.3	6.4	11	16	25	13
PC3	1000	1150	836	1364	2.1	2.81	1.5	10	11	14	10	3
PC4	1155	1250	836	1212	0.5	2.88	1.0	4.2	10	34	12	5
PD1	-	19	52	134	-	1.43	0.6	0.62	--	180	42	2
PD2	40	54	66	81	1.4	0.41	0.5	1.4	12	10	7	5
PD3	101	2500	1298	--	0.6	1.17	2.3	-	7	13	5	-
PD4	20	2200	1100	1040	0.4	2.21	3.2	8.1	3	3	5	4

K13

TABLE K4 (Continued)

Sample Code	Na, mg/l				Mn, mg/l				Fe, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
PE1	315	151	364	-	2.0	5.13	5.0	-	4	15	5	-
PE2	495	300	408	1010	4.5	3.00	4.3	4.4	260	51	15	340
PF1	6	7	24	-	0.3	0.018	0.3	-	3	8	17	-
PF2	40	40	41	-	0.2	0.006	0.6	-	2	10	55	-
PG1	-	-	96	-	-	-	0.1	-	-	-	170	-
PG2	25	93	100	-	0.07	0.053	0.1	-	520	285	95	-
PH1	40	-	18	-	0.03	-	0.1	-	9	-	90	-
PH2	178	2	124	121	0.02	0.001	0.1	0.49	5	10	5	6
PI	87	100	150	-	0.95	0.25	0.8	-	5	26	20	-
PJ	8	5	-	30	0.07	0.0005	-	0.01	15	70	-	29

TABLE K4 (Continued)

Sample	Cu, mg/l				Zn, mg/l				Cd, µg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
PA1	-	24.6	0.5	6	-	0.13	0.004	0.083	--	1.0	0.4	4.0
PA2	35	28	28	16	0.17	0.06	0.012	0.012	0.5	0.9	0.6	0.7
PA3	41	33	8	16	0.07	0.06	0.002	0.015	0.5	0.8	0.3	0.4
PA4	53	31	13	29	0.20	0.02	0.006	0.006	0.5	1.1	0.7	0.5
PB1	-	345	-	14	-	0.65	-	0.013	0	2.0	-	0.4
PB2	42	153	20	14	2.60	3.22	0.095	-	2.6	10.2	0.9	-
PB3	42	74	28	-	2.10	1.95	0.403	-	2.6	9.0	0.4	0
PB4	58	88	35	24	2.10	3.51	0.141	0.06	3.4	4.6	1.6	4
PC1	75	149	160	-	0.47	0.81	.273	ND	2.8	2.0	8.2	0
PC2	36	134	8	16	0.16	0.15	0.042	0.5	0.4	1.2	0.2	0.5
PC3	40	25	13	10	0.13	0.07	0.008	0.012	0.2	1.3	0.4	0.4
PC4	28	43	13	25	0.10	0.06	0.012	0.058	0.1	1.1	0.6	2
PD1	-	341	257	19	-	1.73	1.41	2.48	-	3.0	3.3	3
PD2	16	23	3	14	0.75	0.31	0.181	0.039	1.6	1.1	0.2	3
PD3	3	60	1	-	0.17	0.12	0.055	-	0.2	1.2	0.9	-
PD4	2	1	13	5	0.0	0.07	0.181	0.014	0.1	1.2	1.0	0.2

K45

TABLE K4 (Continued)

Sample Code	Cu, mg/l				Zn, mg/l				Cd, ug/l			
	A	B	C	D	A	B	C	D	A	B	C	D
PE1	14	1.7	1	-	0.22	0.048	0.011	-	0.1	1.2	0.05	-
PE2	19	33	3	11	0.07	0.185	0.019	0.103	5.3	1.1	0.05	0.05
PF1	46	9	1	-	0.10	0.064	0.039	-	0.4	1.0	0.05	-
PF2	6	4	1	-	0.03	0.053	0.010	ND	0.1	1.2	0.05	-
PG1	-	-	35	-	-	-	-	-	-	-	0.03	-
PG2	9	28.5	12	-	0.09	0.160	0.019	-	0.1	1.4	0.02	-
PH1	6	-	3	-	0.06	-	0.007	-	0.5	-	0.02	-
PH2	7	2	1	13	0.05	0.062	0.008	0.061	0.1	1.1	0.05	0.05
PI	4	13	1	-	0.24	0.073	0.012	-	0.5	1.2	0.03	-
PJ	1	1	-	2	0.03	0.022	-	0.021	0.5	1.2	-	0.01

K46

TABLE K4 (Continued)

Sample Code	Ni, $\mu\text{g}/\text{l}$				Hg, $\mu\text{g}/\text{l}$				Pb, $\mu\text{g}/\text{l}$			
	A	B	C	D	A	B	C	D	A	B	C	D
PA1	-	17	31	10	-	0.6	--	--	-	2.3	0.1	3
PA2	27	5	18	9	1.1	0.1	--	--	2	6.35	0.1	0.5
PA3	20	4	18	20	1.1	0.6	--	--	2	4.3	0.1	0.1
PA4	31	4	22	10	1.0	0.0	--	--	2	1.4	0.0	0.0
PB1	-	15	-	8	-	0.3	--	--	-	1.8	-	3
PB2	300	170	51	-	0.2	0.2	--	--	1	1.4	1	-
PB3	270	75	40	-	0.9	0.2	--	--	1	1.0	5	-
PB4	210	210	29	23	0.5	0.0	--	--	1	0.6	0.1	2
PC1	17	23	68	-	0.5	0.0	--	--	1000	3	5	-
PC2	15	5	13	11	0.4	0.0	--	--	ND	1.1	5	3
PC3	13	2	5	5	0.2	0.0	--	--	3.8	1.4	1	1
PC4	11	3	9	17	0.2	0.5	--	--	2.9	1.8	2	1
PD1	-	26	55	93	-	0.2	--	--	-	3.3	4	2
PD2	34	15	9	50	0.2	0.2	--	--	0.5	0.7	2	1
PD3	19	4	7	-	0.2	0.0	--	--	0.1	0.9	1	ND
PD4	15	7	85	23	0.3	0.0	--	--	0.0	3.7	0.1	3

TABLE K4 (Continued)

Sample Code	Ni, $\mu\text{g}/\text{l}$				Hg, $\mu\text{g}/\text{l}$				Pb, $\mu\text{g}/\text{l}$			
	A	B	C	D	A	B	C	D	A	B	C	D
PE1	21	5	15	-	0.4	0.0	--	--	2	0.1	0.0	-
PE2	21	11	11	40	0.6	0.2	--	--	3	0.9	2	4
PF1	11	2	4	-	0.1	0.0	--	--	0.5	0.6	0.3	--
PF2	11	2	5	-	0.1	0.0	--	--	0.1	1.0	2	--
PG1	--	--	7	--	--	--	--	--	--	--	4	--
PG2	11	3	4	--	0.3	0.5	--	--	5	2.7	2	--
PH1	15	-	2	-	0.8	--	--	--	3	--	3	--
PH2	27	3	11	3	0.3	0.5	--	--	2	0.1	3	4
PI	19	2	4	-	0.3	0.1	--	--	0.5	0.0	0.3	-
PJ	11	2	-	0	0.2	0.0	--	--	0.5	0.9	-	2

TABLE K4 (Continued)

Sample Code	pH				Eh, mV				Sulfate, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
PA1	-	7.1	7.9	6.4	-	140	100	90	-	-	567	250
PA2	7.3	7.4	7.2	6.8	-	14	190	100	1887	900	370	1050
PA3	7.5	7.7	8.0	5.5	-	130	-20	170	2176	1140	1275	1504
PA4	7.4	7.3	6.7	6.7	-	190	180	63	2850	1150	310	1000
PB1	-	7.4	6.7	6.3	-	140	300	80	--	--	1200	--
PB2	7.3	6.5	7.3	-	-	250	240	-	2208	1200	850	-
PB3	-	6.3	7.2	-	-	150	140	-	2288	1100	1030	-
PB4	7.2	6.2	7.4	5.6	-	300	150	-31	2368	1800	782	925
PC1	-	5.9	7.3	-	-	310	240	--	-	-	400	-
PC2	-	7.4	7.1	6.4	-	200	250	80	-	-	170	-
PC3	8.0	7.5	6.8	5.6	-	130	250	90	186	550	313	350
PC4	8.3	7.6	6.3	6.7	-	190	40	130	282	450	103	250
PD1	-	4.8	7.5	6.2	-	390	360	31	-	-	450	550
PD2	7.1	7.4	7.0	6.7	-	65	150	50	-	-	490	700
PD3	7.2	7.5	7.1	-	-	260	160	0	181	-	360	-
PD4	7.4	7.2	7.9	5.8	-	120	90	120	131	1400	760	1763

TABLE K4 (Continued)

Sample Code	pH				Eh, mV				Sulfate, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
PE1	7.5	6.8	7.4	-	-	-83	90	-	820	1100	690	-
PE2	7.3	6.7	7.2	6.6	-	-3	100	58	800	1300	765	875
PF1	-	7.9	7.3	-	-	110	250	-	-	-	38	-
PF2	8.1	7.2	7.4	-	-	120	270	-	60	148	130	-
PG1	-	-	7.2	-	-	-	230	-	-	-	-	-
PG2	7.3	7.3	6.8	-	-	250	210	-	180	-	-	-
PH1	-	-	7.2	-	-	-	230	-	-	-	-	-
PH2	8.2	7.4	7.1	6.8	-	150	260	110	145	75	90	40
PI	-	7.7	7.1	5.7	-	140	150	240	-	75	265	516
PJ	8.2	7.6	-	6.1	-	210	-	90	131	50	-	35

K50

TABLE K 4 (Continued)

Sample Code	Chloride, mg/l				Alk., mg/l				TOC, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
PA1	-	-	845	1948	-	-	317	485	-	-	65	180
PA2	6358	1615	2127	3913	517	484	461	638	35	45	70	195
PA3	6514	4794	4690	5916	471	1052	1066	963	5	110	120	310
PA4	6462	4533	3819	4686	400	977	826	733	ND	85	90	240
PB1	-	-	2793	-	-	-	422	-	-	-	45	-
PB2	9641	4221	3460	-	110	163	394	-	50	45	45	-
PB3	9797	4229	3152	-	207	185	394	-	20	65	55	-
PB4	9224	6097	3050	3406	189	185	408	393	5	60	45	150
PC1	-	-	450	-	-	-	34	-	-	-	10	-
PC2	-	-	589	-	-	-	312	-	-	-	35	-
PC3	1355	1355	999	2538	814	735	610	576	30	215	60	160
PC4	1355	1511	948	2148	845	823	634	581	-	140	55	160
PD1	-	-	93	125	-	-	-	125	-	-	9	20
PD2	-	-	82	130	-	-	48	37	-	-	20	22
PD3	165	-	2229	-	70	-	298	-	25	-	30	-
PD4	16	85	2024	1731	45	304	250	205	30	45	30	50

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TABLE K4 (Continued)

Sample Code	Chloride, mg/l				Alk., mg/l				TOC, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
PE1	269	165	458	-	121	136	322	-	20	35	30	-
PE2	625	258	550	1153	233	-	366	479	10	45	30	235
PF1	-	-	34	-	-	-	89	-	-	-	10	-
PF2	104	66	77	-	178	66	77	-	-	30	2	-
PG1	-	-	85	-	-	-	91	-	-	-	37	-
PG2	24	-	-	-	62	-	-	-	20	-	-	-
PH1	-	-	-	-	-	-	-	-	-	-	13	-
PH2	80	82	103	154	361	189	307	364	-	30	15	110
PI	-	72	119	106	-	154	165	257	-	55	20	85
PJ	29	15	-	48	114	40	-	120	-	10	-	20

K52

TABLE K 4 (Continued)

Sample Code	Total Inorganic Carbon, mg/l				Total Carbon, mg/l				Phosphate, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
PA1	-	-	75	110	-	-	140	290	-	-	-	-
PA2	125	135	100	165	160	180	170	360	0.083	-	0.07	0.06
PA3	110	280	240	230	115	390	360	540	0.042	-	0.16	0.14
PA4	90	270	190	190	90	355	280	430	0.010	-	0.09	0.07
PB1	-	-	100	-	-	-	145	-	-	-	0.02	-
PB2	30	55	105	-	80	110	160	-	-	-	0.02	-
PB3	60	55	95	-	80	120	150	-	0.007	-	0.02	-
PB4	60	60	105	110	65	120	150	260	0.015	-	-	0.5
PC1	-	-	10	-	-	-	20	-	-	-	-	-
PC2	-	-	70	-	-	-	105	-	-	-	0.01	-
PC3	190	195	140	150	220	410	200	310	0.061	-	0.10	0.15
PC4	-	220	150	150	-	360	205	310	0.026	-	0.06	0.12
PD1	-	-	2	35	-	-	11	55	-	-	0.01	-
PD2	-	-	5	8	-	-	25	30	-	-	-	-
PD3	20	-	60	ND	45	-	90	-	0.002	-	-	-
PD4	10	75	50	50	40	120	80	100	0.005	-	-	0.07

TABLE K4 (Concluded)

Sample Code	Total Inorganic Carbon, mg/l				Total Carbon, mg/l				Phosphate, mg/l			
	A	B	C	D	A	B	C	D	A	B	C	D
PE1	30	45	65	-	50	80	95	-	0.038	-	0.01	-
PE2	65	55	70	165	75	100	100	400	0.007	-	0.02	-
PF1	-	-	20	-	-	-	30	-	-	-	0.01	-
PF2	-	20	18	-	35	-	-	-	0.018	-	-	-
PG1	-	-	18	-	-	-	55	-	-	-	-	-
PG2	15	-	-	-	35	-	-	-	0.018	-	-	-
PH1	-	-	27	-	-	-	40	-	-	-	-	-
PH2	-	110	75	90	-	140	90	200	0.012	-	0.09	-
PI	-	40	50	55	-	95	70	140	0.002	-	-	0.04
PJ	-	10	-	30	-	20	-	50	0.004	-	-	0.08

APPENDIX L: ANALYTICAL PROCEDURES

Core Sediment Samples

Carbon--total organic carbon (TOC)

1. Weigh about 5 g of sediment sample in a 150-ml beaker. Adjust pH below 2 to remove carbonates²⁰⁶ by adding 1:1 HCl; then bubble N₂ through the sample for about 10 minutes. Dry the sample in the same beaker for 24 hours in the temperature range of 70° to 100°C. Weigh a portion of this dried sample, about 0.5 to 1 g into a special Leco TOC crucible. Determine TOC content using a Leco TC-12 automatic carbon determinator.

Oil and grease

2. Determine oil and grease content by extracting a known weight of sediment with petroleum ether.²⁰⁶ After the phase separation, transfer the extract to a flask of known weight. Then evaporate the extract in an oil bath at 70°C until a constant weight is obtained. Use the relationship

$$\text{oil and grease, mg/kg} = \frac{\text{residue, g}}{\text{dried weight, g}} \times 10^6 \quad (\text{L1})$$

Chlorinated hydrocarbons (chlorinated pesticides and PCB's)

3. The overall method includes sample extraction, cleanup and separation, and identification of chlorinated hydrocarbons in accordance with the published literature.^{65,207-213} The details are described below.

4. Extraction. Weigh 10 g of wet sediment in a 500-ml Erlenmeyer flask with a ground-glass stopper and also weigh another 10 g of sediment to determine moisture content. Add 250 ml of acetonitrile (pesticide quality, Mallinkrodt) to the flask and shake for 1 hour on a gyratory shaker. Store the sample in a constant temperature chamber (14 ± 2°C) overnight. Shake the sample again for 2 hours and filter through 5 g of celite (celite 545, Sargent Welch) media on Whatman No. 4 filter paper under a mild vacuum. At this time, add another 100 ml of acetonitrile to avoid the possible loss of chlorinated hydrocarbons on the

flask wall, celite, or residue. Then transfer the filtrate to a 500-ml Kuderna-Danish concentrator and concentrate to 5 ml on a water bath. Transfer the concentrated extract (filtrate) to a 1000-ml separatory funnel containing 200 ml of double-distilled water and 10 ml of saturated aqueous NaCl. Use 80 ml of petroleum ether (pesticide quality) to clean the concentrator and add to the separatory funnel. Hand-shake the funnel for 5 minutes and then keep still until a clear separation of phases occurs. Drain the aqueous phase (bottom layer) into another separatory funnel containing 80 ml of petroleum ether for the second extraction. After the third extraction, discard the aqueous phase and collect all petroleum ether extracts into a Kuderna-Danish concentrator. After the petroleum ether extract is concentrated to approximately 5 ml, elute it on the prepared activated florsil column. (It should be noted that since sulfur is present in large amounts in every sediment every extract should be treated with mercury to remove sulfur before injection into the gas chromatograph.)

5. Florosil column elution. Pack a chromatographic tube (450 by 28 mm) having a removable frittered glass and teflon stopcock with 15 g of activated florosil (60/100 mesh, G.C. grade) and top it with 15 g of anhydrous sodium sulfate. Elute first with 175 ml of zero percent ethyl ether (EE)*, next with 100 ml of 6 percent EE, and finally with 150 ml of 15 percent EE. During elution, control the flow rate with the stopcock and maintain at approximately 2 ml per minute. (With this florosil column elution, PCB's and most of the DDE are recovered in zero percent EE, most organochlorine compounds in 6 percent EE, and endrin and dieldrin in 15 percent EE.) Concentrate the eluted sample again and measure the exact volume.

6. Identification and quantification. The purities of standard solutions of chlorinated hydrocarbons should be more than 99 percent. Use DDT series standards manufactured by Supelco and PCB standards and dieldrin standards manufactured by Monsanto and

* Zero percent EE = 0 percent (by volume) ethyl ether + 100 percent petroleum ether; 6 percent EE = 6 percent ethyl ether + 94 percent petroleum ether; and 15 percent EE = 6 percent ethyl ether + 85 percent petroleum ether.

and Shell, respectively. Also use a Hewlett-Packard research gas chromatograph model 5750 equipped with a Ni⁶³ electron capture detector. Pack the column (1220 by 4 mm) with 5 percent QF-1 (chromosorb W-HP, 80/100 mesh, Sargent Welch) and use the carrier gas consisting of 95 percent argon and 5 percent methane.

7. Perform preliminary sample injections to evaluate the need for further concentration or dilution of the samples.

8. Identify the sample components by comparing the retention times of unknown peaks to the known peaks of reference standard solutions. Quantify these components by comparing the peak height of the identified component to the peaks of the component in the reference standard solution. In addition to a single-component reference standard solutions, prepared multicomponent solutions with different concentration and component combinations. (This is done mainly to solve the problem of quantification of components with close retention times, like o, p' DDD and o, p' DDT, or p, p' DDT in 6 percent EE-eluted samples.

9. Extraction efficiency. The recovery efficiencies obtained at the University of Southern California¹¹⁹ and those given in the literature^{214,215} are compared in Table L1.

TABLE L1
Recovery Efficiency of Chlorinated Hydrocarbons
From Marine Sediments

<u>Pesticide</u>	<u>Recovery Efficiency, percent</u>		
	<u>Chen and Choi</u> ¹¹⁹	<u>Goerlitz and Law*</u> ²¹⁴	<u>Woolson</u> ²¹⁵
p,p' DDE	86-94	97.1-99.5	96
o,p' DDE	81-91		--
p,p' DDD	87-97	97.6-100	97
p,p' DDT	85-99		--
p,p' DDT	86-94	97.2-100	89
o,p' DDT	85-98		90
Dieldrin	85-94	--	91
PCB's	93-102	--	--

*Average values for p, p' and o,p'.

Acid-soluble sulfides

10. Use a titrimetric method²⁰⁶ for sulfide determination. (A 1-litre reaction flask and two 250-ml absorption flasks are necessary.) The procedure is as follows:

- a. Measure 5 ml zinc acetate and 95 ml distilled water into each of the two absorption flasks. Connect the reaction flask and two absorption flasks in a series and purge the system with N₂ gas at least 2 minutes. Transfer about 5 g of sediment into the reaction flask and add 500 ml of distilled water with complete mixing.
- b. Acidify the sample with 10 ml of concentrated H₂SO₄ and replace the prepared 2-hole stopper tightly. Pass N₂ through the sample for 1 hour.
- c. Add 10 ml of iodine solution and 2.5 ml concentrated HCl to each of the absorption flasks; stopper and shake to mix thoroughly.
- d. Transfer the contents of both flasks to a 500-ml flask and backtitrate with 0.025N sodium thiosulfate titrant using a starch solution as indicator. Run a blank using the same reagents. Use the relationship

$$\Sigma S^{-2}, \text{ mg/kg} = \frac{(\text{iodine, ml} - \text{Na}_2\text{S}_2\text{O}_3, \text{ ml})}{\text{dry weight, g}} \times 400 \text{ (L2)}$$

Nitrogen

11. Analyze both organic and ammonium nitrogen according to Standard Methods.²⁰⁶ Briefly, place a 1.5-g sample in a Kjeldahl flask. Add 180 ml distilled water and 15 ml phosphate buffer solution. Distill into a flask containing 30 ml boric acid until 120 ml is collected. Titrate the solution with 0.02N H₂SO₄ to determine the ammonia nitrogen content. Add 30 ml digestion reagent to the remaining portion and heat under a hood for about 30 minutes. Cool and dilute to 180 ml. Titrate with sodium hydroxide-sodium thiosulfate reagent. Distill and collect 120 ml of distillate into a flask containing 30 ml boric acid. Titrate with 0.02N H₂SO₄ to determine the organic nitrogen content. Carry a blank determination on distilled water and reagents. Use the relationship

$$N, \text{ mg/kg} = \frac{(a - b) C \times 14,000}{\text{dry weight, g}} \quad (\text{L3})$$

where a = amount of H₂SO₄ solution used for sample, ml
 b = amount of H₂SO₄ solution used for blank, ml
 c = normality of H₂SO₄ solution

Phosphorus

12. The total phosphorus analysis includes acid digestion.²⁰⁶ Place about 1 g of well-mixed sample into a Teflon beaker. Treat it with 4 to 5 drops of HF, 5 ml HNO₃, and 3 ml HClO₄ solution. Digest the mixture on a hot plate until the solution is almost dry. Cool and add 20 ml of distilled water then centrifuge the digested sample. Collect the supernatant in a 250-ml Teflon beaker. Adjust the pH to 0.2 to 0.3 with 6N HNO₃ then pass the supernatant through a cation exchange resin, such as ANGC-243 (manufactured by Ionac Chemical Co.) and collect the eluate in a beaker, adjusting the flow rate to no greater than 5 ml per minute. After passing the liquid through the column three times, neutralize the solution with 6N NaOH and 6N HNO₃ to a pH of 7. Dilute the solution to exactly 200 ml. Regenerate the ion exchange resin with 1:1 HCl and wash with distilled water.

13. Pipet 50 ml of digested sample. Add 2.0 ml molybdate acid solution and mix by swirling. Add 2.0 ml sulfonic acid solution and mix again. After exactly 5 minutes, measure the absorbance versus the blank at a wavelength of 690 mμ. Prepare a calibration curve by using a suitable volume of standard phosphate solution.

Trace metals

14. Core sediment samples. Use a Perkin Elmer model 305B and a Perkin Elmer model 60 atomic absorption spectrophotometer, each equipped with a flame and graphite atomizer (HGA 2100) and Deuterium Arc background corrector, for the metals analysis. The HGA direct injection technique, as outlined in "Analytical Methods for AA Spectroscopy Using the HGA Graphite Furnace" provided by

Perkin Elmer, can be used with the Deuterium Arc background corrector to measure trace metal concentrations ranging from a few $\mu\text{g}/\text{l}$ to several hundred $\mu\text{g}/\text{l}$. Concentrations ranging from several hundred $\mu\text{g}/\text{l}$ to the ppm range can be determined with the flame atomizer. Dilution with deionized distilled water is necessary for certain samples in order to decrease the concentrations to a suitable working range. Tables L2 and L3 summarize the operating conditions, sensitivities, and working ranges for the flame and HGA atomizer for the metals analysis. Mercury was determined by the cold vapor method.

15. Ammonium acetate extractable elements (Ca, Mg, Na, K, Mn, Zn, Fe, Cd, Hg, Pb, Cu, Ni). Transfer a well-mixed subsample of a sediment²¹⁶ to a tared 250-ml polycarbonate centrifuge bottle under a nitrogen atmosphere inside a glove bag. Add oxygen-free, double-distilled water to the bottle to obtain a sediment (water ratio 1:5). Take another sample to determine the moisture content and percent solids. Seal the centrifuge bottles then shake for 90 minutes. Separate the soluble phase via centrifugation and vacuum filtration through 0.45- μm membrane filters in a glove bage under nitrogen.

16. Add 1.0 N ammonium acetate (deaerated) solution to the entire residue from above to obtain a 1:6 sediment-to-extract ratio based on the original sample weight. Complete this step in a glove bag under a nitrogen atmosphere. Shake the sealed centrifuge bottles for 90 minutes on a mechanical shaker. Separate the exchangeable phase via centrifugation and oxygen-free vacuum filtration through a 0.05- μm membrane filter. Acidify the solution to a pH of 1 to 2 for trace metals analysis.

17. Total acid-digestable elements (Ca, Mg, Na, K, Mn, Zn, Fe, Cd, Hg, Pb, Cu, Ni).²¹⁶ Solid sample for the determination of metals (except Hg) will be digested by concentrations of HF, HNO_3 and HClO_3 until clear solution at 175°C in Teflon beaker (with Teflon cover). Spectrophotometers (Models 305B and 460) will be used for the analysis of metals. Both flame and heated graphite atomizers (HGA 2100) will be used for total sample analysis. The choice of an atomizer is dependent on the suitable linear range of the element.

18. Trace metals except mercury. Determine the moisture content of about 1 g of wet sediment. Weigh the sediment into a Teflon beaker. Digest the sample with 6 ml HNO_3 , 4 ml HF, and 3 ml HClO_4 in a covered Teflon beaker at approximately 175°C . After evaporation to about 2 ml, dilute the sample to a fixed volume and centrifuge, if necessary, to eliminate solids.

19. Mercury. Weigh about 5 g of well-mixed sample into a Erlenmeyer flask and treat with 20 ml concentrated HNO_3 and 15 ml of 2-percent KMnO_4 . Seal the flask and heat in a constant temperature water bath at 70°C for 12 hours. Allow the flask to cool and then centrifuge the digested sample. Collect the supernatant in a 100-ml volumetric flask and dilute to the etched mark.

Particle size distribution

20. Pretreat the sediment sample with 30 percent H_2O_2 to remove organic matter using 6 mg/l of sodium hexametaphosphate (NaPO_3)₆ (J. T. Baker Chemical Co.) solution as a dispersing agent. After wet-seiving the sample using a U. S. Standard No. 230 sieve, analyze the particles of the fine fraction ($\leq 65 \mu\text{m}$) in accordance with the pipette method.²¹⁷

Cation exchange capacity

21. Determine the cation exchange capacity using the sodium saturation methods described in Methods of Soil Analysis.

Bulk density.

22. Determine the bulk density using the core method as described in Methods of Soil Analysis, Part I.²¹⁷

Hydraulic conductivity

23. Hydraulic conductivity (coefficient of permeability) is defined as the rate of discharge of water under laminar flow conditions through a unit cross-sectional area of a porous media under a unit hydraulic gradient at a temperature of 20°C . The falling head method is generally used for relatively impervious soils, such as fine sand, clay, and silt where the flow rate is very small (10^{-4} cm/sec). A laboratory designed permemeater, (Figure L1) using the falling head method, is used for this analysis. Calculate the hydraulic conductivity as

$$K = \frac{QL}{Ath} \quad (L4)$$

Where Q = quantity of water discharge

L = distance between manometers

A = cross-sectional area of porous media

t = total time of discharge

h = headloss between manometers

The K values are standardized to $K_{20^{\circ}\text{C}}$ by the use of a viscosity correction table. ²¹⁸

Percent moisture

24. Determine the percent moisture of sediment samples in accordance with (ASTM) Designation D 2216-71, "Standard Method of Laboratory Determination of Moisture Content of Soils."²¹⁶ (This procedure expresses the moisture content as a percentage of the weight of water in a given mass of soil to the weight of the solid particles. The moisture content is determined by drying in a drying oven at $100 \pm 5^{\circ}\text{C}$.)

Moisture-holding capacity

25. The moisture-holding capacity is defined as the smallest value to which the water content of a soil can be reduced by gravity.⁷³ Determine the moisture-holding capacity (moisture equivalent) in accordance with ASTM Designation D 425-69, "Standard Method of Test for Centrifuge Moisture Equivalent of Soils."⁷⁰ (The general procedure involves the determination of the moisture content of a soil after it has been saturated with water and then centrifuged in a Gooch crucible for 1 hour at 1000 g's. It should be noted that this procedure only approximates natural percolation and it cannot be assumed that the centrifuge moisture equivalent represents the in situ field capacity.^{71,72} Many investigators have shown, however, that the moisture equivalent can be correlated with the actual field capacity for many soil samples. ²¹⁹⁻²²⁴

Interstitial soil-water samples (less than 0.45 μm)

Carbon total and inorganic ²²⁵

26. Use a Beckman Model 915A total organic carbon analyzer

TABLE L2
Operating Conditions for the Flame Atomizer on the Perkin Elmer 305B
Atomic Absorption Spectrophotometer

Element	Wave-length nm	Slit	Oxidant and Fuel	Flame Condition	Sensitivity ppm	Suitable Working Range ppm
Cd	227.7	4	Air acetylene	Oxidizing-lean blue	0.025	0.025 -2
Cu	324.0	4	"	"	0.09	0.09-5
Fe	247.2 247.9	3	"	"	0.12	0.12-5
Mn	278.5 278.8 279.1	3	"	"	0.055	0.055-3
Ni	230.0	4	"	"	0.15	0.15-5
Pb	282.4 279.0	4	"	"	0.5	0.5-20
Sn	212.6	4	"	"	0.018	0.018-1
Ca	213.6(vis)	4	"	Reducing-rich yellow	1	1-20
Mg	284.4(uv)	4	"	"	1	1-40
Na	Emission 297.1(vis)	4	"	Oxidizing-lean blue	1	1-30
K	Emission 385.5(vis)	4	"	"	1	1-5

TABLE L3
Operating Conditions for HGA Direct Injection Method

Sample back- ground	Ele- ment	Wave- length nm	Silt	Back- ground correc- tor	Sam- ple size μ	Drying		Charring		Atomizing		Sensi- vity
						Temp °C	Time sec	Temp °C	Time sec	Temp °C	Time sec	
Aqueous	Cd	228.0UV	4	w/	5050	115	20-50	300	30	1500	7	1.5
	Cu	324.7UV	4	2/o	"	"	"	950	"	2550	"	30
	Fe	248.3UV	3	w/	"	"	"	1250	"	2400	"	15
	Mn	279.5UV	3	w/	"	"	"	1100	"	2400	"	4
	Ni	231.2UV	3	w/	"	"	"	1200	"	2550	"	100
	Pb	283.3UV	4	wor w/o	"	"	"	550	"	2000	"	20
	Zn	213.9UV	4	w/	"	"	"	500	"	2000	"	0.5

to determine:

- a. Total carbon (organic carbon plus carbon in carbonates).
- b. Inorganic (i.e., carbonate) carbon.

For determination of total organic carbon (TOC), perform two analyses on successive identical samples; the desired quantity is the difference between the two values obtained. (Both analyses are based on conversion of sample carbon into carbon dioxide for measurement by the nondispersive infrared analyzer. The basic model 915A total organic carbon analyzer consists of two interconnected units: a sample-inject/furnace module and a model 865 nondispersive infrared analyzer. For a carrier-gas/oxidizer, the system required a maximum of 300 cc per minute of clean, pressurized, suitably regulated air or oxygen (ultrapure grade or equivalent). Results of analyses register as peaks on a stripchart recorder. A Beckman 10-in potentiometric recorder is used. The ranges of the model 915A TOC analyzer are 0 to 5 and 0 to 4000 ppm. It can achieve sensitivity better than 0 to 5 ppm. Repeatability is ± 2 percent of full scale from 50 to 4000 ppm and ± 5 percent of full scale at 5 ppm.

Oil and grease

27. Determine oil and grease using the method described in paragraph 2. ²⁰⁶

Chlorinated hydrocarbons

28. Use the method of analysis outlined in paragraph 3-9. (The volume of sample used will range from 250 to 750 ml depending on concentration of chlorinated hydrocarbons.)

Total sulfides

29. Use an Orion Sulfide Ion Electrode (Model 94-6) with a Corning portable pH/mV meter to determine the total sulfides.

Sulfates

30. Determine sulfates using the turbidimetric method described in Standard Methods. ²⁰⁶

Phosphorus

31. Determine orthophosphate using the aminonaphtholsulfonic acid method. ²⁰⁶

Soluble metals

32. Use the method described in paragraph 17.

Chlorides

33. Determine the levels of chloride ions using a titrimetric method with mercuric nitrate as titrant at a pH of 2.3 to 2.8 in the presence of diphenyl-carbazone indicator. ²⁰⁶

Alkalinity

34. Determine alkalinity using the indicator method. Acidify the sample and then back titrate with NaOH using phenolphthalein as the indicator. ²⁰⁶

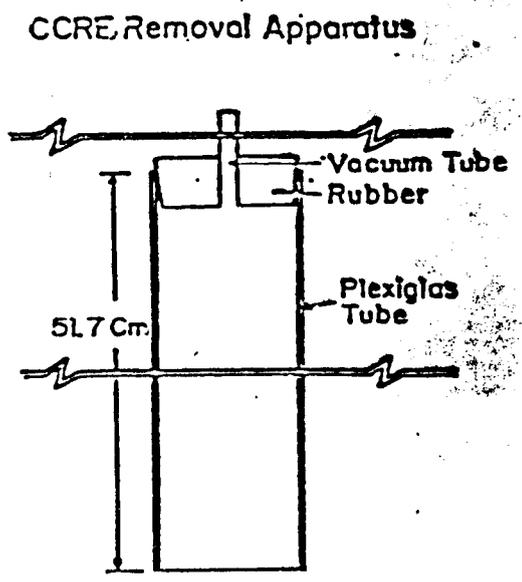
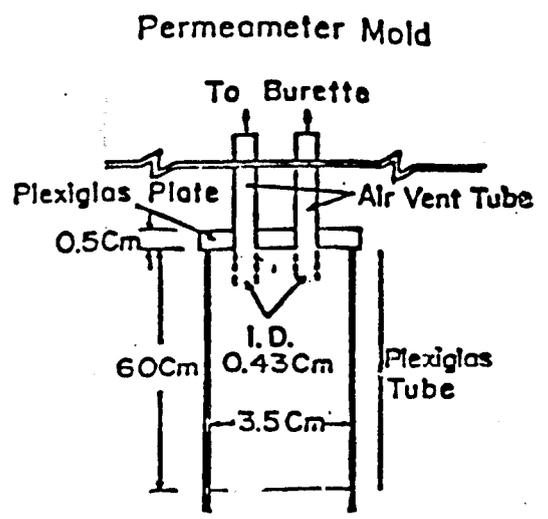
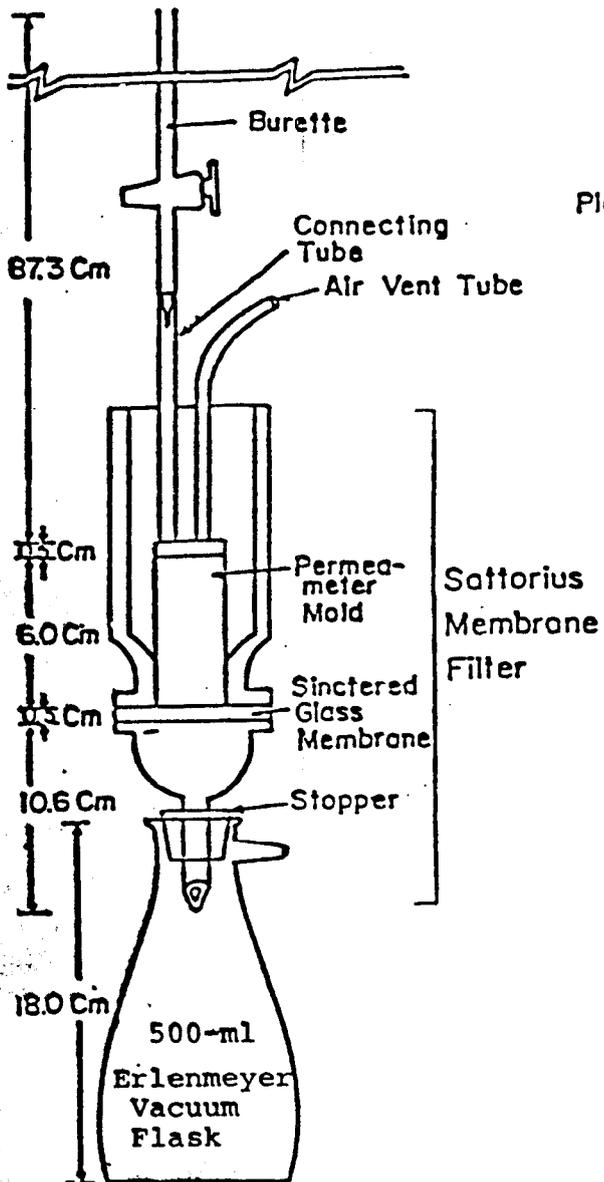


Figure L1. Modified laboratory permeameter.

In accordance with letter from DAEN-RDC, DAEN-ASI dated 22 July 1977, Subject: Facsimile Catalog Cards for Laboratory Technical Publications, a facsimile catalog card in Library of Congress MARC format is reproduced below.

Yu, Kar Y

Physical and chemical characterization of dredged material sediments and leachates in confined land disposal areas / by Kar Y. Yu, Kenneth Y. Chen, Environmental Engineering Program, University of Southern California, Los Angeles, Calif., and Robert D. Morrison, James L. Mang, SCS Engineers, Long Beach, Calif. Vicksburg, Miss. : U. S. Waterways Experiment Station ; Springfield, Va. : available from National Technical Information Service, 1978.

xiv, 241, [199] p. : ill. ; 27 cm. (Technical report - U. S. Army Engineer Waterways Experiment Station ; D-78-43)

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Appendices A-I, on microfiche in pocket.

References: p. 96-112.

1. Dredged material.
2. Dredged material disposal.

(Continued on next card)

Yu, Kar Y

Physical and chemical characterization of dredged material sediments and leachates in confined land disposal areas . . . 1978. (Card 2)

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